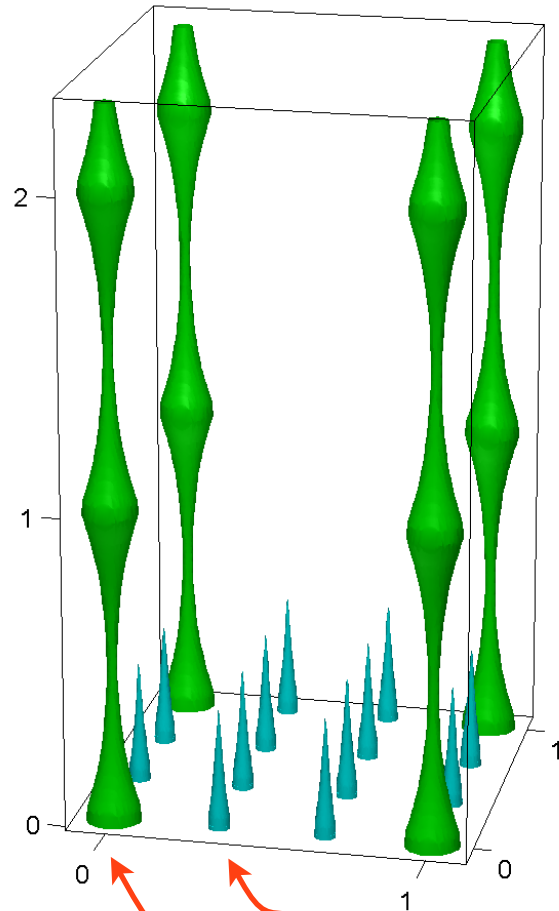
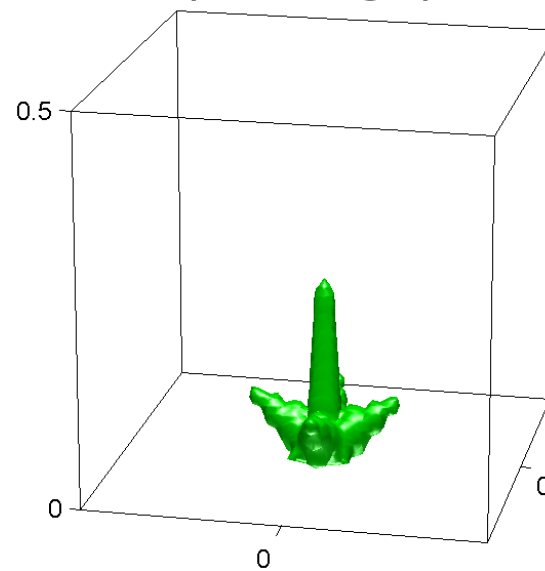


# Surface and Interface Scattering

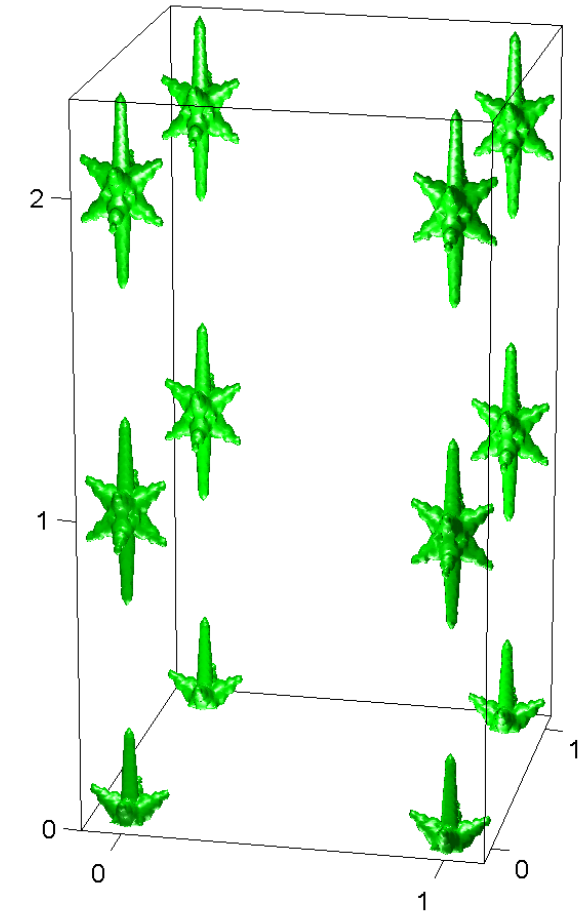
Dillon Fong (fong@anl.gov)  
Materials Science Division  
Argonne National Laboratory

## Surface x-ray diffraction (SXRD, SXS, GIXS, GIXD, ...)

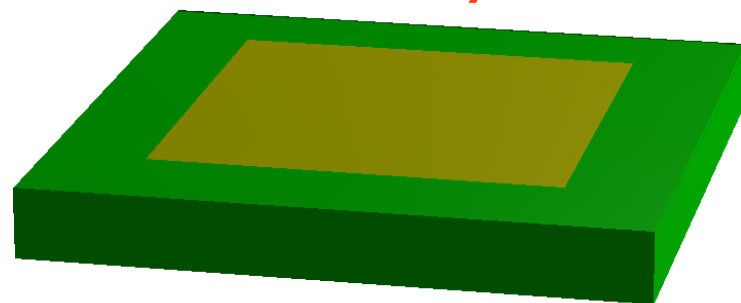
## 1D Fourier transform

3D Fourier transform  
(average)

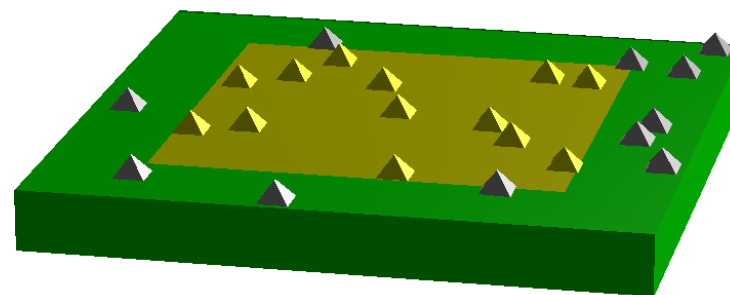
## 3D Fourier transform



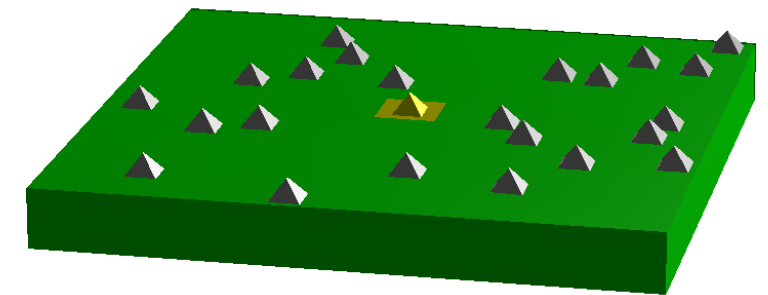
superstructure rods (SRs)  
crystal truncation rods (CTRs)



SXRD



GISAXS

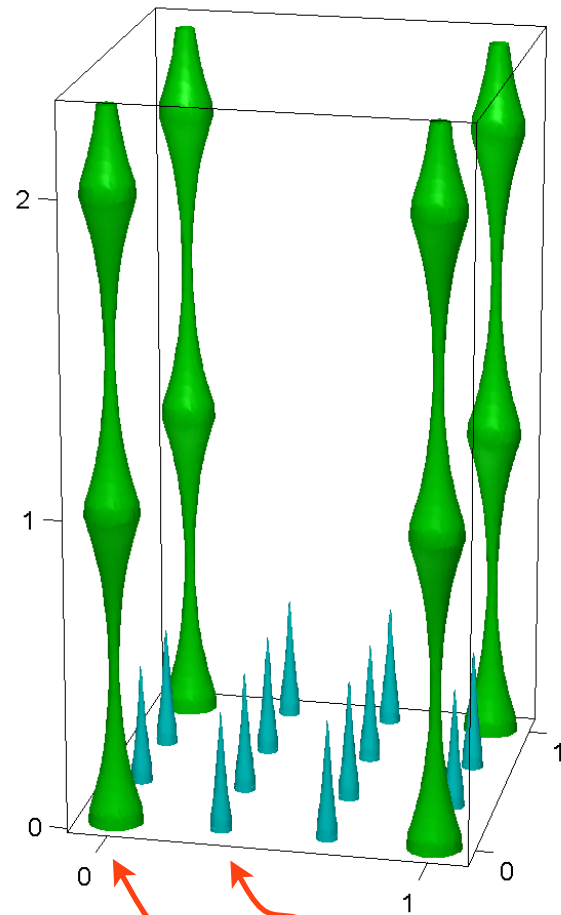


CDI

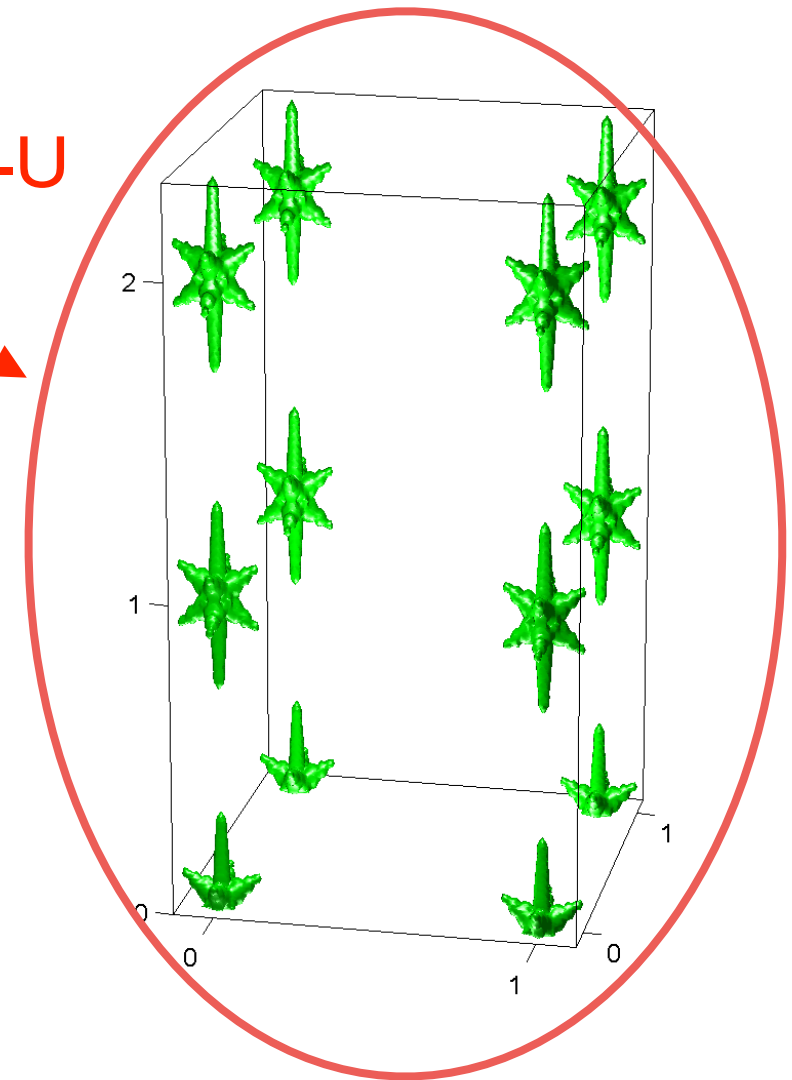
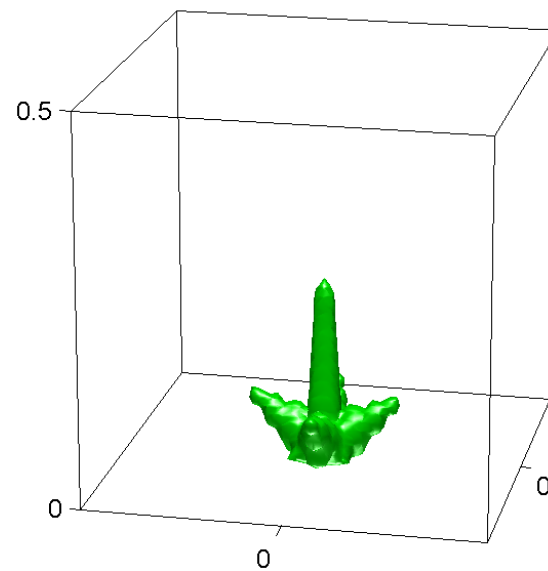
D. D. Fong *et al.* MRS Bulletin **35**, 504 (2010)



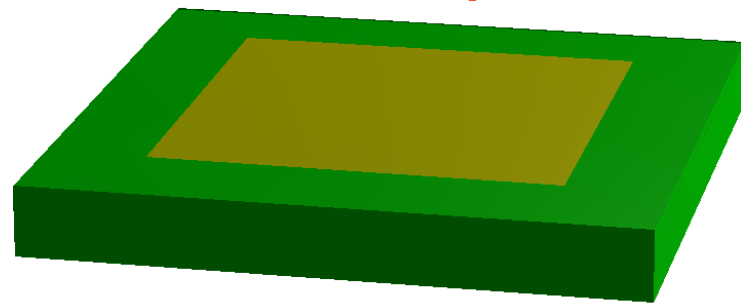
## Surface x-ray diffraction (SXRD, SXS, GIXS, GIXD, ...)



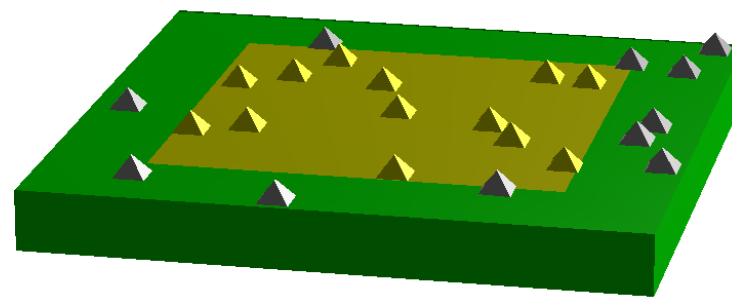
enhanced by APS-U



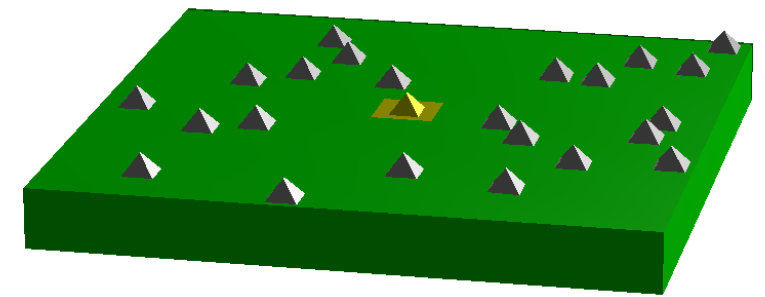
superstructure rods (SRs)  
crystal truncation rods (CTRs)



SXRD



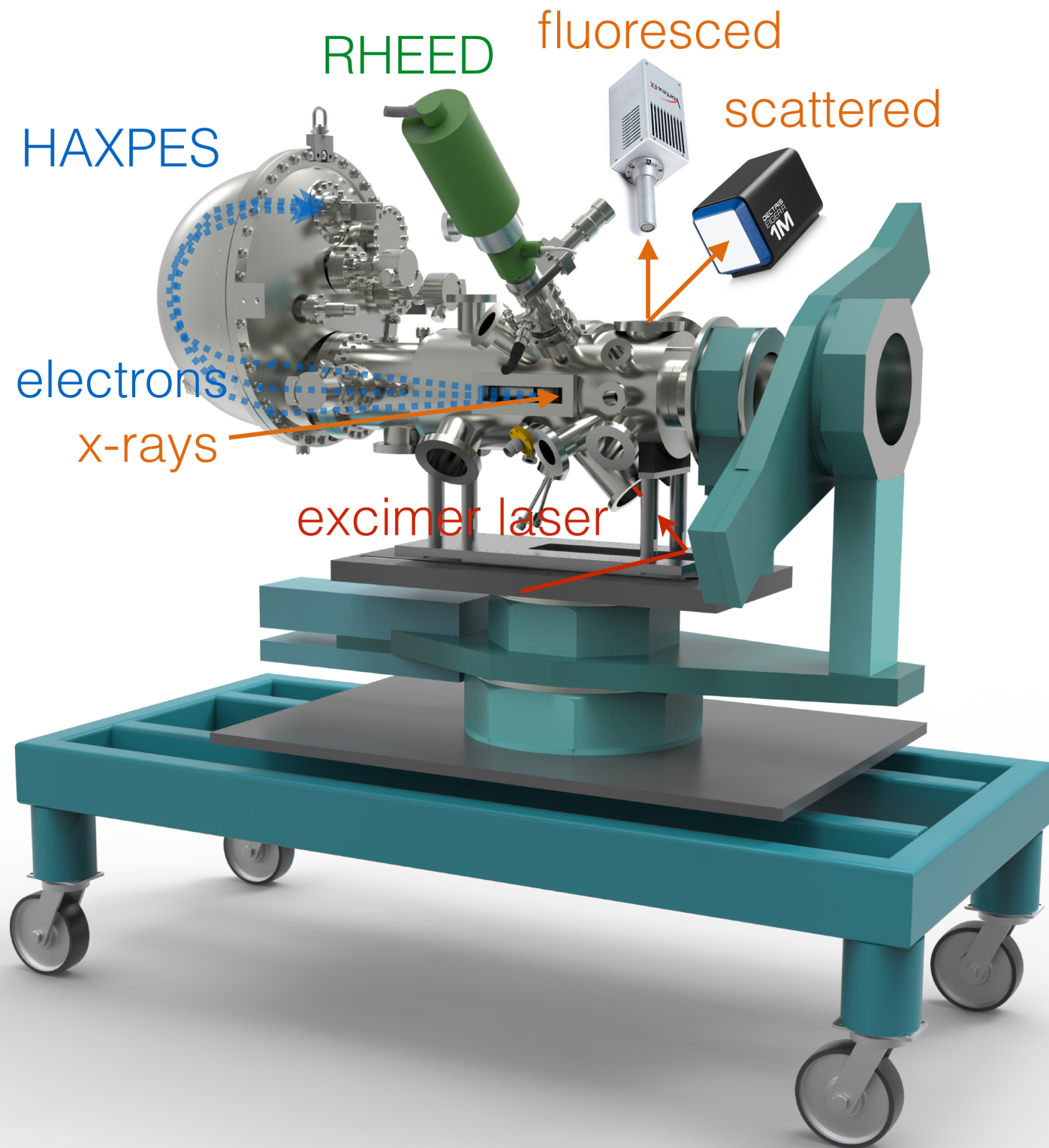
GISAXS



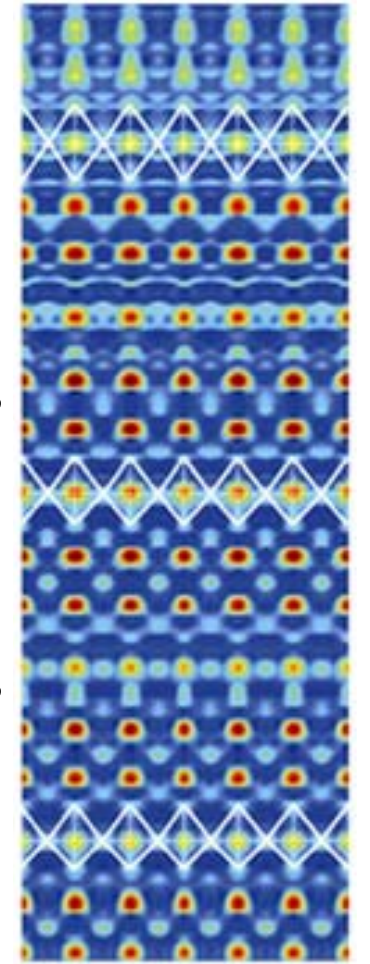
CDI

D. D. Fong *et al.* MRS Bulletin **35**, 504 (2010)

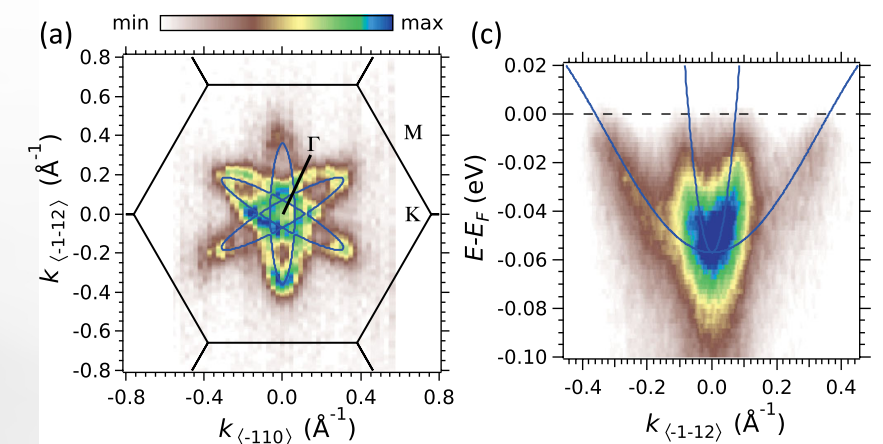
# Motivation: Watch materials creation



- atomic structure (SXRD)
- occupied electronic levels (HAXPES)
- unoccupied electronic levels (XANES)
- band structure (HARPES)



H. Zhou *et al.*, PNAS 107, 8103 (2010).

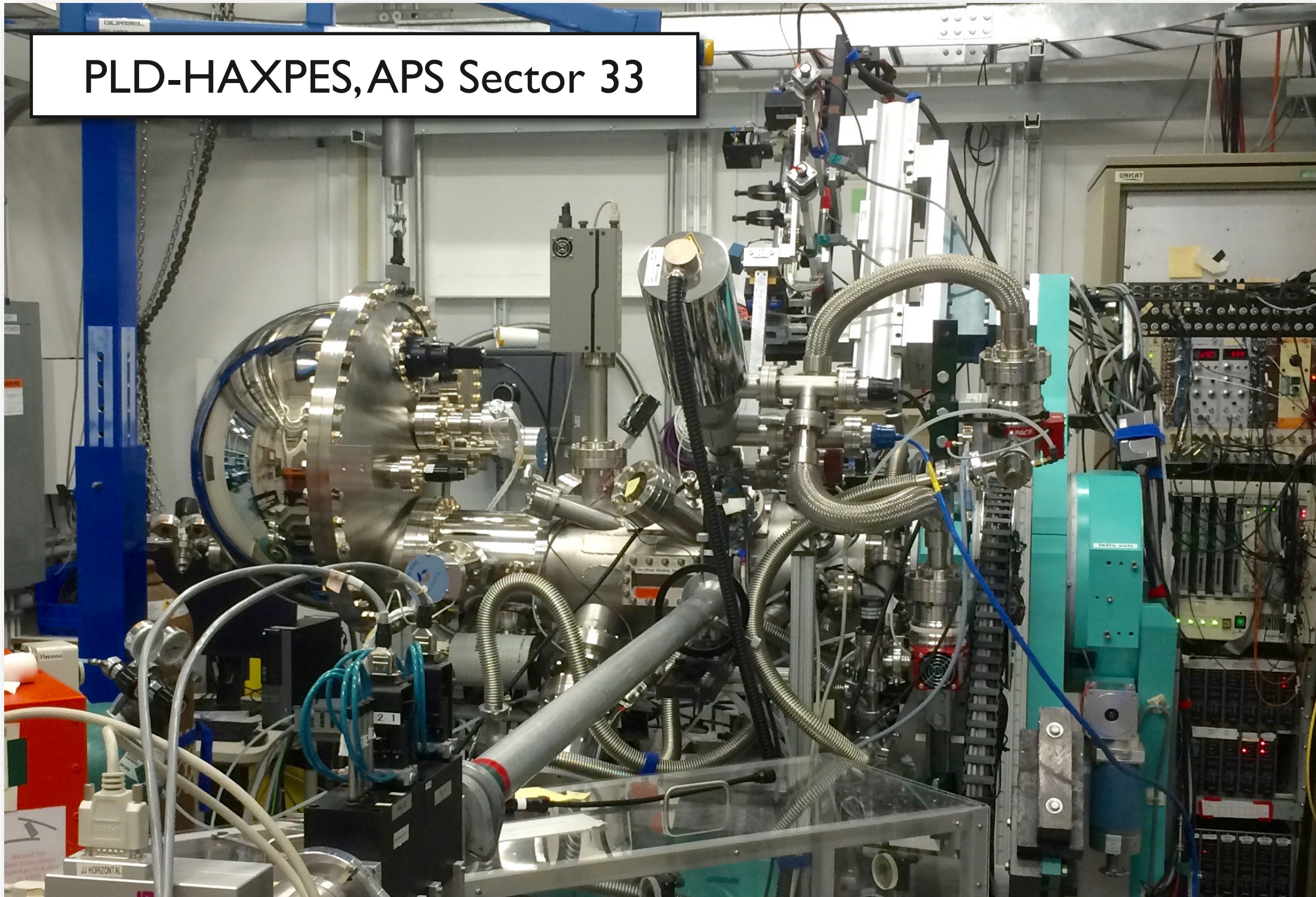


T.C. Rödel *et al.*, Phys. Rev. Appl. 1, 051002 (2014).



# Motivation: Watch materials creation & property evolution during creation

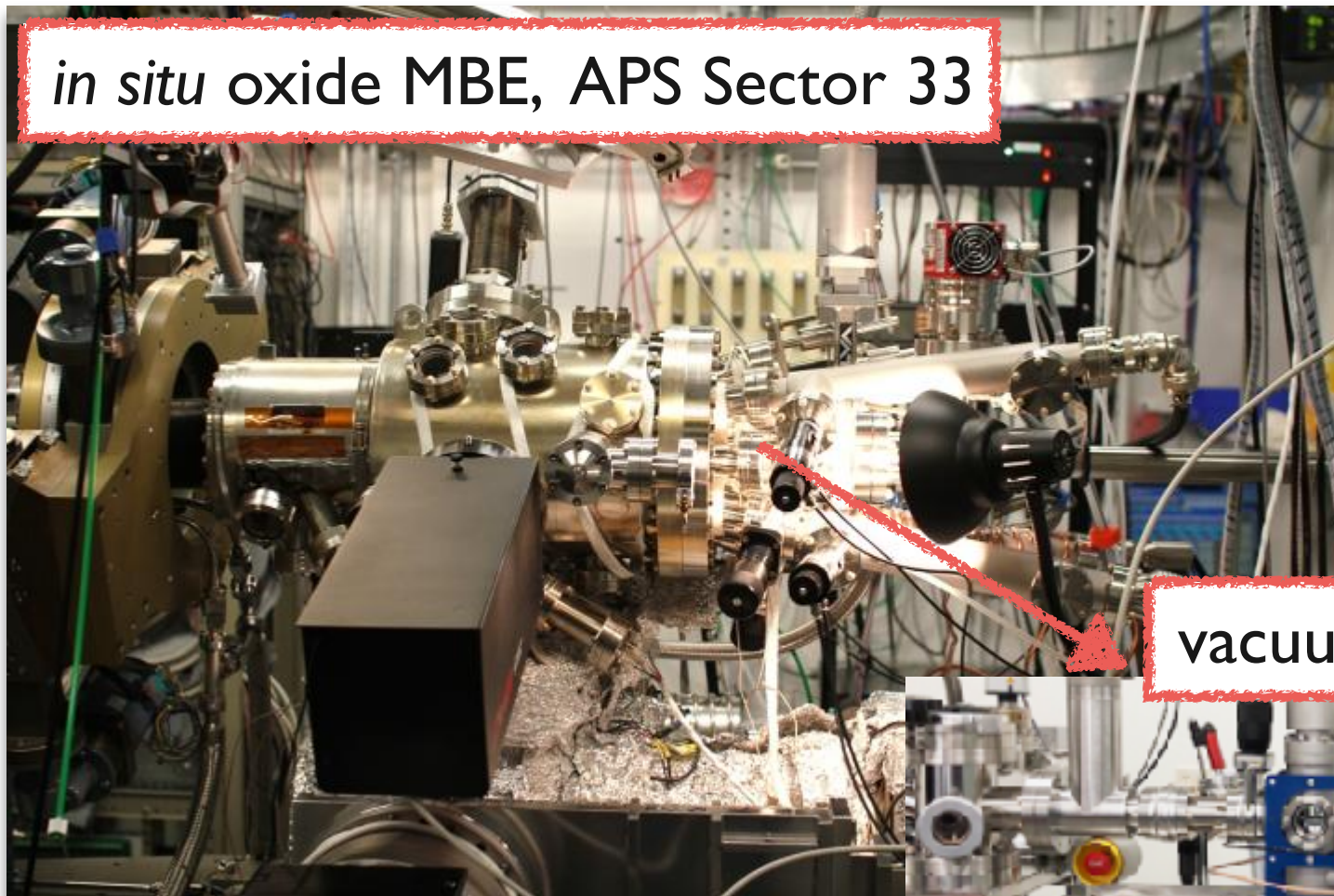
## PLD-HAXPES, APS Sector 33



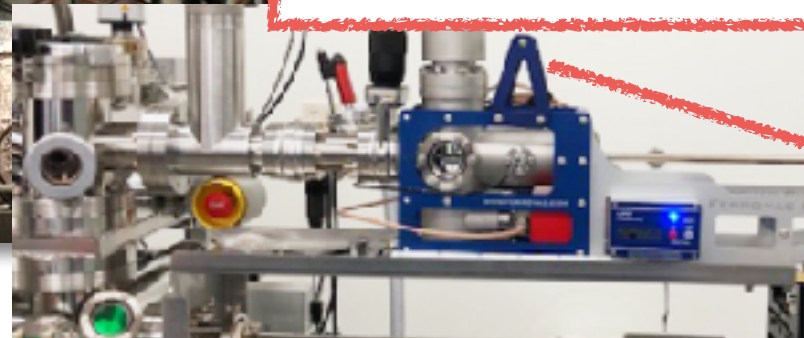


# Motivation: Watch materials creation & property evolution during creation

*in situ* oxide MBE, APS Sector 33



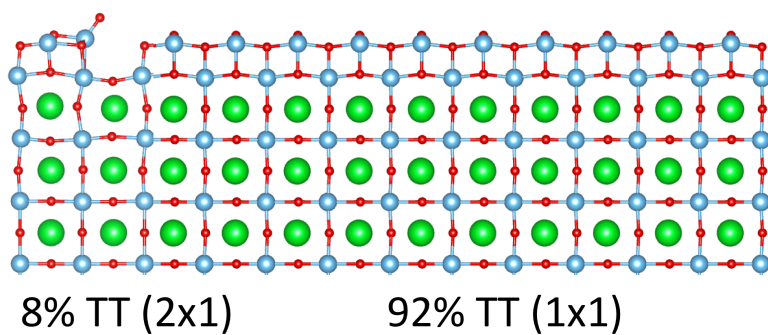
vacuum suitcase



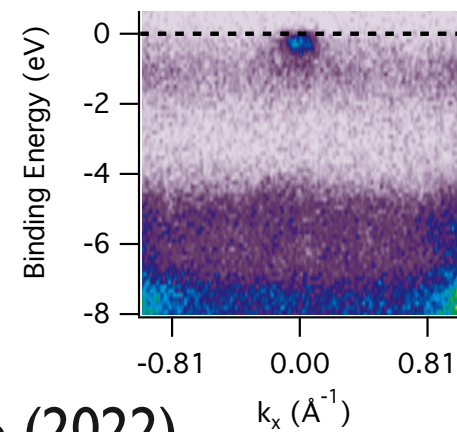
ARPES at Sector 29



atomic structure



electronic structure

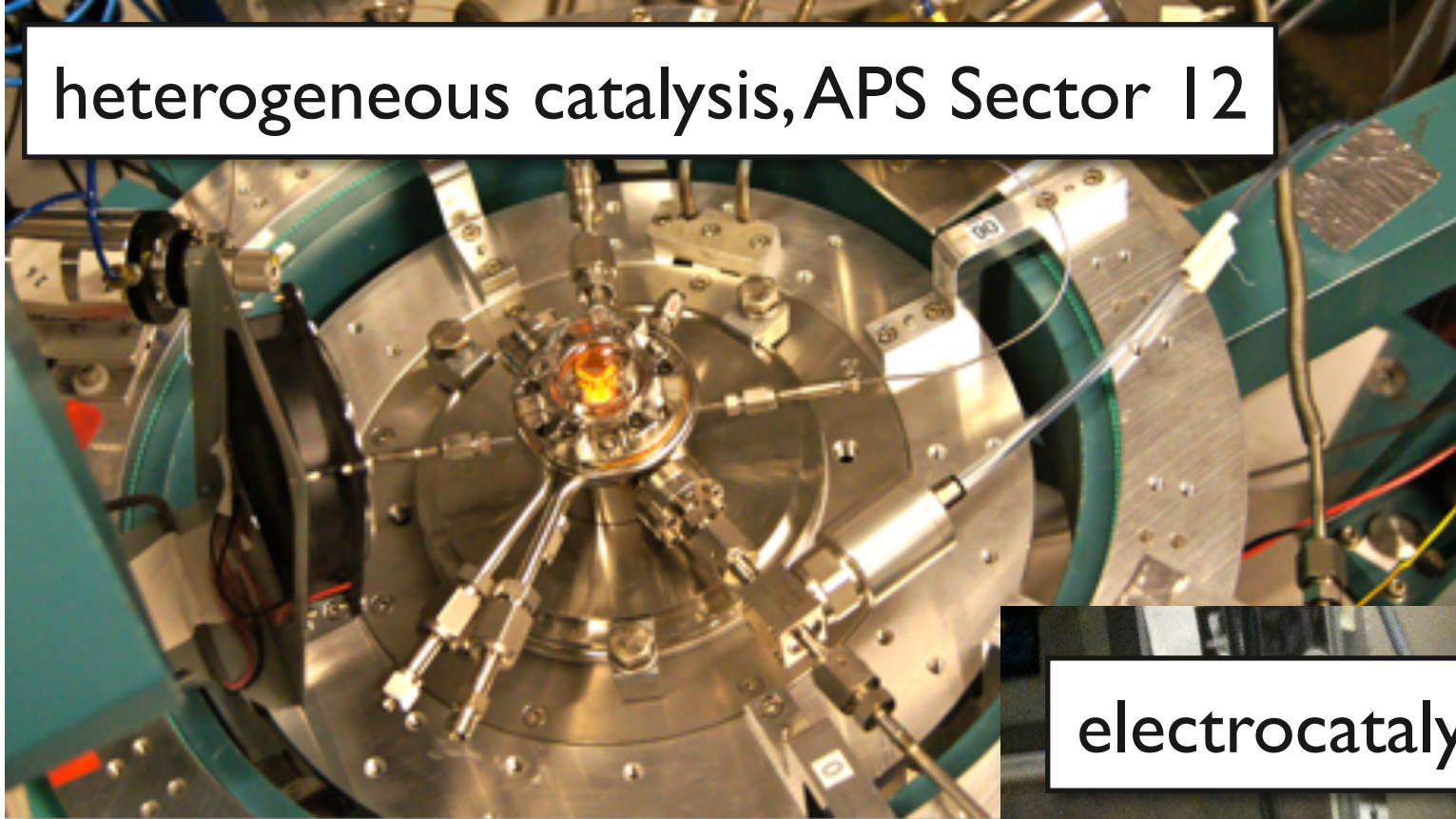


X. Yan et al. Adv. Mater. 34, 2200866 (2022)

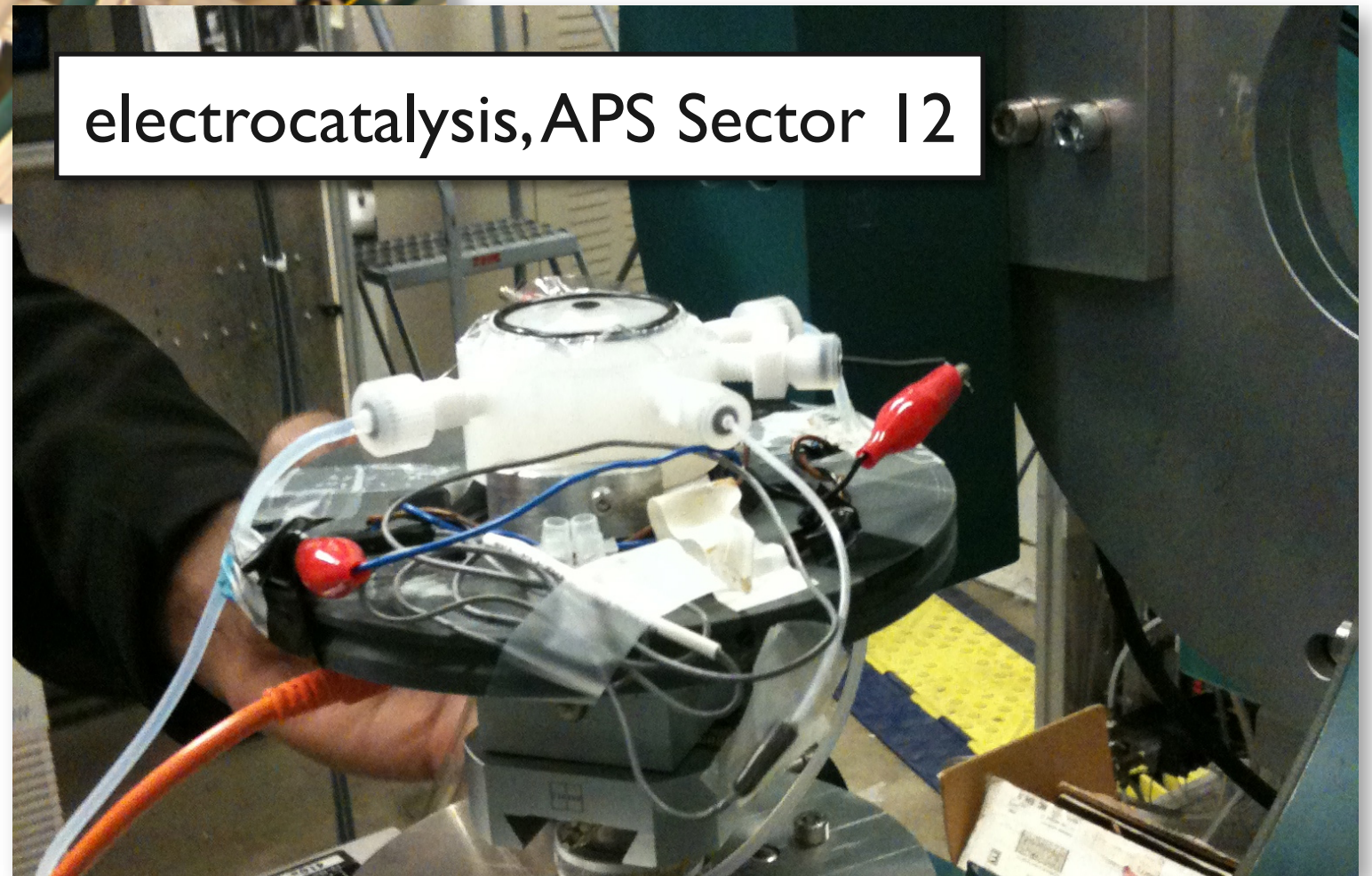


# Motivation: Watch surfaces during reaction

heterogeneous catalysis, APS Sector 12



electrocatalysis, APS Sector 12

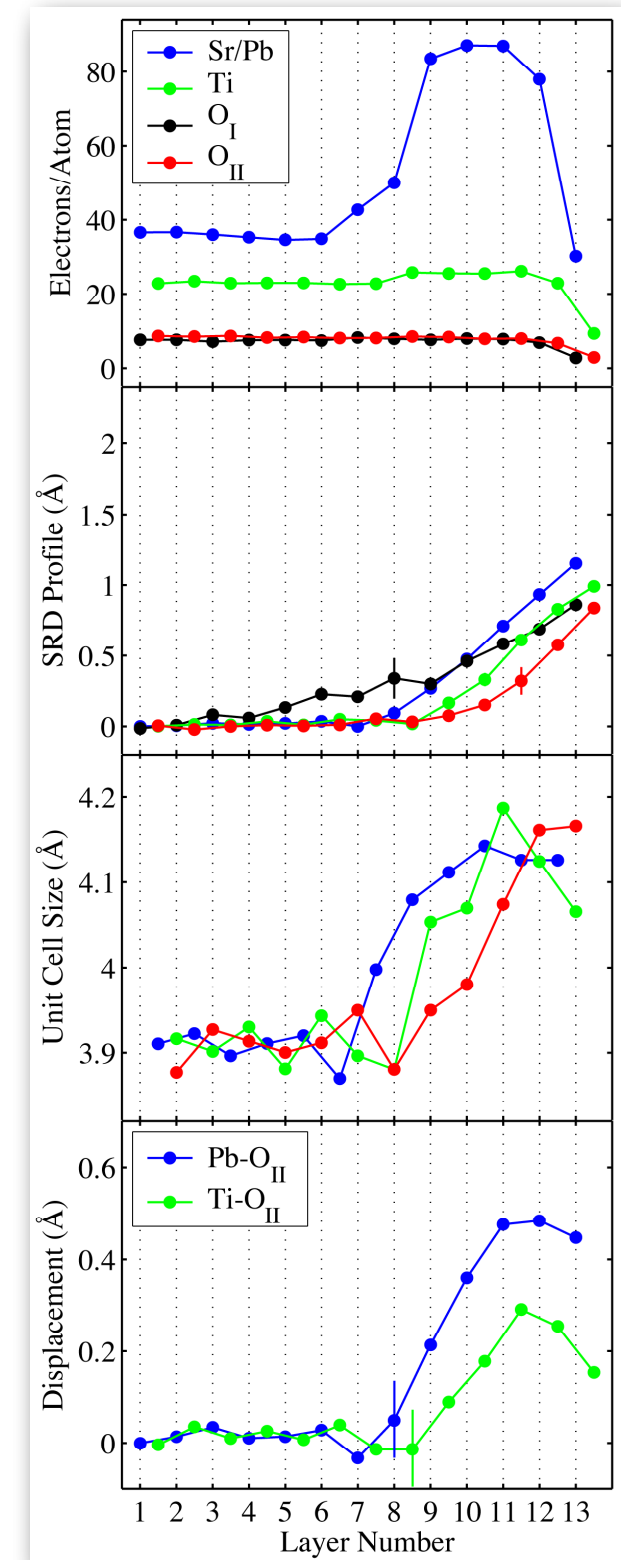
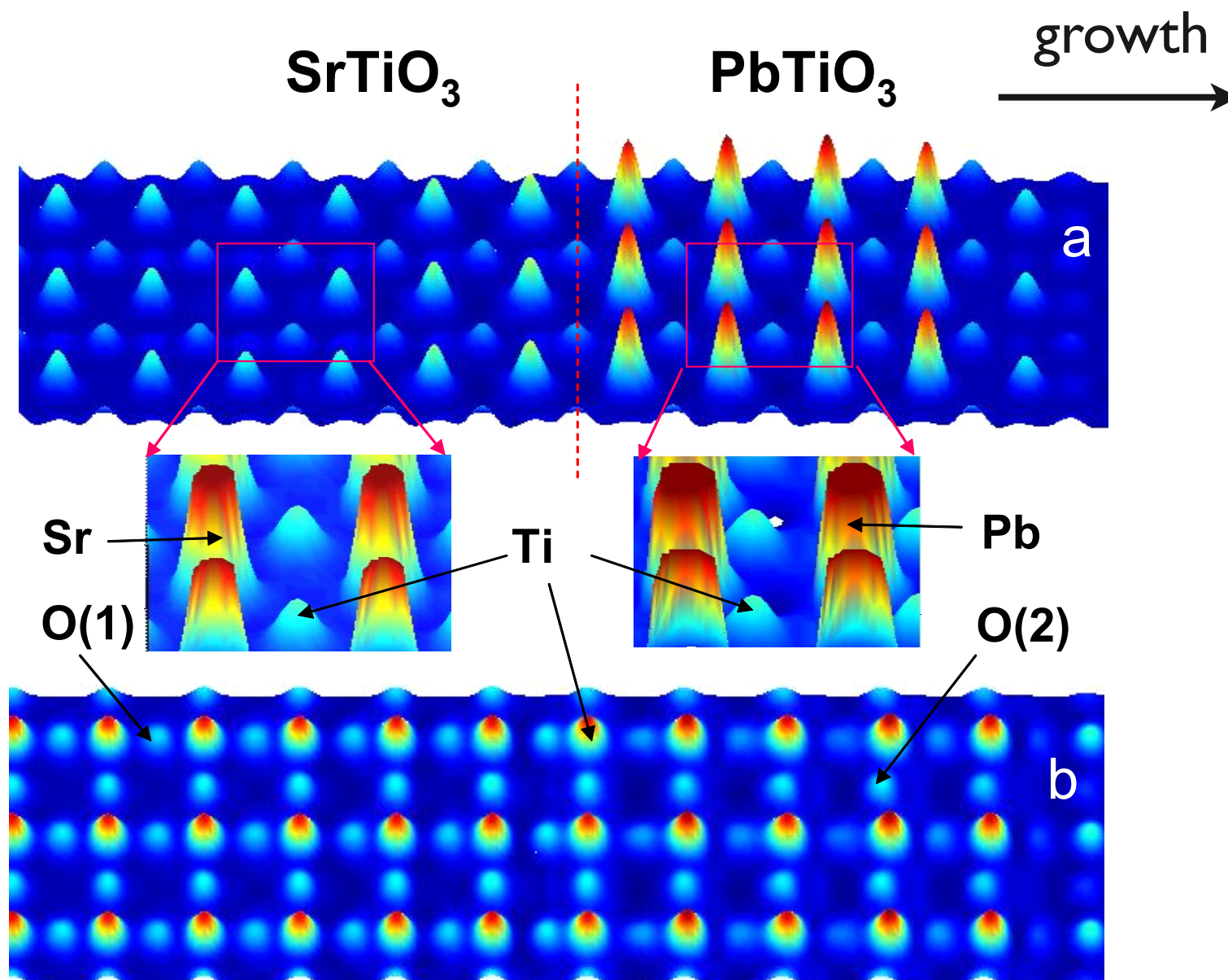




# Example from APS Sector 12

## PbTiO<sub>3</sub>/SrTiO<sub>3</sub> (001)

- can look at 3D atomic resolution structure (like TEM)
- but can look at non-destructively



D. D. Fong *et al.* Phys. Rev. B **71**, 144112 (2005)

## I. Surface X-ray Diffraction (SXRD)

- Modeling  $F(Q)$ 
  - *Structure factor for a crystal*
  - *Structure for a film / substrate*
    - Effect of roughness
  - *Fitting examples*
- **Why model? Can understand what SXRD is good for**
- **I will assume you are all working on epitaxial heterostructures...**

## II. Direct methods

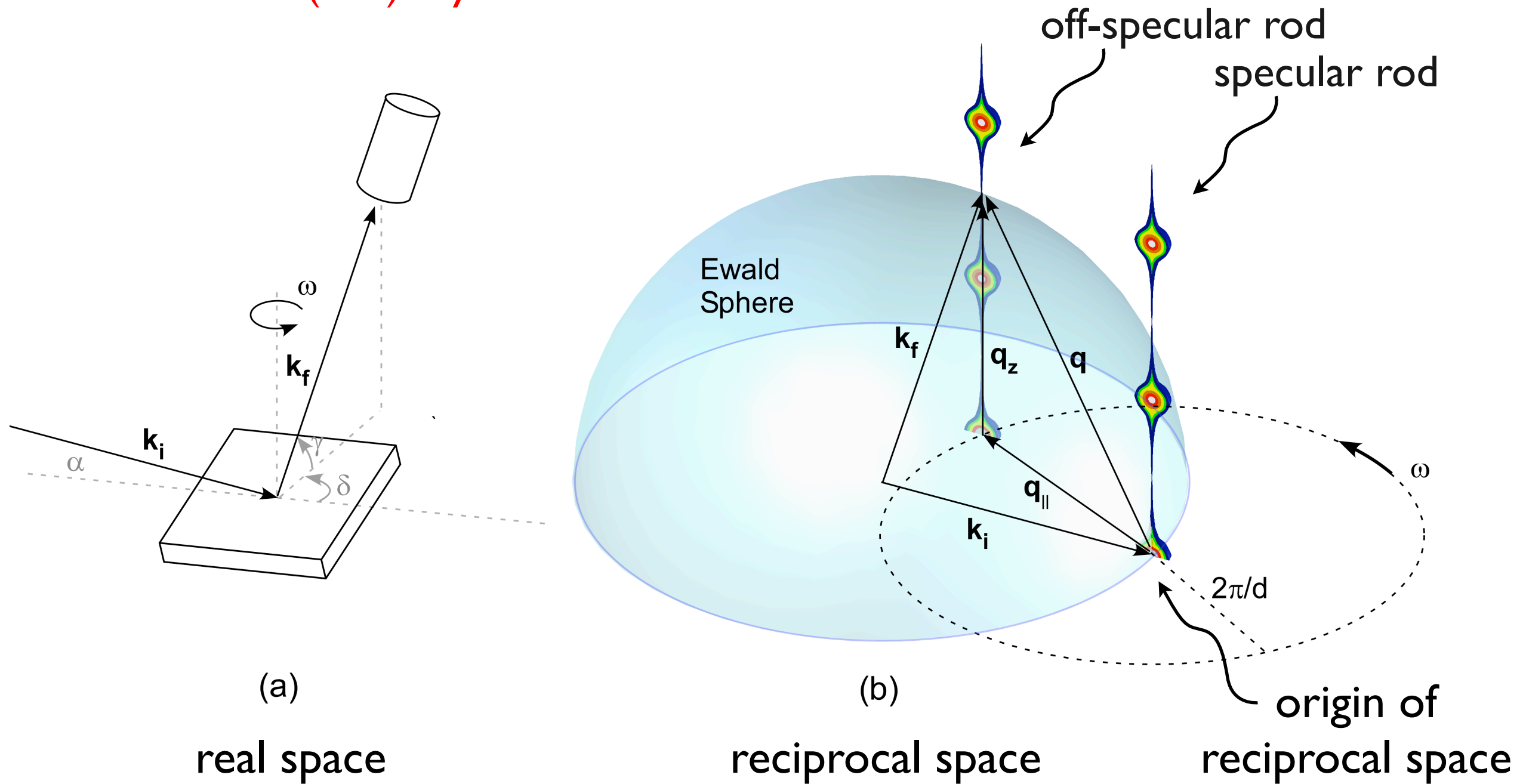
## III. Example results

## IV. Practicalities

## V. X-ray photon correlation spectroscopy (XPCS)

## SXRD geometry

I often work with (001) crystals



T.T. Fister & D. D. Fong in *Thin Film Metal-Oxides*, Springer (2010)



Modeling  $F(Q)$  for a CTREx.  $\text{PbTiO}_3 / \text{SrTiO}_3$  (001)

$$F_{\text{CTR}}(\mathbf{Q}) = N_1 N_2 F_{\text{column}}(\mathbf{Q})$$

$$F_{\text{column}}(\mathbf{Q}) = \sum_{n=0}^{\infty} F_n^{\text{unit cell}}(\mathbf{Q}) e^{-n(iQ_z d_n)}$$

= geometric series:  $a + ar + ar^2 + ar^3 + \dots$

Example geom series:  $\{1, 1/2, 1/4, 1/8, 1/16, 1/32, \dots\}$

What is the sum over the first 6 terms?

$a = 1$  (first term)

$r = 1/2$  (common ratio)

$N = 6$  terms

Useful formulas for CTRs:

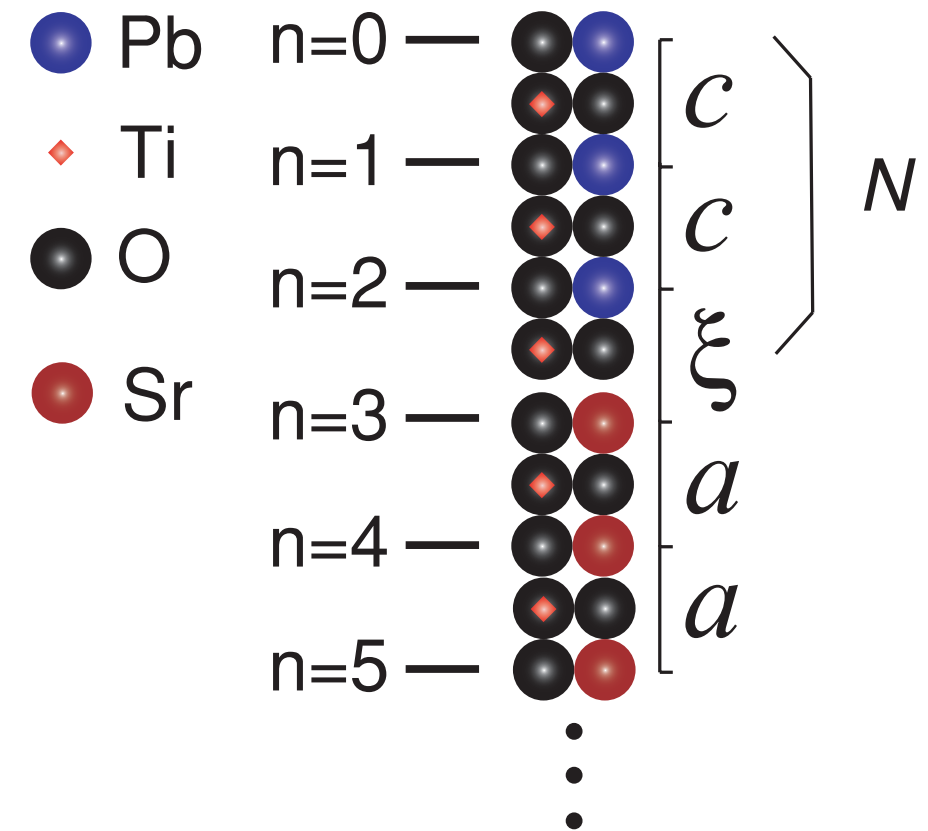
$$\sum_{n=0}^{N-1} ar^n = a \left( \frac{1 - r^N}{1 - r} \right)$$

$$= 1.96875$$

$$\sum_{n=0}^{\infty} ar^n = a \left( \frac{1}{1 - r} \right)$$

$$= 2$$

We will use both of these expressions for film and substrate

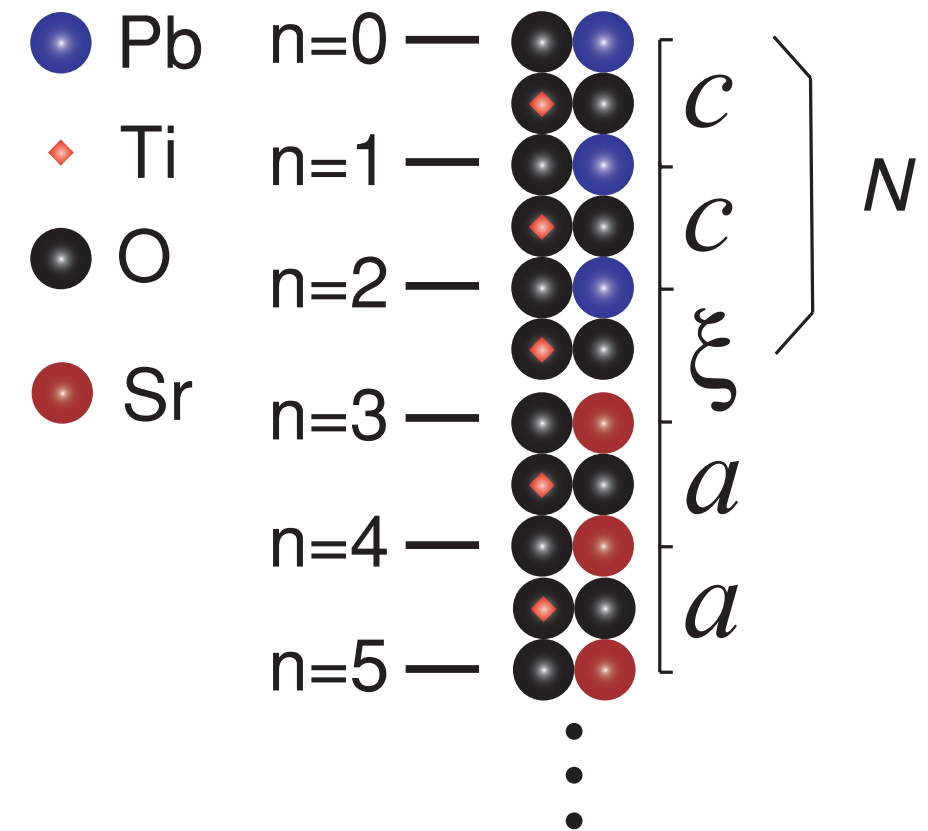


Modeling  $F(Q)$  for a CTREx.  $\text{PbTiO}_3 / \text{SrTiO}_3$  (001)

$$F_{\text{CTR}}(\mathbf{Q}) = N_1 N_2 F_{\text{column}}(\mathbf{Q})$$

$$F_{\text{column}}(\mathbf{Q}) = \sum_{n=0}^{\infty} F_n^{\text{unit cell}}(\mathbf{Q}) e^{-n(iQ_z d_n)}$$

= geometric series:  $a + ar + ar^2 + ar^3 + \dots$



film

$$a = F_{\text{film}}^{\text{unit cell}}$$

$$r = e^{-iQ_z c}$$

 $N = \text{number of film unit cells}$ 

substrate

$$a = F_{\text{sub}}^{\text{unit cell}}$$

$$r = e^{-iQ_z a}$$

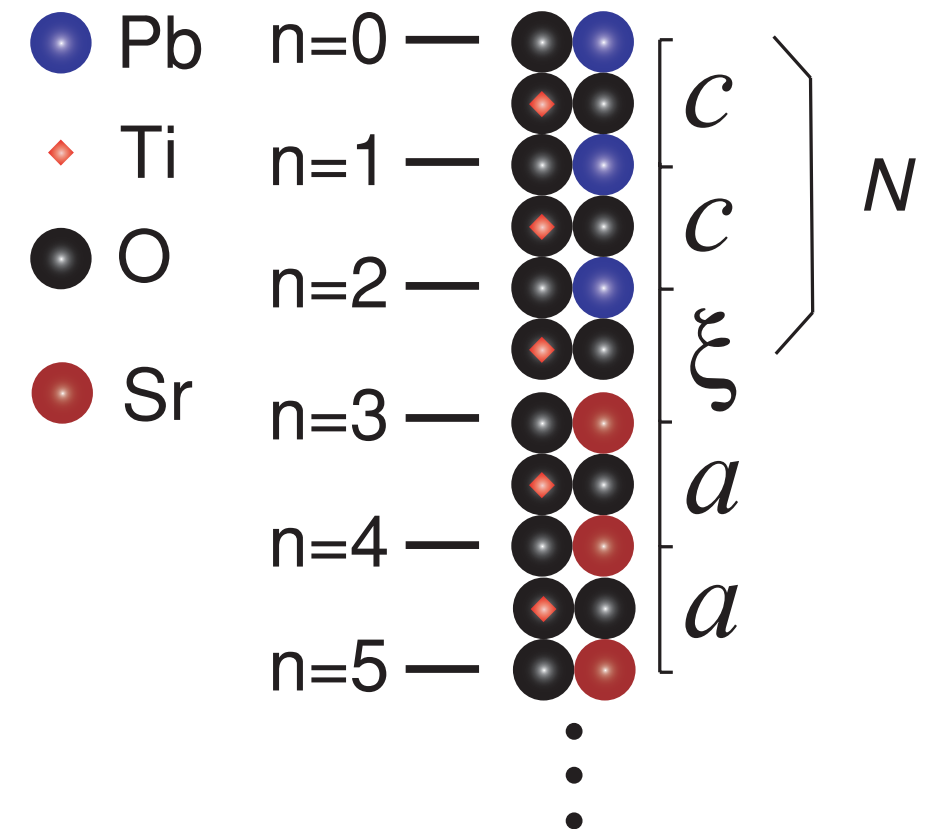
 $N = \infty$

Modeling  $F(Q)$  for a CTREx.  $\text{PbTiO}_3 / \text{SrTiO}_3$  (001)

$$F_{\text{CTR}}(\mathbf{Q}) = N_1 N_2 F_{\text{column}}(\mathbf{Q})$$

$$F_{\text{column}}(\mathbf{Q}) = \sum_{n=0}^{\infty} F_n^{\text{unit cell}}(\mathbf{Q}) e^{-n(iQ_z d_n)}$$

= geometric series:  $a + ar + ar^2 + ar^3 + \dots$



$$F_{\text{column}}(\mathbf{Q}) = F_{\text{PbTiO}_3}^{\text{unit cell}}(\mathbf{Q}) \left( \frac{1 - e^{-iNQ_z c}}{1 - e^{-iQ_z c}} \right) + e^{-iQ_z((N-1)c + \xi)} F_{\text{SrTiO}_3}^{\text{unit cell}}(\mathbf{Q}) \frac{1}{1 - e^{-iQ_z a}}$$

interface phase factor

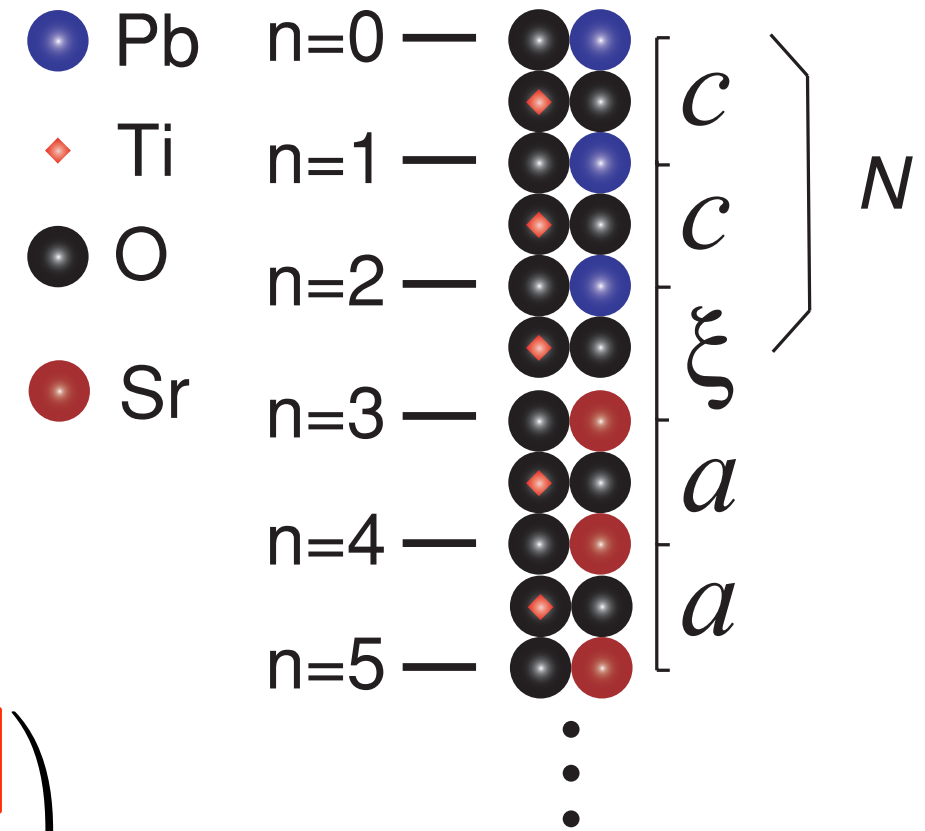
Modeling  $F(Q)$  for a CTR + absorptionEx.  $\text{PbTiO}_3 / \text{SrTiO}_3$  (001)

$$F_{\text{CTR}}(\mathbf{Q}) = N_1 N_2 F_{\text{column}}(\mathbf{Q})$$

$$F_{\text{column}}(\mathbf{Q}) = \sum_{n=0}^{\infty} F_n^{\text{unit cell}}(\mathbf{Q}) e^{-n(iQ_z d_n + \boxed{d_n / \zeta_n})}$$

absorption

$$F_{\text{column}}(\mathbf{Q}) = F_{\text{PbTiO}_3}^{\text{unit cell}}(\mathbf{Q}) \left( \frac{1 - e^{-iNQ_z c} \boxed{e^{-Nc / \zeta_{\text{PbTiO}_3}}}}{1 - e^{-iQ_z c} \boxed{e^{-c / \zeta_{\text{PbTiO}_3}}}} \right) + e^{-iQ_z((N-1)c + \xi)} \boxed{e^{-((N-1)c + \xi) / \zeta_{\text{PbTiO}_3}}} F_{\text{SrTiO}_3}^{\text{unit cell}}(\mathbf{Q}) \frac{1}{1 - e^{-iQ_z a} \boxed{e^{-a / \zeta_{\text{SrTiO}_3}}}}$$

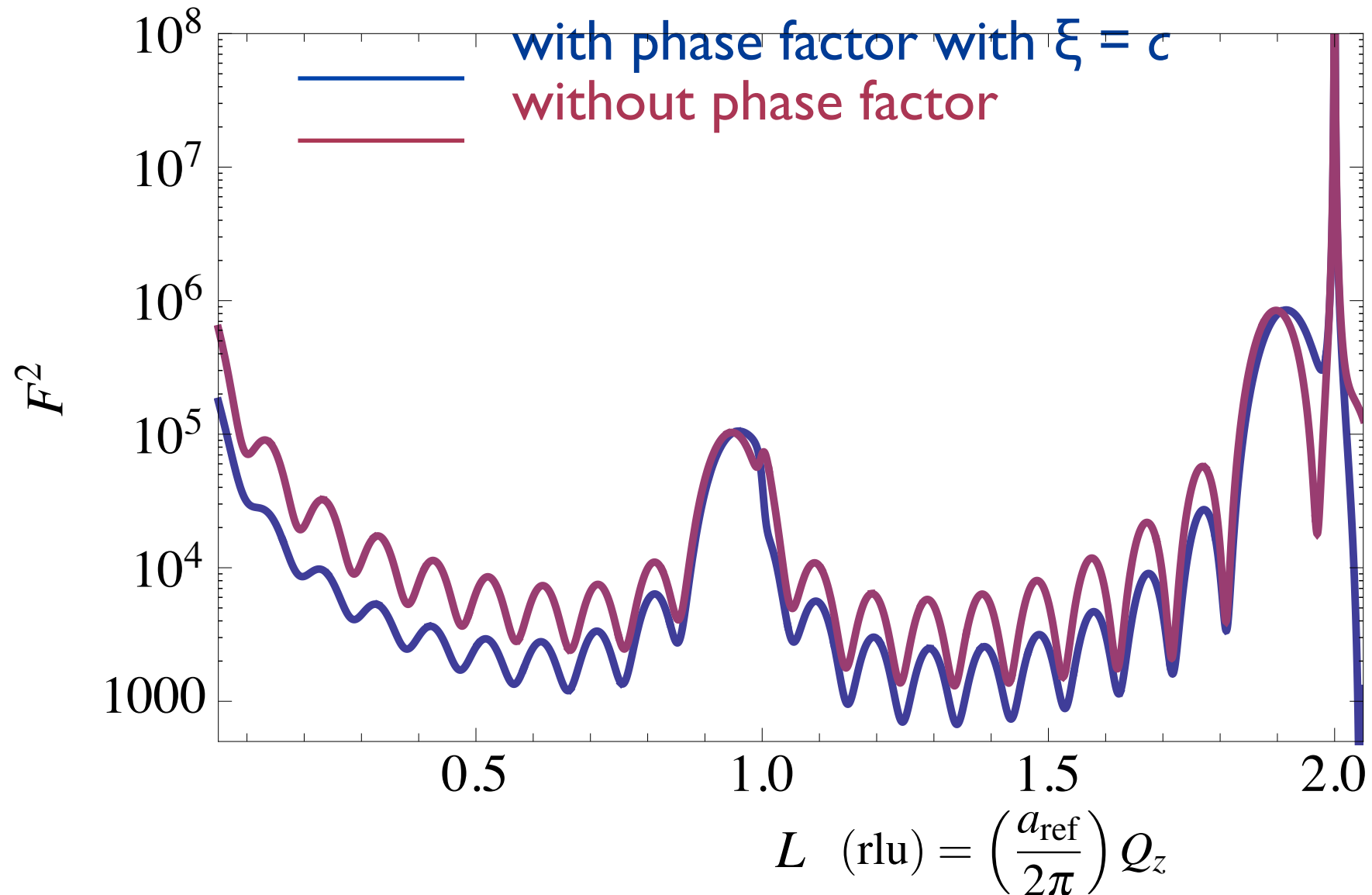
where  $\zeta_n = \lambda q_z / 4\pi \mu_n$

# Modeling $F(Q)$ for a CTR + absorption

Don't forget the interface phase factor

- Ex.  $\text{PbTiO}_3 / \text{SrTiO}_3$  (001)

~~$$F_{\text{column}}(\mathbf{Q}) = F_{\text{PbTiO}_3}^{\text{unit cell}}(\mathbf{Q}) \left( \frac{1 - e^{-iN\mathbf{Q}_z c}}{1 - e^{-i\mathbf{Q}_z c}} \right) + F_{\text{SrTiO}_3}^{\text{unit cell}}(\mathbf{Q}) \frac{1}{1 - e^{-i\mathbf{Q}_z a}}$$~~



$$\text{thickness} = \frac{a_{\text{ref}}}{\Delta_{\text{minima}}} \sim \frac{a_{\text{ref}}}{\text{FWHM}_{\text{Bragg}}}$$

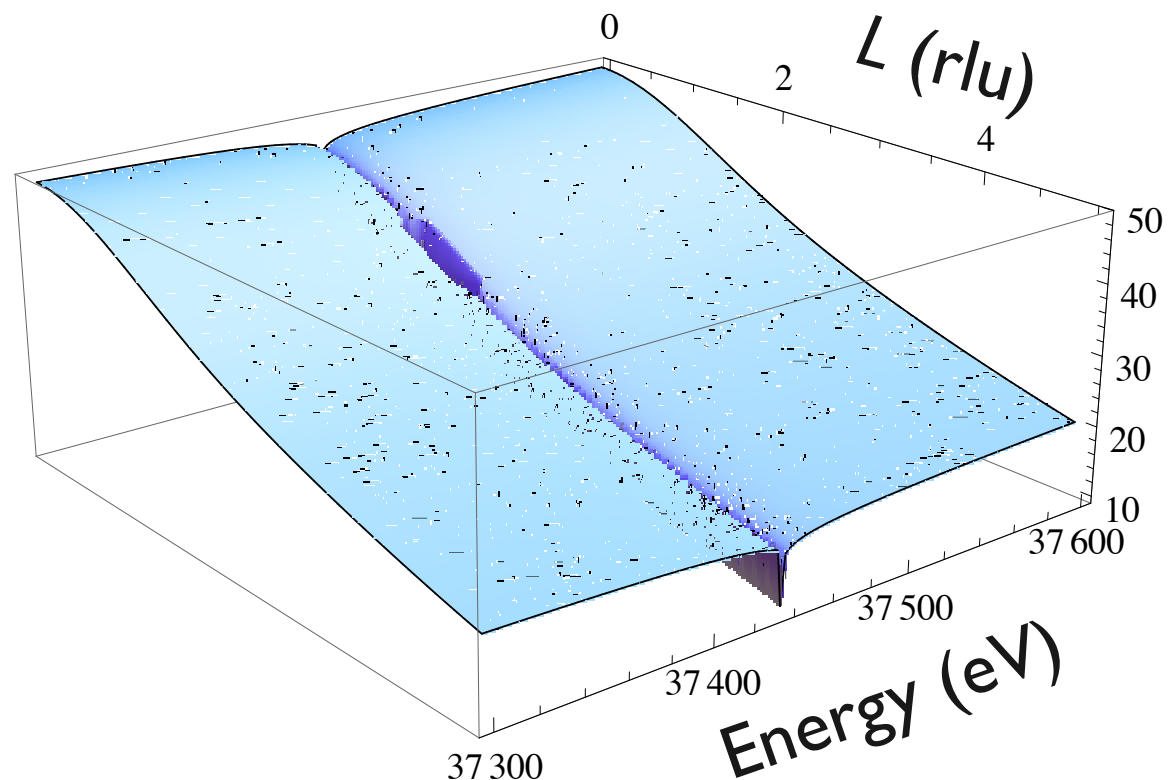
# Modeling $F(Q)$ for a CTR + temperature effects + X-ray energy effects

Unit cell structure factor:

$$F_{\text{PbTiO}_3}^{\text{unit cell}}(\mathbf{Q}) =$$

$$\sum_{j=1}^{N_{uc}} f_j(Q) \overset{\text{DW factor}}{e^{-B_j(Q/4\pi)^2}} e^{i\mathbf{Q}\cdot\mathbf{R}_j}$$

Atomic form factor:



$$=$$

$$+ f_{\text{O}(1)}(Q) e^{-B_{\text{O}(1)}(Q/4\pi)^2}$$

$$+ f_{\text{O}(2)}(Q) e^{-B_{\text{O}(2)}(Q/4\pi)^2} e^{iQ_y a/2} e^{iQ_z(\pm\delta z_{\text{O}(2)} - c/2)}$$

$$+ f_{\text{O}(2)}(Q) e^{-B_{\text{O}(2)}(Q/4\pi)^2} e^{iQ_x a/2} e^{iQ_y a/2} e^{iQ_z(\pm\delta z_{\text{O}(2)} - c/2)}$$

$$+ f_{\text{Ti}}(Q) e^{-B_{\text{Ti}}(Q/4\pi)^2} e^{iQ_z(\pm\delta z_{\text{Ti}} - c/2)}$$

$$+ f_{\text{Pb}}(Q) e^{-B_{\text{Pb}}(Q/4\pi)^2} e^{iQ_x a/2} e^{iQ_y a/2} e^{iQ_z(\pm\delta z_{\text{Pb}})}$$

$\text{Re}(f_{\text{Ba}})$

$$f(Q, E) = f_0(Q) + f'(E) + i f''(E)$$

see f0\_WaasKirf.dat

- based on Waasmaier-Kirfel model:

D. Waasmaier & A. Kirfel, Acta Cryst. **A51**,  
416-413 (1995).

see [http://henke.lbl.gov/optical\\_constants/sf/sf.tar.gz](http://henke.lbl.gov/optical_constants/sf/sf.tar.gz), from D.T. Cromer & D. Liberman, Acta Cryst. **A37**, 267 (1981)  
or <http://www.tagen.tohoku.ac.jp/general/building/iamp/database/scm/AXS/> from Y. Waseda, Novel Application of Anomalous (Resonance) X-ray Scattering for Structural Characterization of Disordered Materials. New York. Springer. 1984

# Modeling $F(Q)$ for a CTR + temperature effects

## Debye-Waller factors

- need to look up in the literature
  - e.g., *isotropic Debye Waller factors*

**Table 5.** Calculated temperature factors  $B(\kappa)$ ,  $\text{\AA}^2$ , for models 4, 5 and 6 compared with experimentally determined values for  $\text{BaTiO}_3$ .

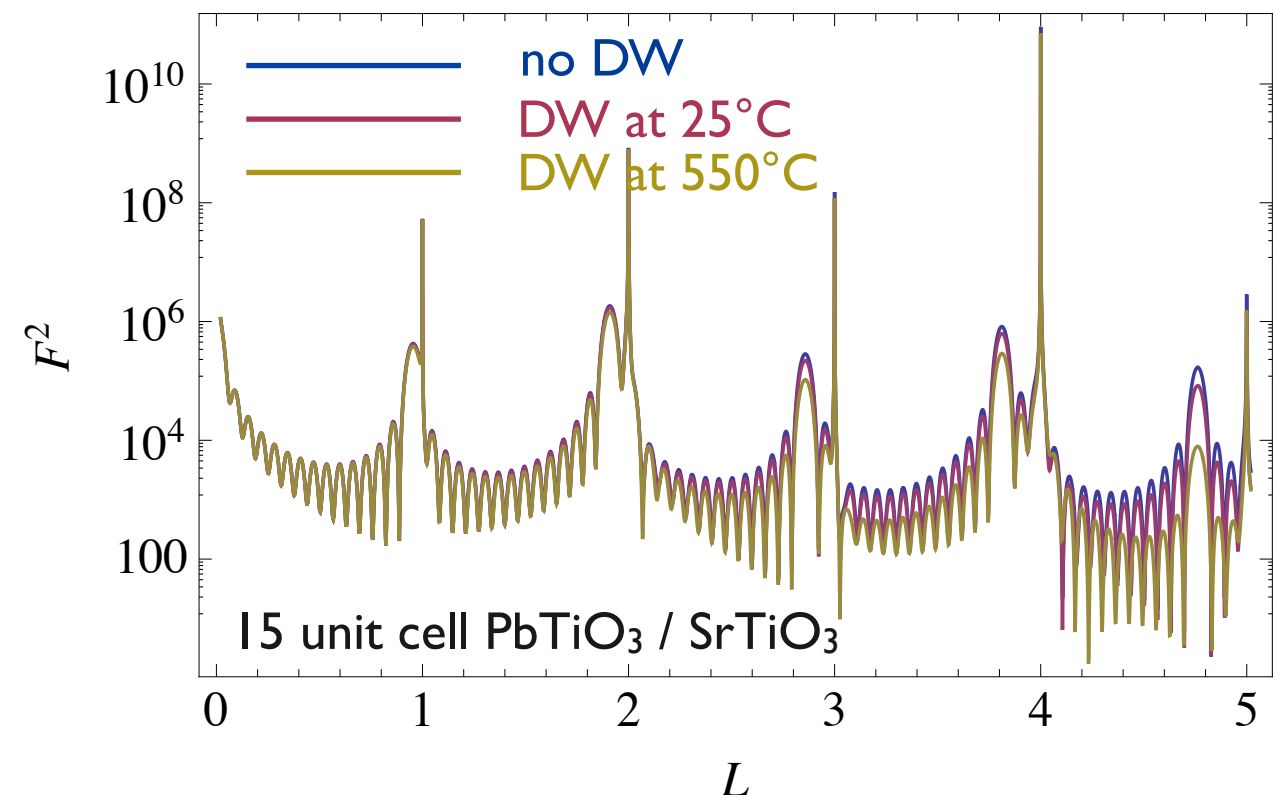
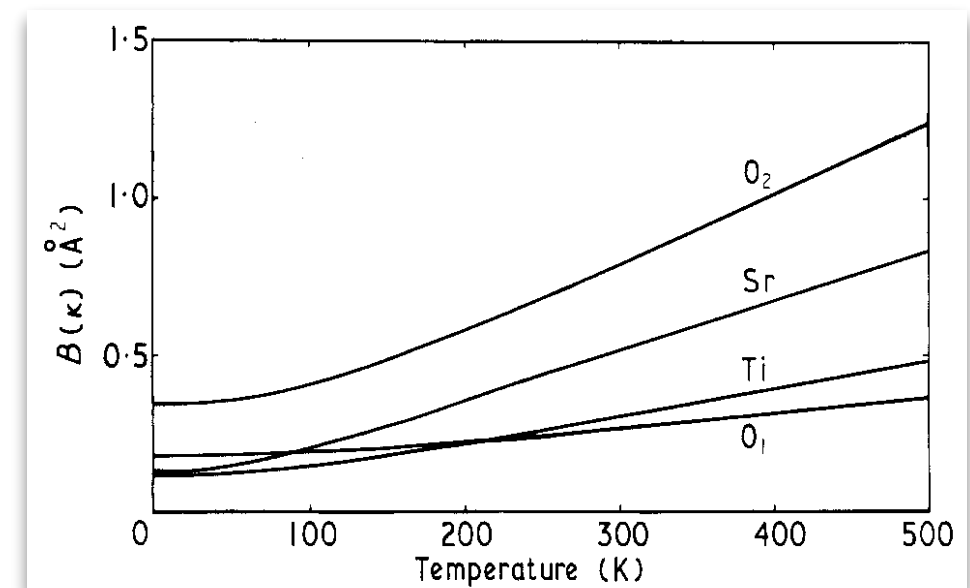
Temperature (K)	Model	$B(\text{Sr})$	$B(\text{Ti})$	$B(\text{O}_1)$	$B(\text{O}_2)$
100	4 (90)	0.199	0.135	0.194	0.402
	5 (90)	0.208	0.155	0.185	0.397
	6 (90)	0.228	0.194	0.195	0.399
300	4 (297)	0.492	0.251	0.278	0.807
	5 (297)	0.511	0.303	0.258	0.790
	6 (297)	0.526	0.352	0.275	0.783

for  $\text{SrTiO}_3$ : W. G. Stirling, *J. Phys. C* **5**, 2711 (1972)

**Table 2.** Summary of parameters refined at all temperatures (Pb at origin)

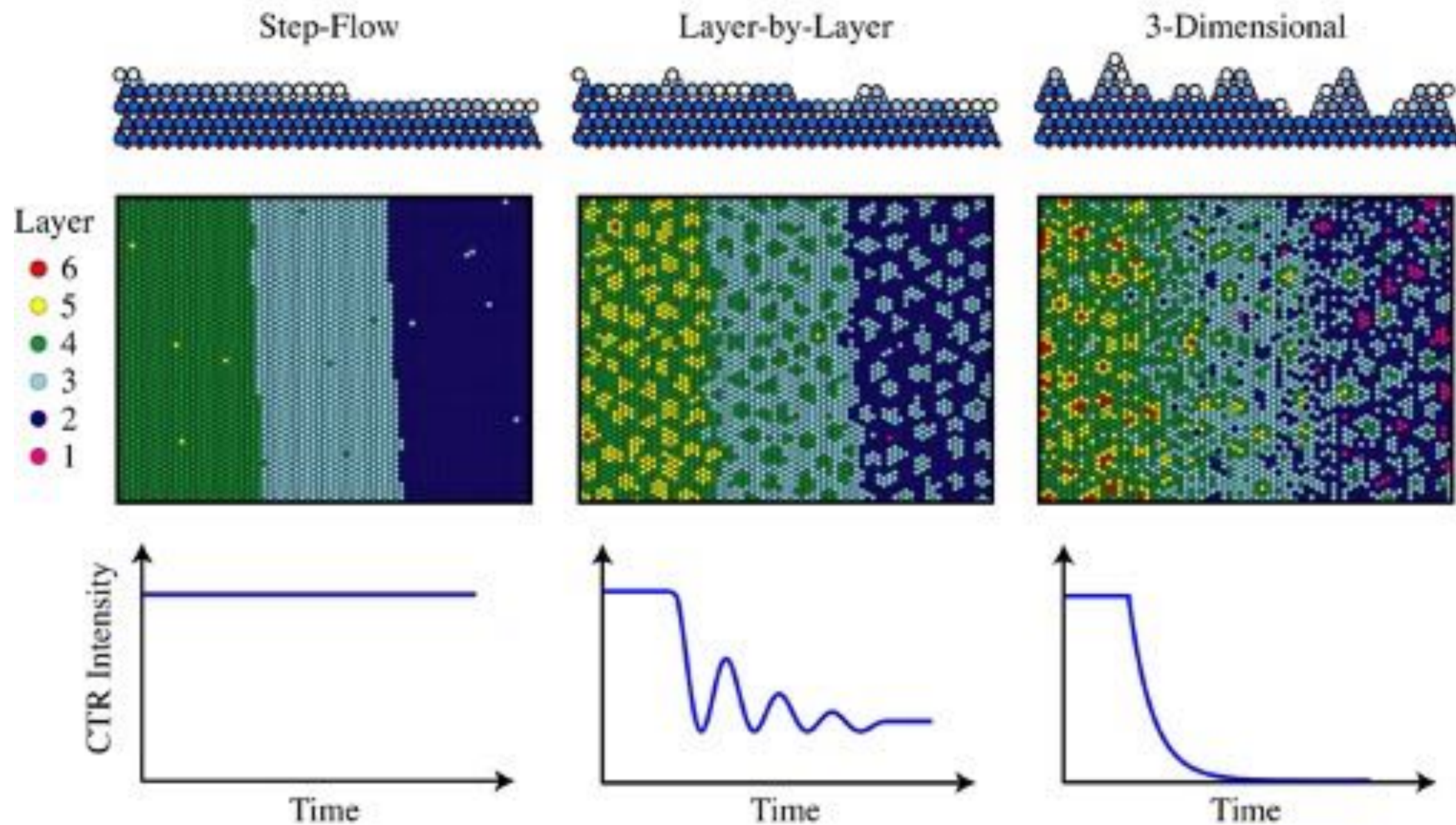
	-183°C	-115°C	25°C	550°C
Isotropic temperature factor refinement				
$\delta z_{\text{Ti}}(\text{\AA})$	0.167	0.171	0.162	0
$\delta z_{\text{O}(1)}(\text{\AA})$	0.492	0.479	0.473	0
$\delta z_{\text{O}(2)}(\text{\AA})$	0.505	0.504	0.486	0
$B(\text{Pb})$	0.378 (100)	0.757 (84)	0.706 (89)	2.711 (167)
$B(\text{Ti})$	0.284 (215)	0.364 (187)	0.060 (170)	0.694 (225)
$B[\text{O}(1)]$	0.670 (140)	0.713 (123)	0.351 (117)	1.549 (102)
$B[\text{O}(2)]$	0.498 (98)	0.862 (85)	0.477 (75)	$B[\text{O}(1)]$
$R_{\text{nuc}}$	5.22	5.90	4.35	3.10
$R_{\text{prof}}$	12.47	12.21	10.19	12.07
$R_w$	15.20	15.87	12.83	16.57

for  $\text{PbTiO}_3$ : A. M. Glazer & S.A. Mabud, *Acta Cryst. B* **34**, 1065 (1978)





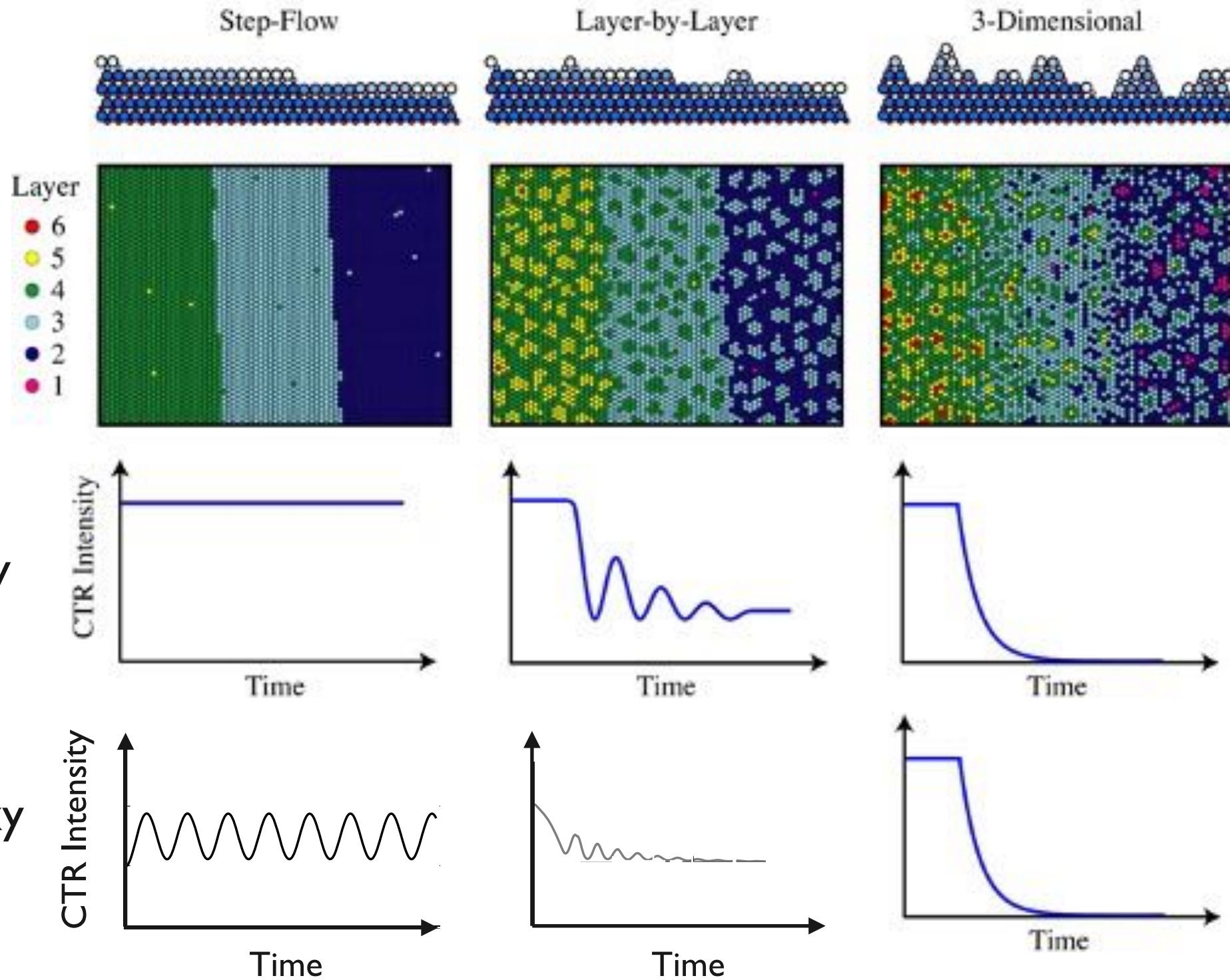
# Watching @ 0 0 1/2 during homoepitaxy



- ★ Layer-by-layer growth: CTR intensity oscillates as individual monolayers nucleate and coalesce



# Homoepitaxy vs heteroepitaxy

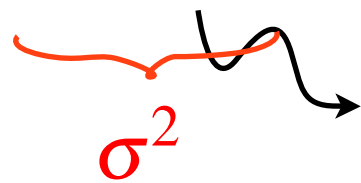


# Modeling $F(Q)$ for a CTR + continuous roughness

## Continuous roughness

- Gaussian distribution of step heights about a mean surface

$$R^2 = e^{-4\pi^2 \langle \Delta p^2 \rangle (Q_z - Q_B)^2}$$



mean square deviation of step heights in units of the lattice spacing

$$I(Q) = R^2(Q)I_0(Q)$$

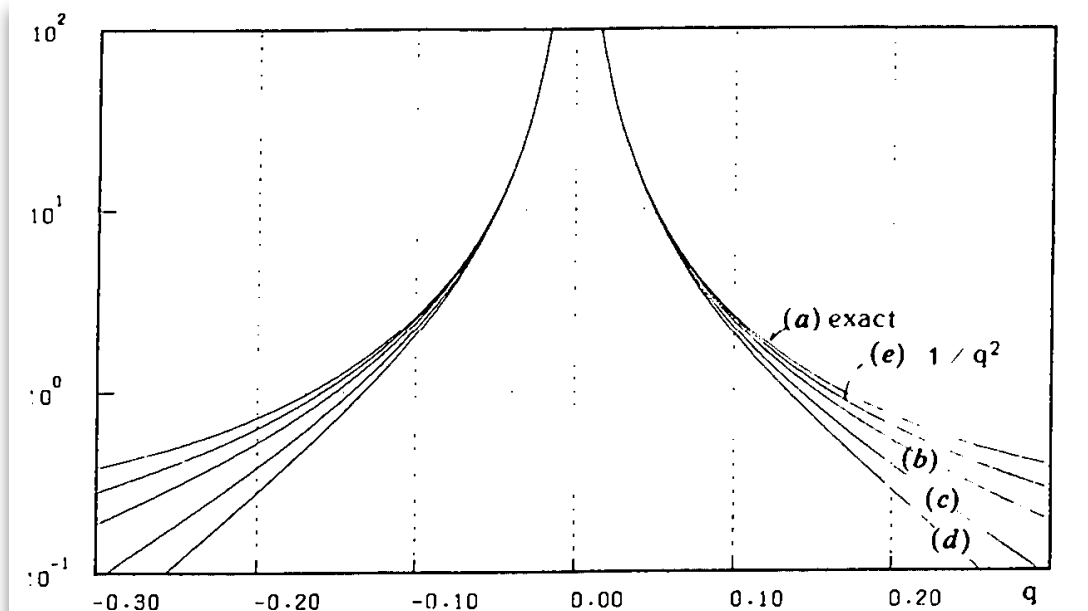
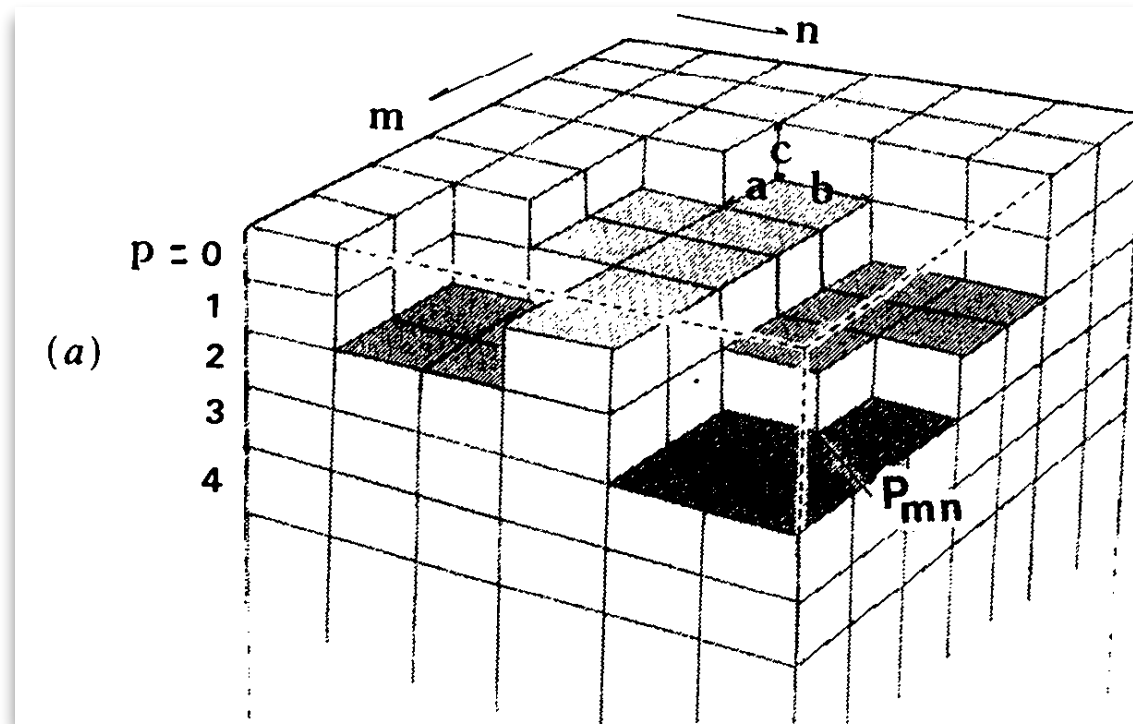


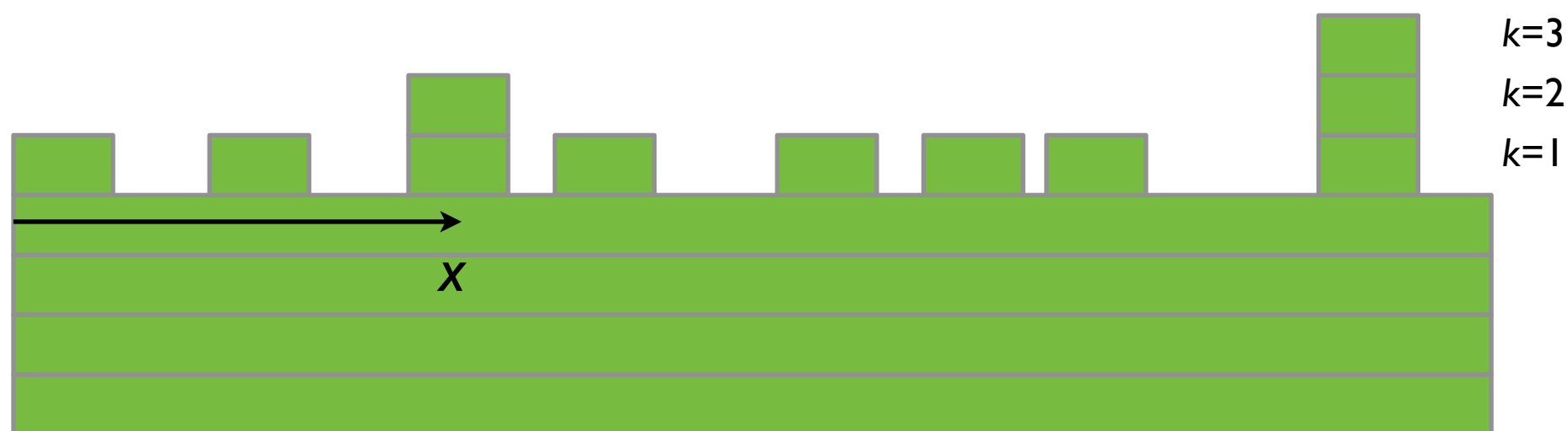
Fig. 6. Intensity change of the CTR scattering along the rod for several different degrees of surface roughness. (a) Ideal flat surface; (b), (c) and (d) rough surfaces with  $\langle \Delta p^2 \rangle = 0.2, 0.4$  and  $0.6$  in Debye-Waller-like factor, respectively; (e) the  $1/q^2$  relation, showing its deviation from the exact calculation (a) for the ideally flat surface.

J. Harada, Acta Cryst. A **48**, 764 (1992)

# Modeling $F(Q)$ for a CTR + continuous + discrete roughness

## Discrete roughness - more general

- can account for non-Gaussian thickness non-uniformity (e.g., bimodal distribution)
  - e.g., in PLD, for  $n$  pulses of (random) growth



Probability of getting exactly  $k$  layers to grow at unit cell position  $x$  after  $n$  pulses, with each pulse resulting in a coverage of  $p$  (i.e., binomial distribution)

$$P(X = k) = \binom{n}{k} p^k (1 - p)^{(n-k)} \quad \text{where} \quad \binom{n}{k} = \frac{n!}{k!(n-k)!}$$

in our language

$p = \text{coverage}, \theta$

$n = \sigma_d^2 / (c^2 \theta(1-\theta))$

$$R^2 = \left[ 1 - 4\theta(1-\theta) \sin^2(\pi L) \right]^{\frac{\sigma_d^2}{c^2 \theta(1-\theta)}}$$

D. Dale et al., Phys. Rev. B **74**, 085419 (2006)

# Modeling roughness during heteroepitaxial growth

Good for modeling thin film growth & roughness evolution ( $\theta$ =fraction covered)

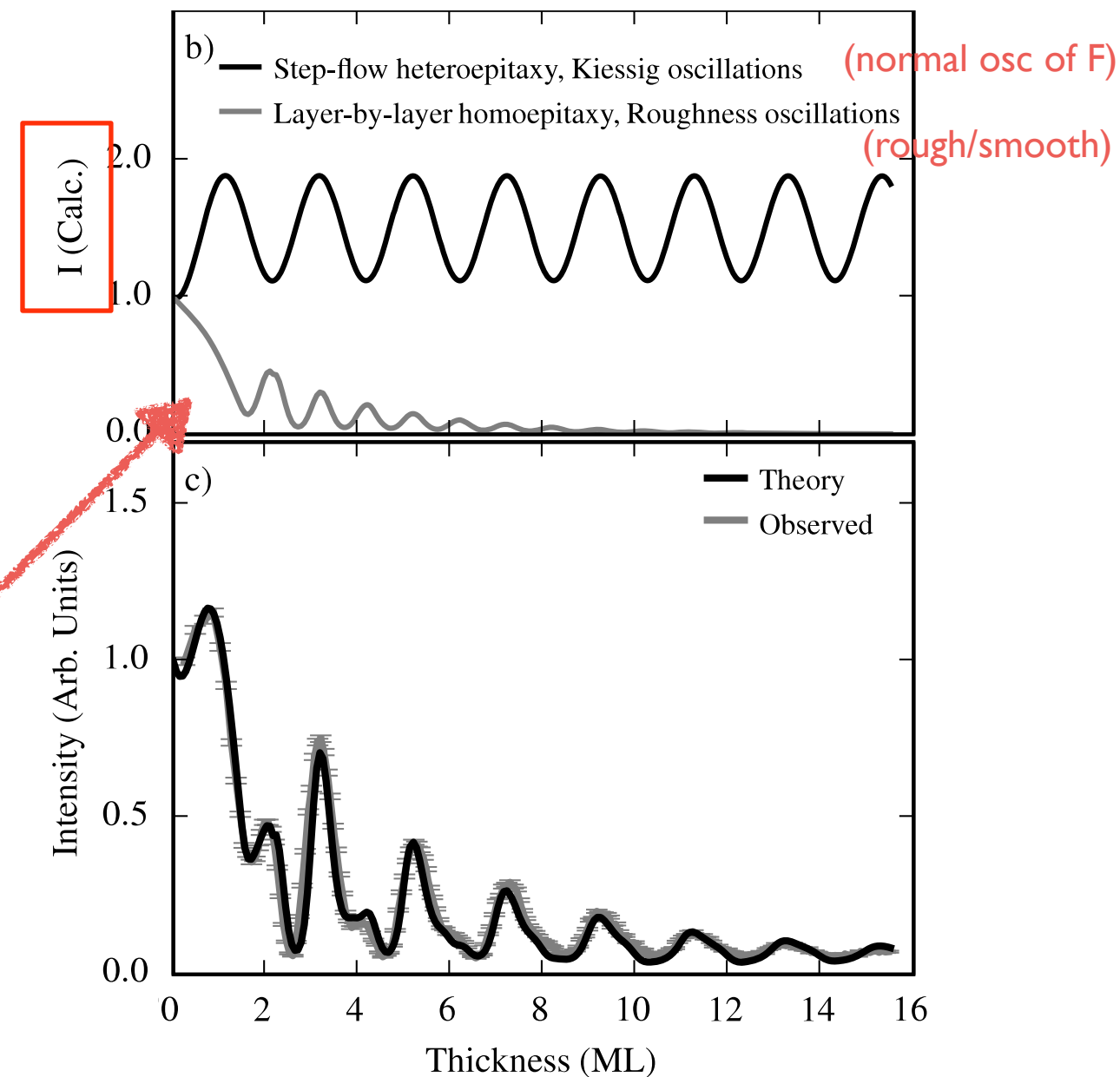
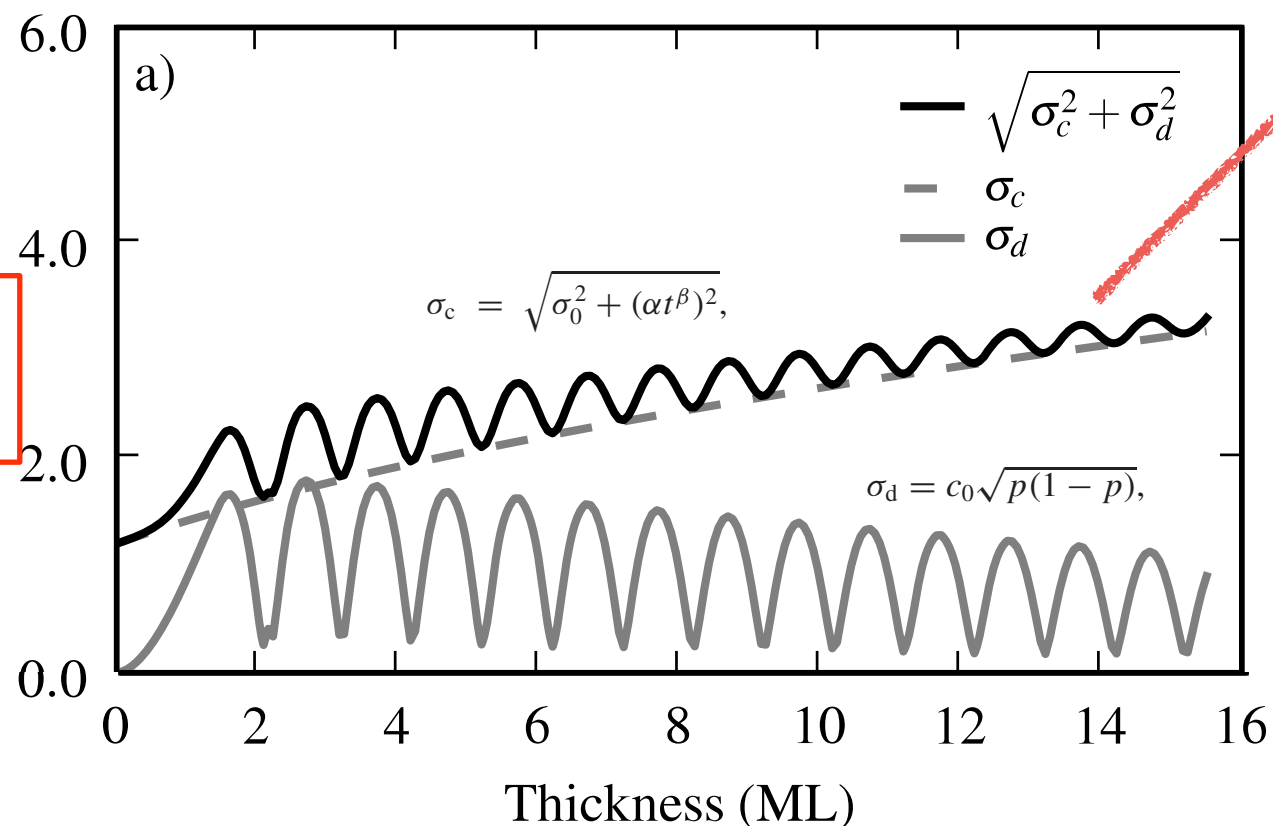
@ 0 0 1/2

$$\sigma_{\text{total}} = \sqrt{\sigma_{\text{continuous}}^2 + \sigma_{\text{discrete}}^2} \quad \text{becomes}$$

$$R(Q)^2 = e^{-\frac{4\sigma_c^2}{a^2} \sin^2(Q_z a/2)} \left[ 1 - 4\theta(1-\theta) \sin^2(\pi L) \right] \frac{\sigma_d^2}{c^2 \theta(1-\theta)}$$

$$I(Q) = R^2(Q) I_0(Q)$$

## Growth of LSMO/STO(001) by PLD



You can separate continuous vs discrete roughness components

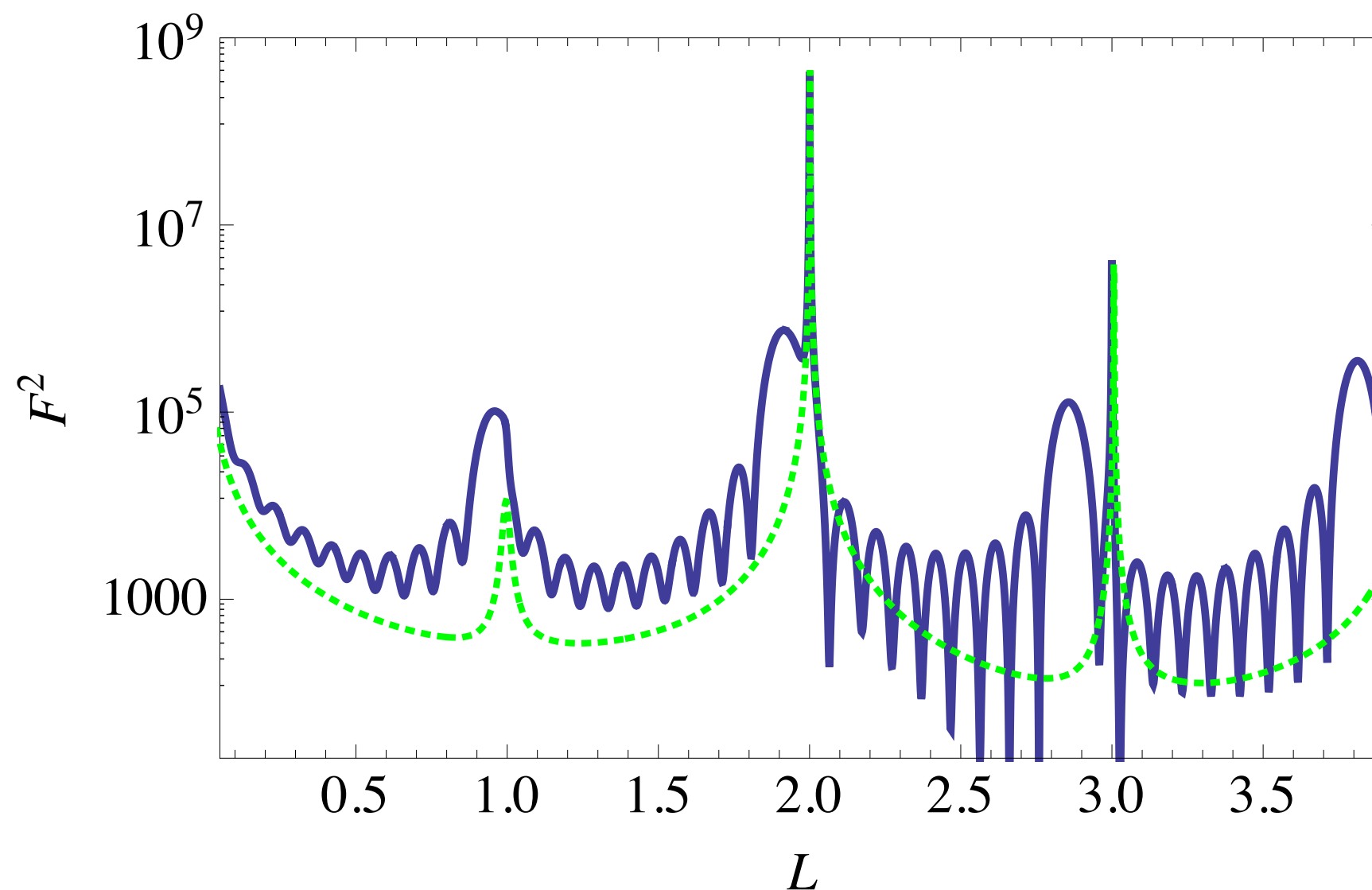
D. Dale et al., J. Phys: Condens. Matter **20**, 264008 (2008)

# Example calculations

## Thickness fringes - compare to STO (green)

- changes in electron density and/or lattice parameter

10uc PTO/STO with  $c_{\text{film}}=4.1 \text{ \AA}$ ,  $a_{\text{sub}}=3.905 \text{ \AA}$ ,  $\xi = 3.905 \text{ \AA}$  (both  $\rho$  and  $c$ )





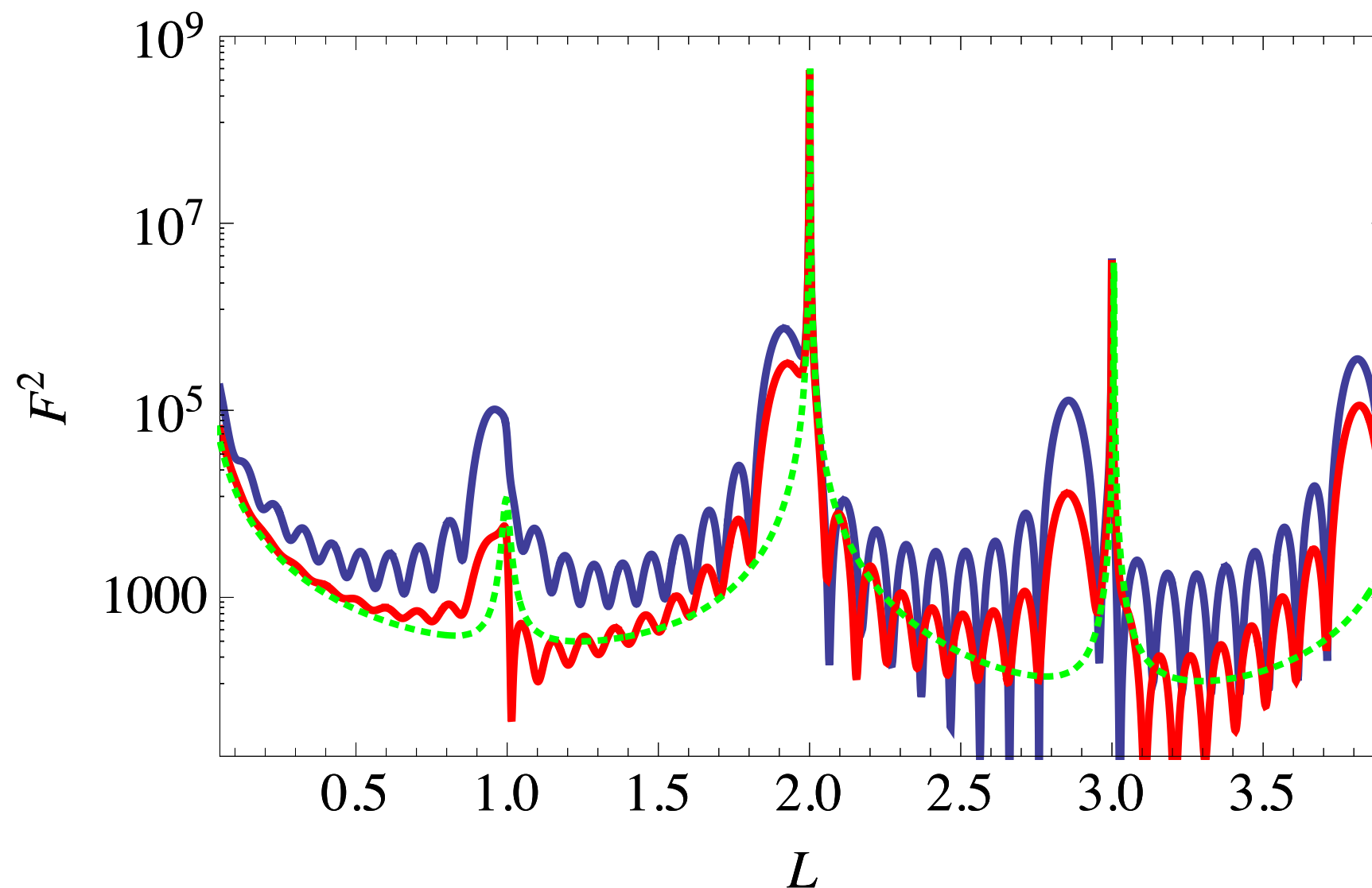
# Example calculations

## Thickness fringes - compare to STO (green)

- changes in electron density and/or lattice parameter

10uc PTO/STO with  $c_{\text{film}}=4.1 \text{ \AA}$ ,  $a_{\text{sub}}=3.905 \text{ \AA}$ ,  $\xi = 3.905 \text{ \AA}$  (both  $\Delta\rho$  and  $\Delta c$ )

10uc STO/STO with  $c_{\text{film}}=4.1 \text{ \AA}$ ,  $a_{\text{sub}}=3.905 \text{ \AA}$ ,  $\xi = 3.905 \text{ \AA}$  (just  $\Delta c$ )

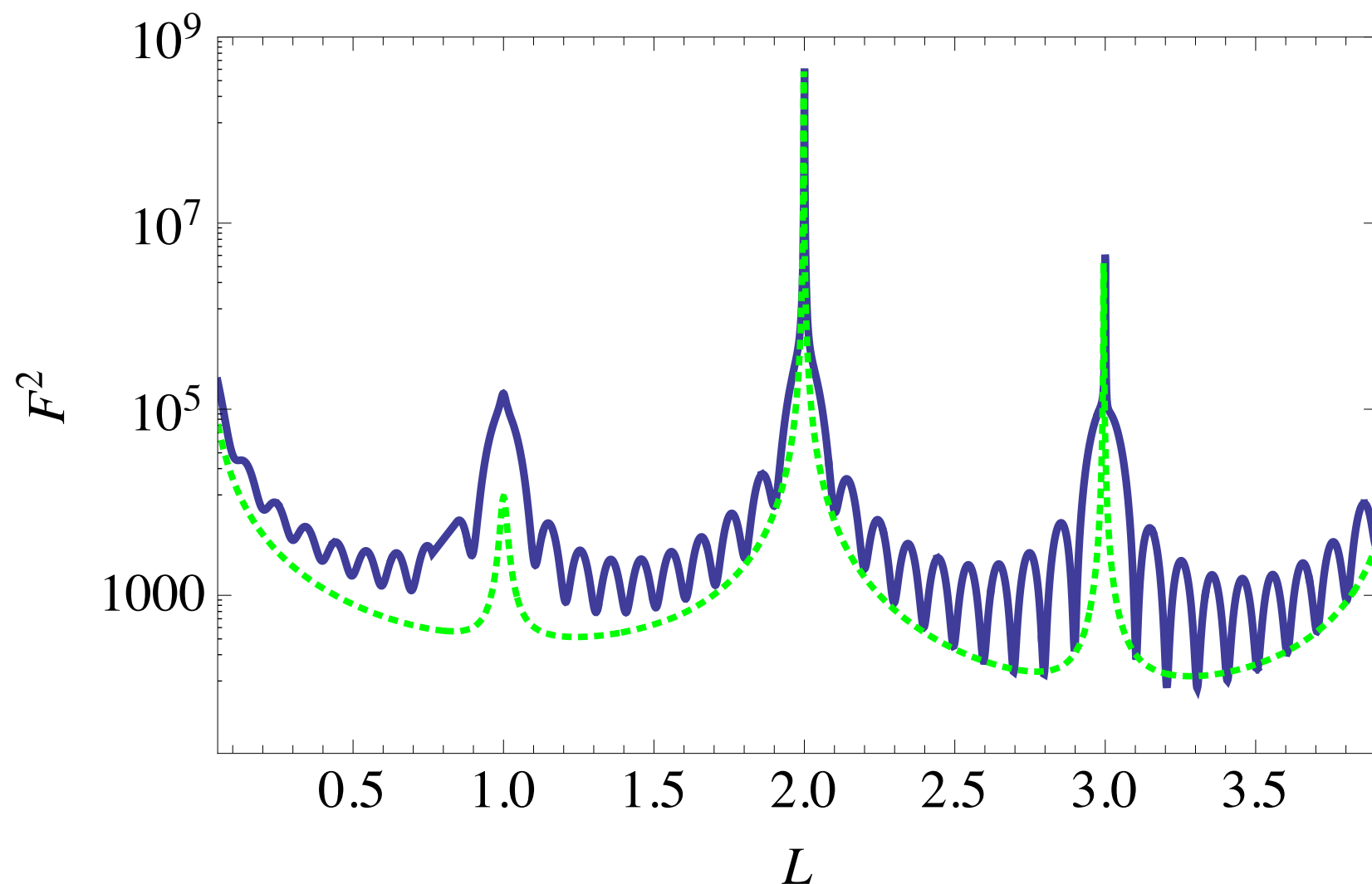


## Example calculations

Thickness fringes - compare to STO (green)

- changes in electron density and/or lattice parameter

10uc PTO/STO with  $c_{\text{film}}=3.905 \text{ \AA}$ ,  $a_{\text{sub}}=3.905 \text{ \AA}$ ,  $\xi = 3.905 \text{ \AA}$  (just  $\Delta\rho$ )



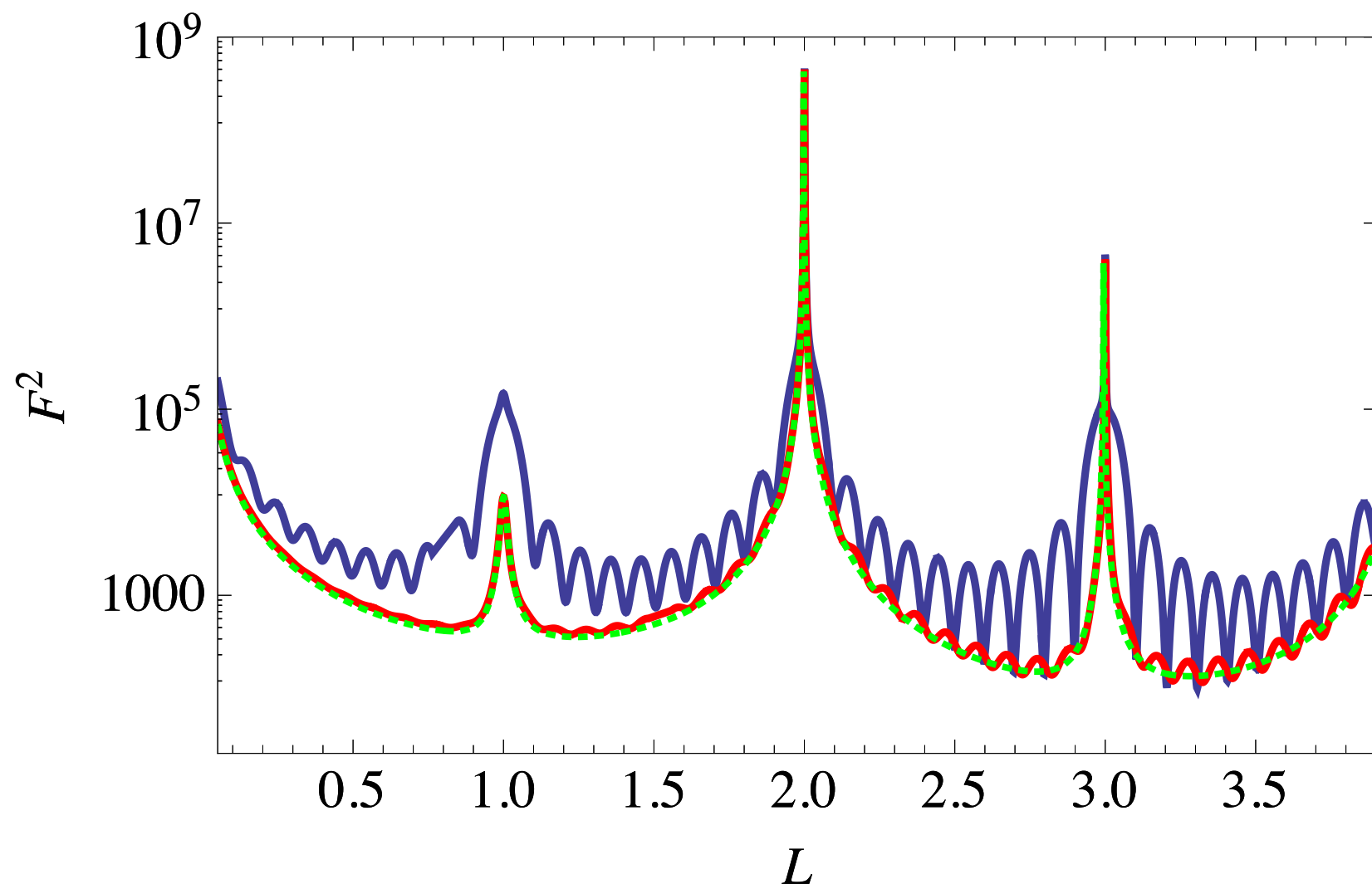
# Example calculations

## Thickness fringes - compare to STO (green)

- changes in electron density and/or lattice parameter

10uc PTO/STO with  $c_{\text{film}}=3.905 \text{ \AA}$ ,  $a_{\text{sub}}=3.905 \text{ \AA}$ ,  $\xi = 3.905 \text{ \AA}$  (just  $\Delta\rho$ )

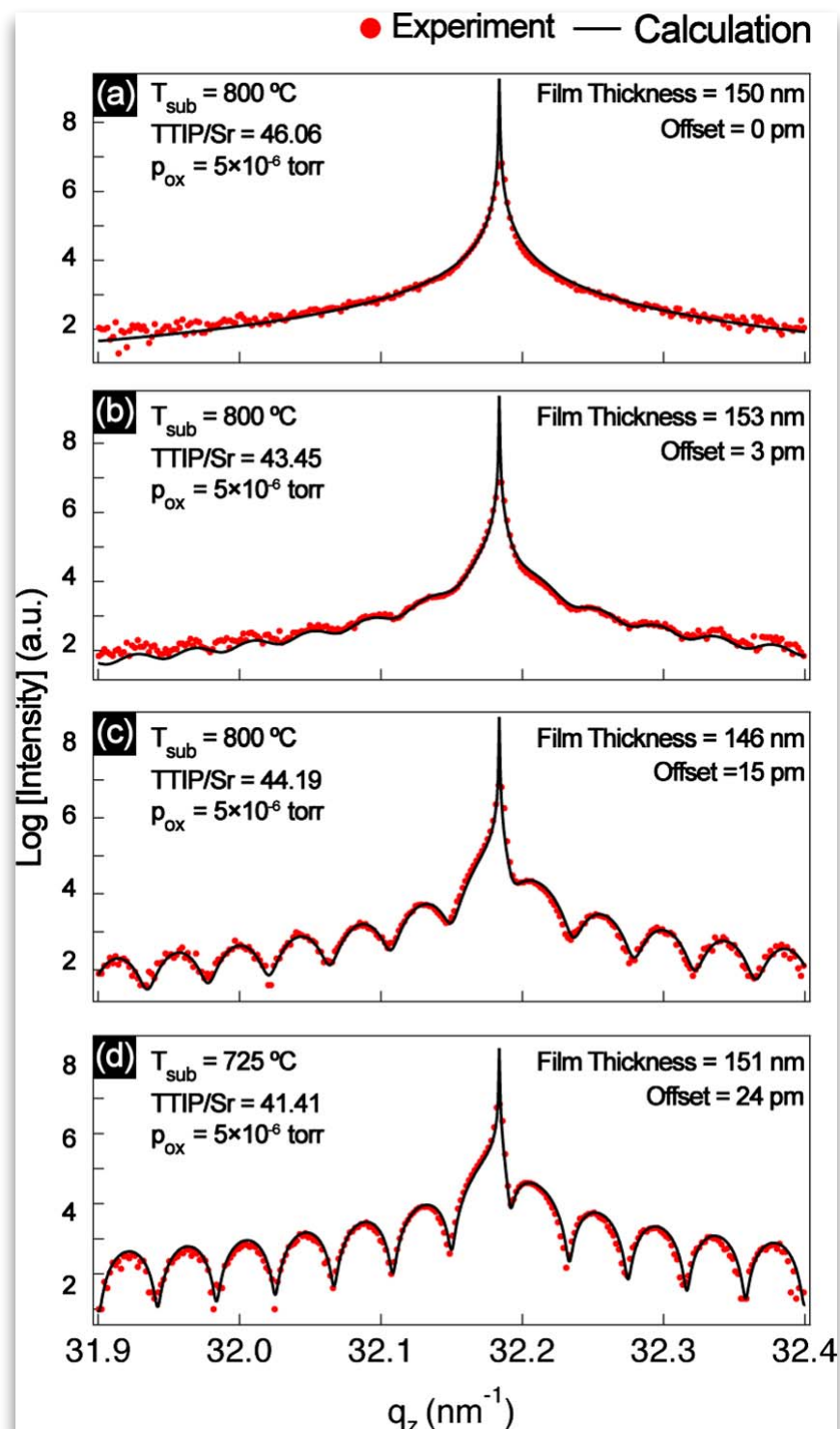
10uc STO/STO with  $c_{\text{film}}=3.905 \text{ \AA}$ ,  $a_{\text{sub}}=3.905 \text{ \AA}$ ,  $\xi = 3.93 \text{ \AA}$  (just  $\xi$ )



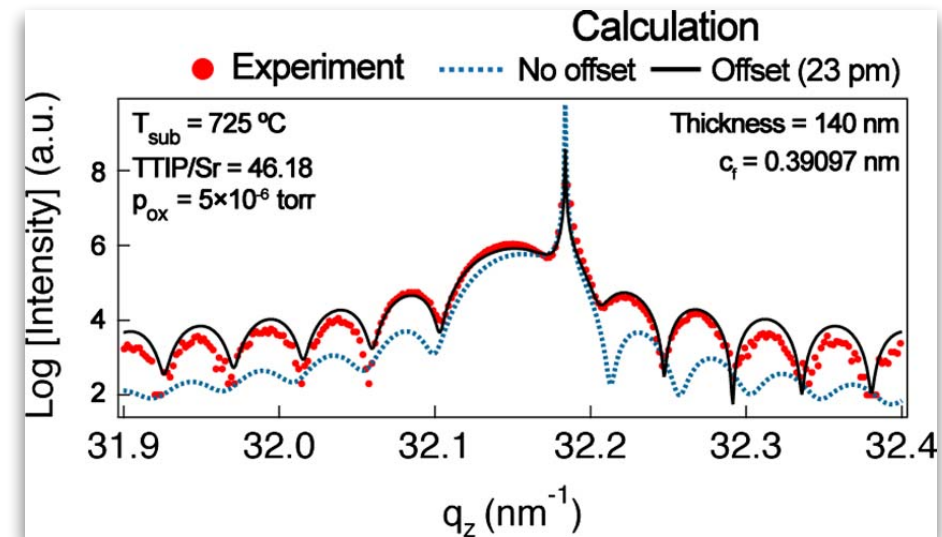


# Experimental verification - hybrid MBE + MOCVD

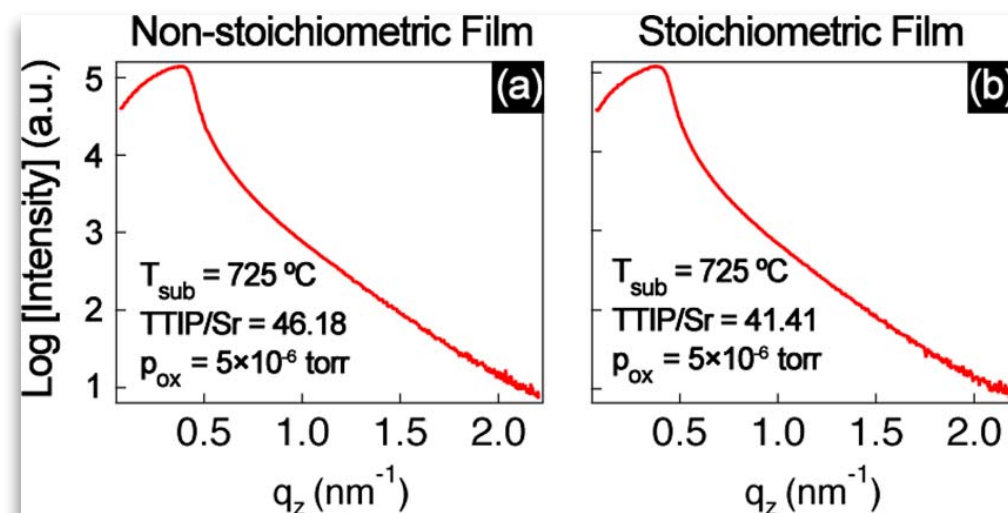
stoichiometric STO on STO with different  $\xi$



purposefully non-stoichiometric STO



reflectivity is  $\sim$  insensitive to the stoichiometry



LeBeau *et al.*, Appl. Phys. Lett. **95**, 142905 (2009)

# A few words on grazing incidence studies

# Index of refraction

$$n = 1 - \delta + i\beta$$

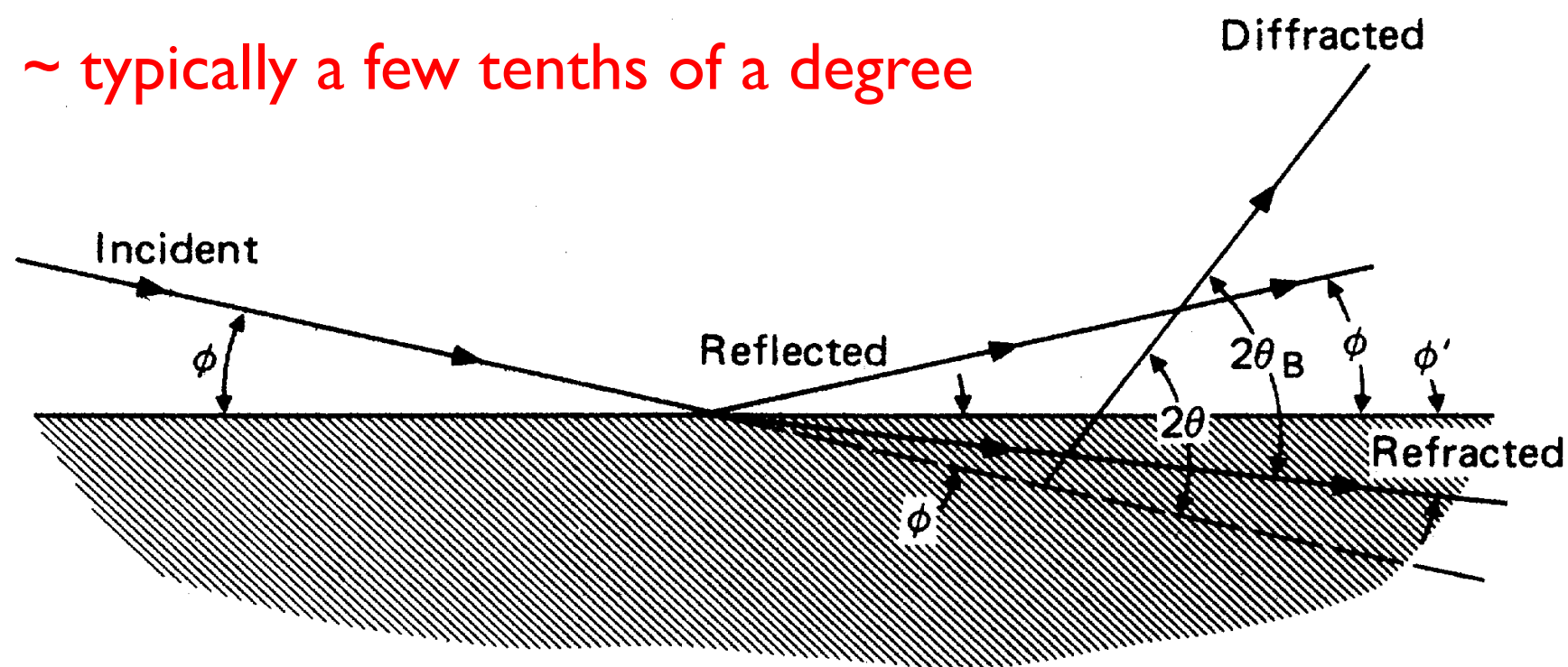
where  $\delta$  related to mass density and  $f'(Q)$

$\beta$  related to absorption and  $f''(Q)$

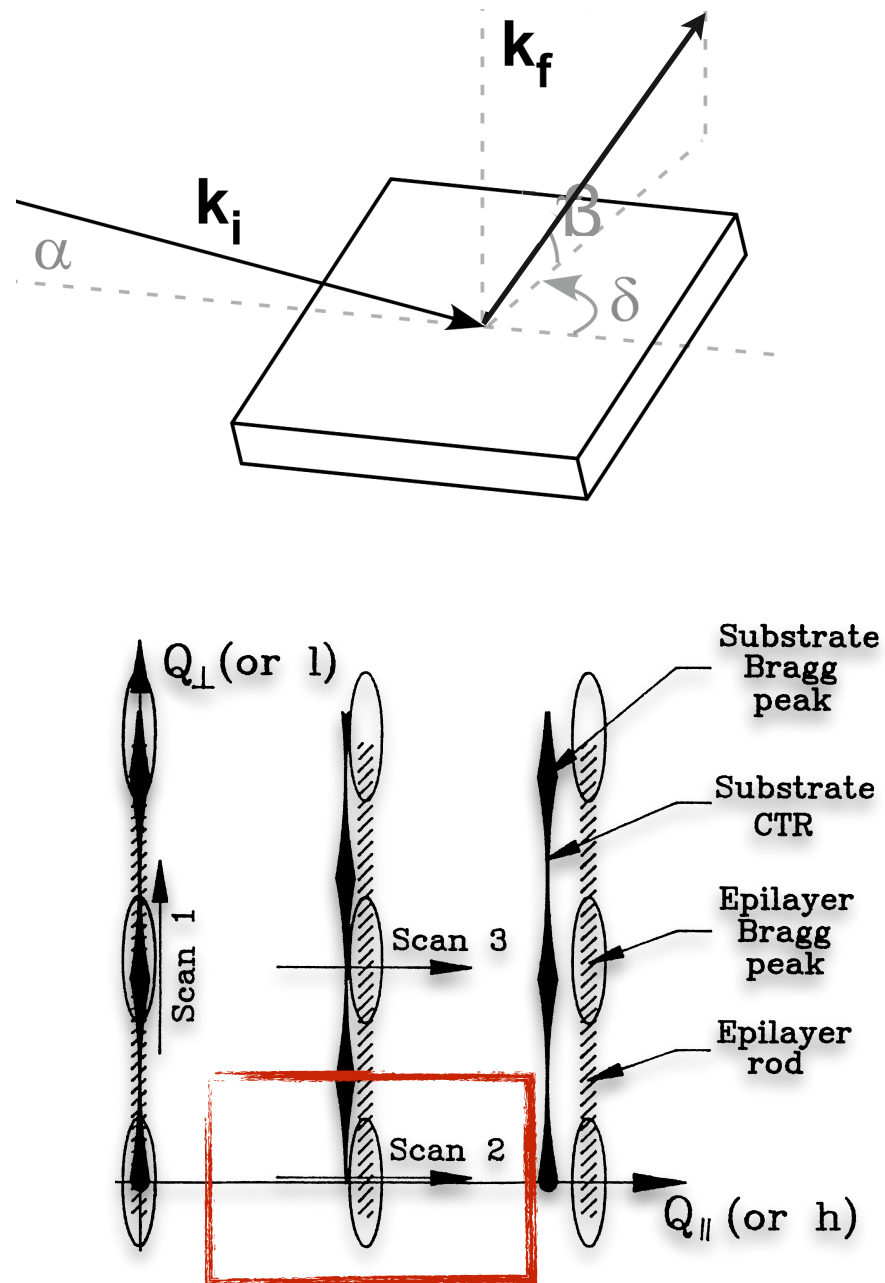
$$n \equiv 1 - \frac{2\pi \rho_{at} r_0}{k^2} \{f^0(0) + f' + i f''\}$$

critical angle for total external reflection:  $\alpha_c = (2\delta)^{1/2}$

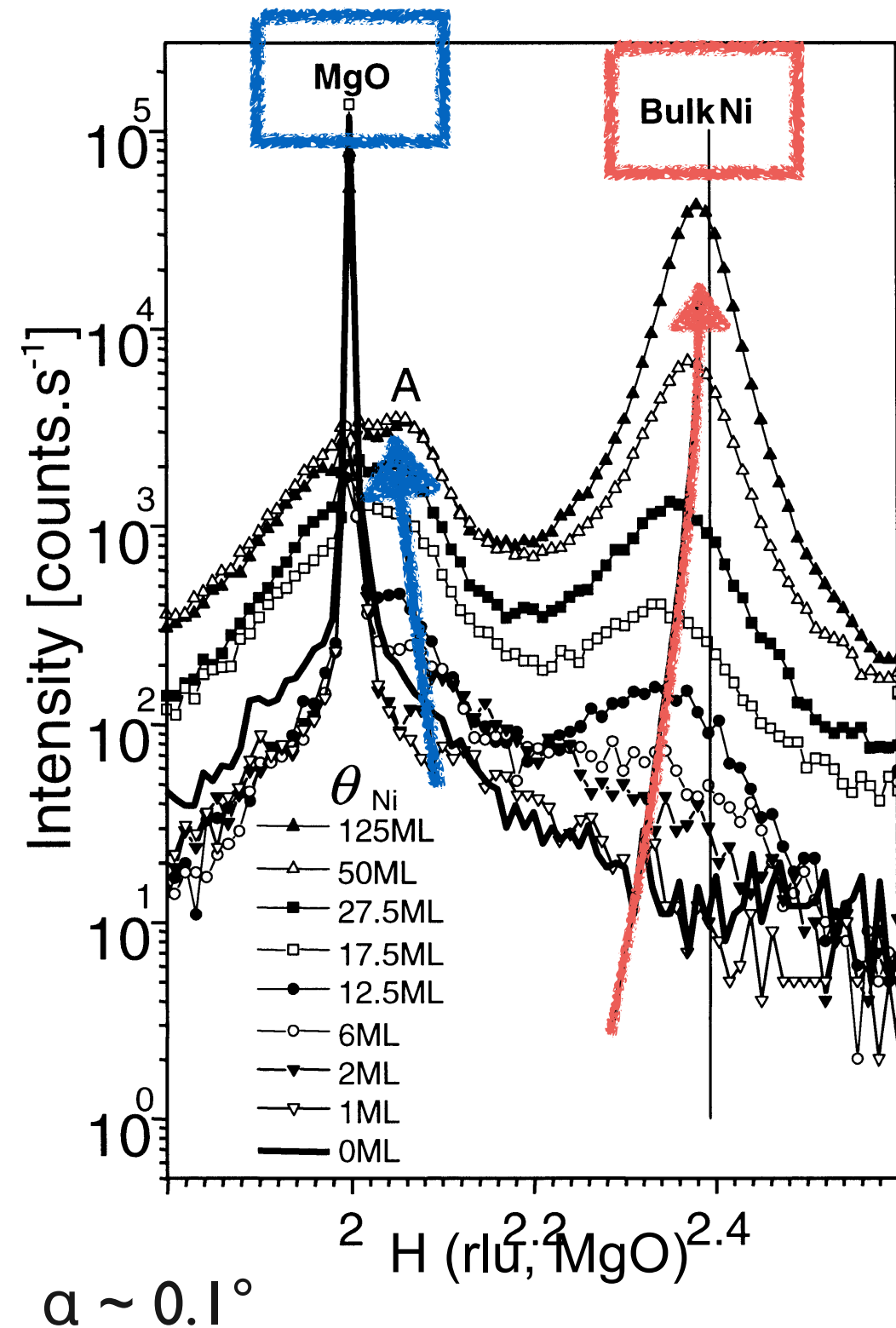
~ typically a few tenths of a degree



M. Toney and S. Brennan, Phys. Rev. B. **39**, 7963 (1989)

In-plane peaks ( $L \sim 0$ ): grazing incidence diffraction

G. Renaud, Surf. Sci. Rep. **32**, 1 (1998)



( $L \sim 0.05$ : also near  $\alpha_c$  but exiting the sample)



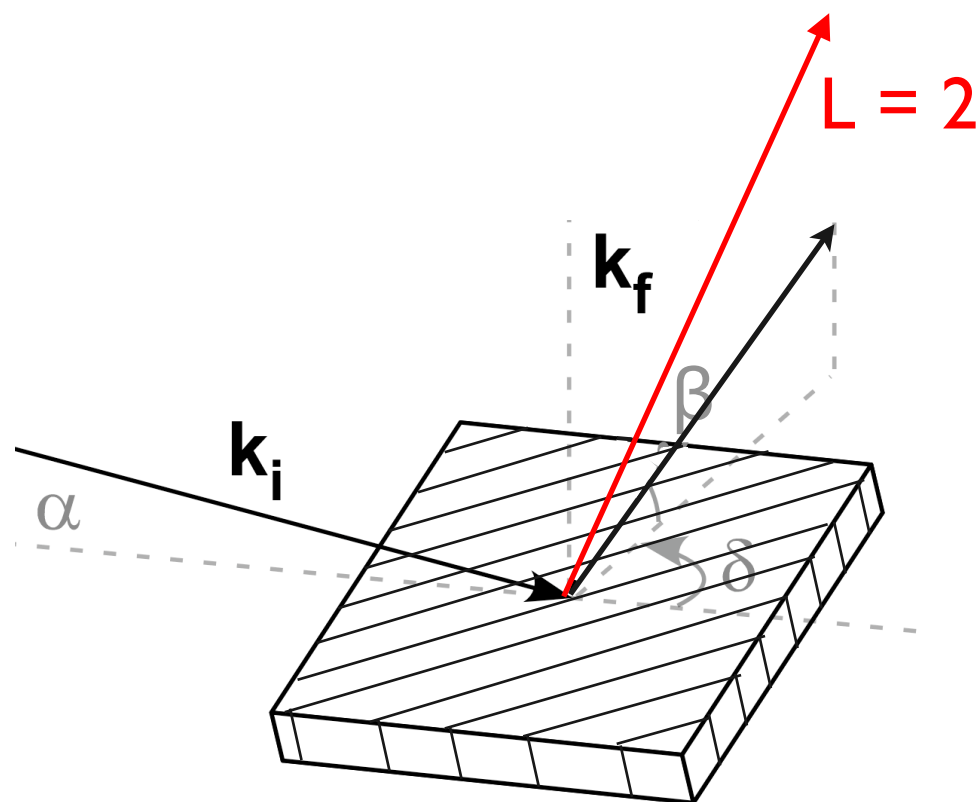
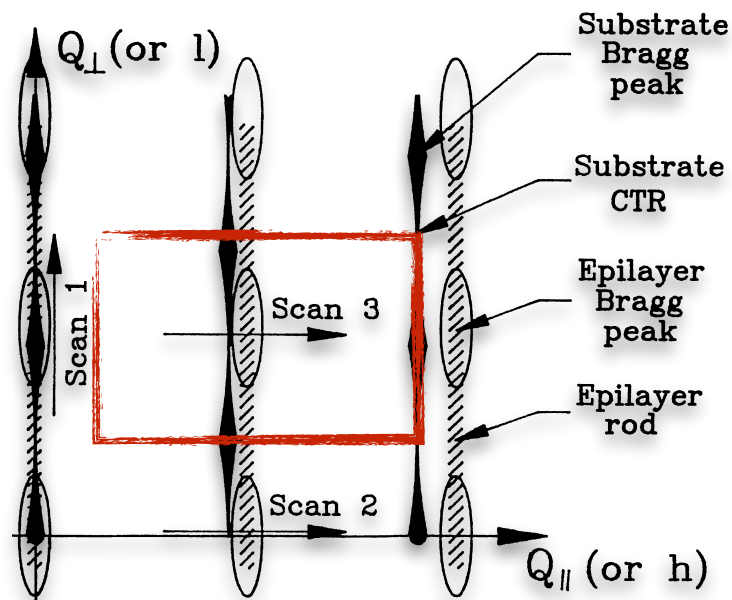
Growth of  $\text{Pb}(\text{Zr},\text{Ti})\text{O}_3$  films on  $\text{SrTiO}_3$  (001)A photograph of a Molecular Beam Epitaxy (MOCVD) system mounted on a Z-axis diffractometer. The setup is housed in a large, industrial-grade metal enclosure with a glass viewing window. Inside, various components are visible, including a central vertical chamber wrapped in silver thermal insulation, a substrate stage at the bottom, and a complex network of pipes and electrical cables. A red arrow points from the right side of the image towards the central chamber. The text 'MOCVD mounted on Z-axis diffractometer' is overlaid in a blue box at the top of the image. The text 'Sector 12, APS' is located in the bottom left corner of the image area. The text 'X-rays' is on the right side of the image, with a red arrow pointing towards the central chamber.

MOCVD mounted on Z-axis diffractometer

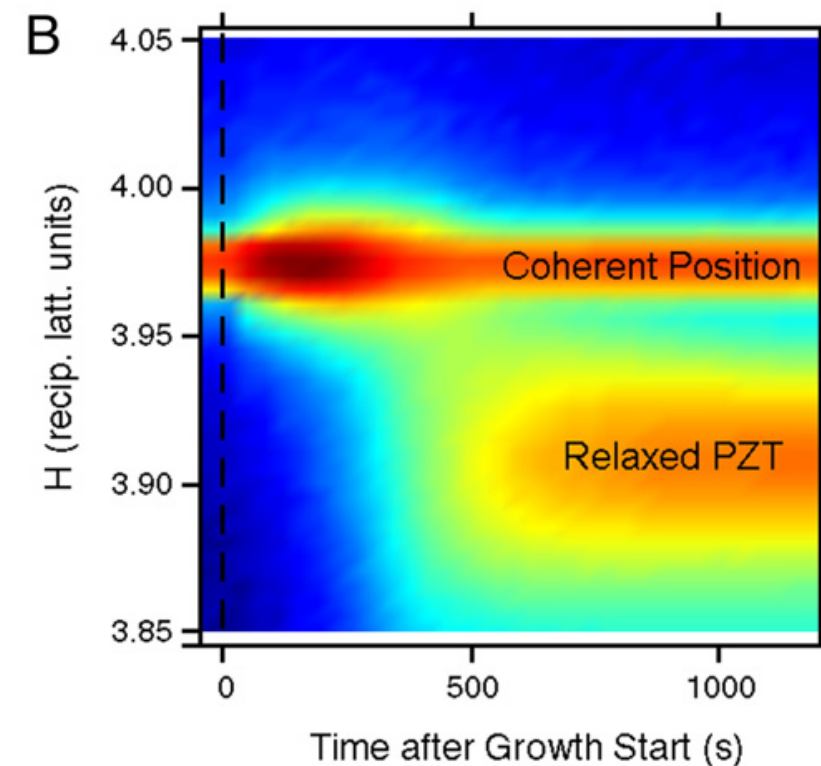
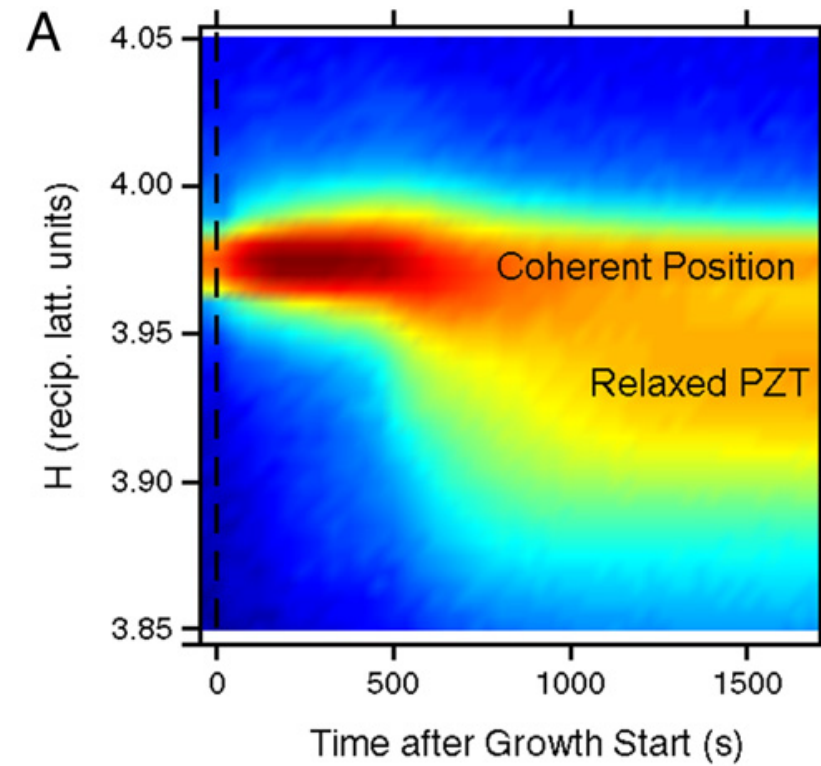
X-rays

Sector 12, APS

# In-plane peaks ( $L \neq 0$ ): grazing incidence diffraction



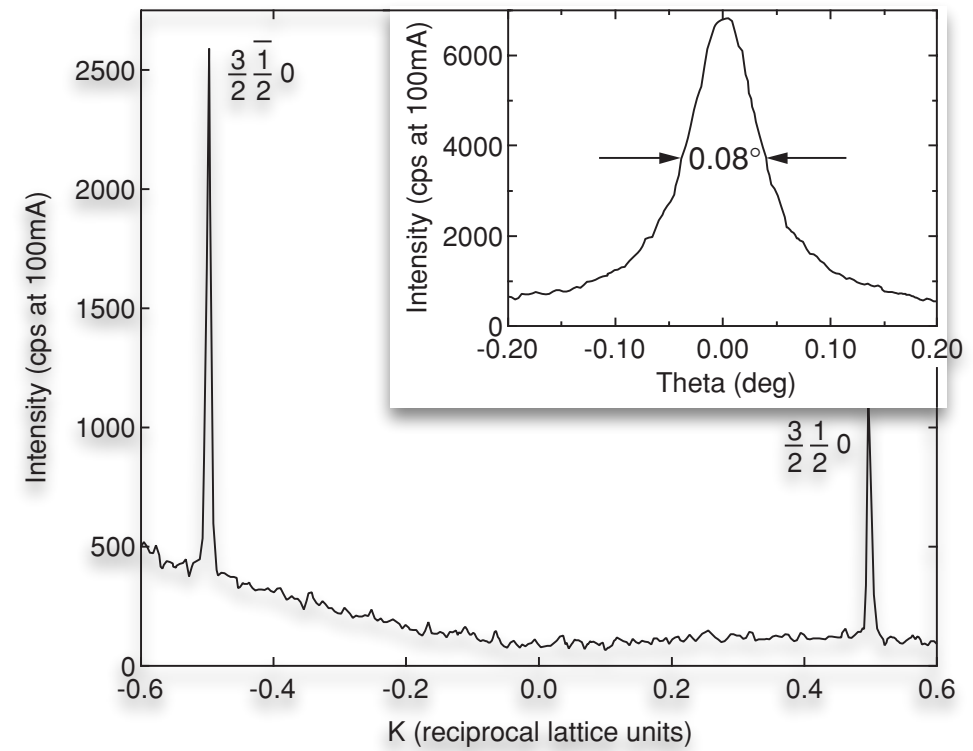
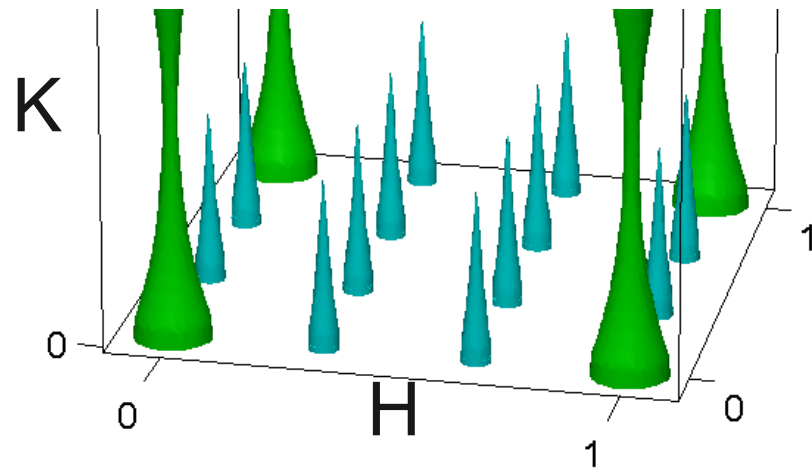
G. Renaud, Surf. Sci. Rep. **32**, 1 (1998)



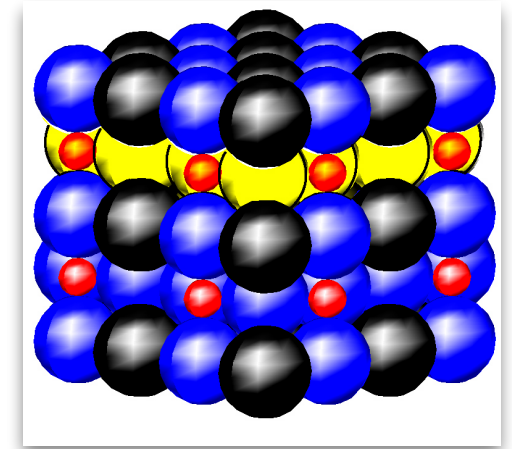
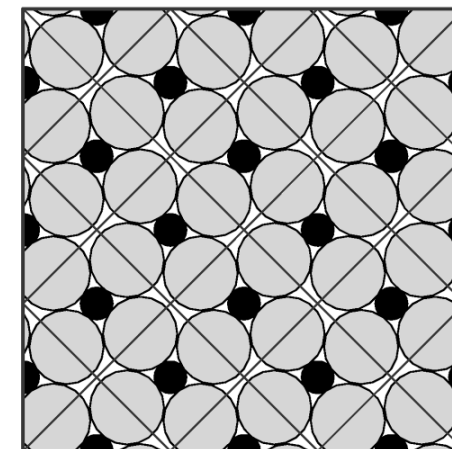
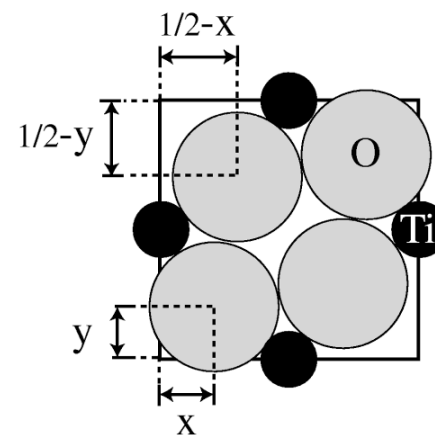
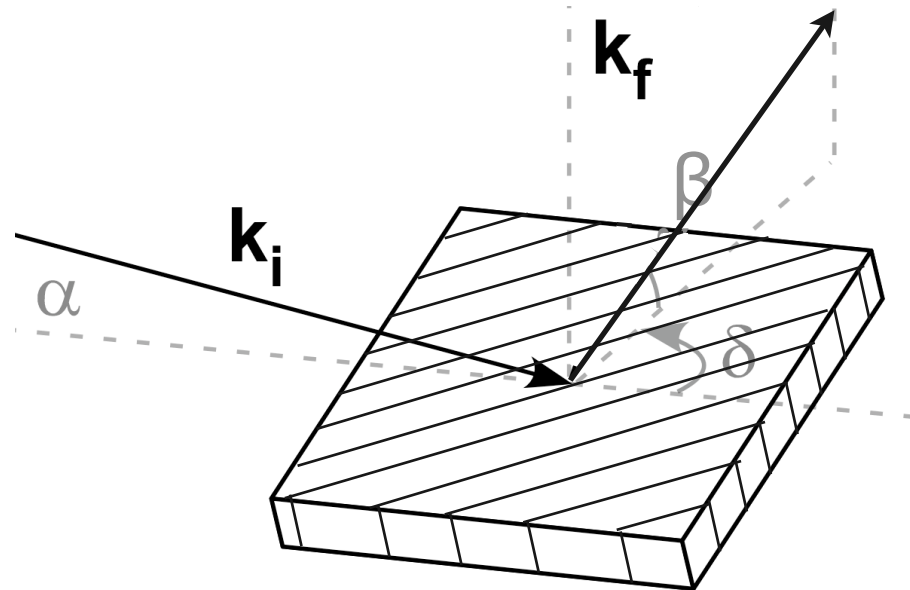
R.-V. Wang et al., Thin Solid Films **515**, 5593 (2007)



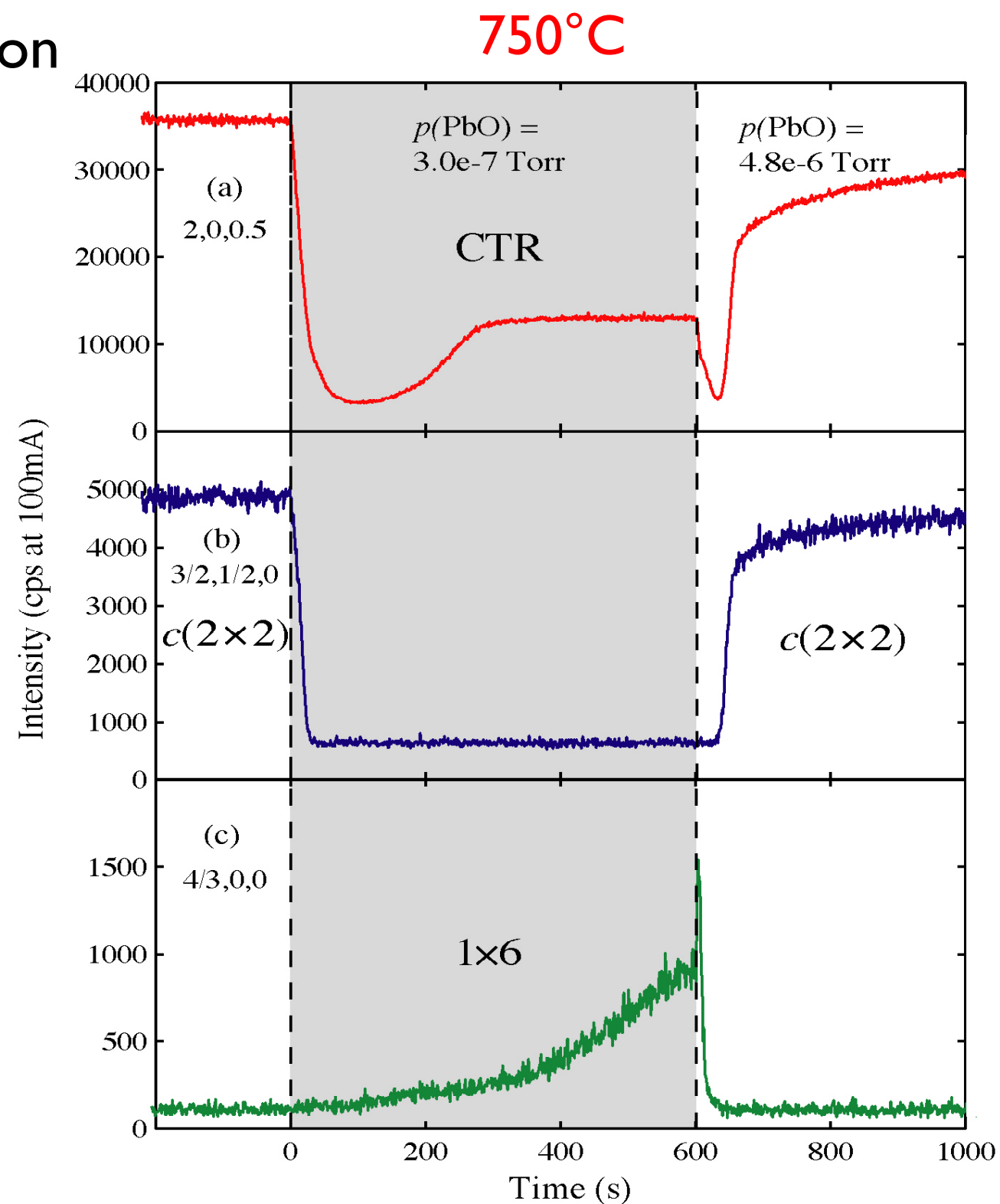
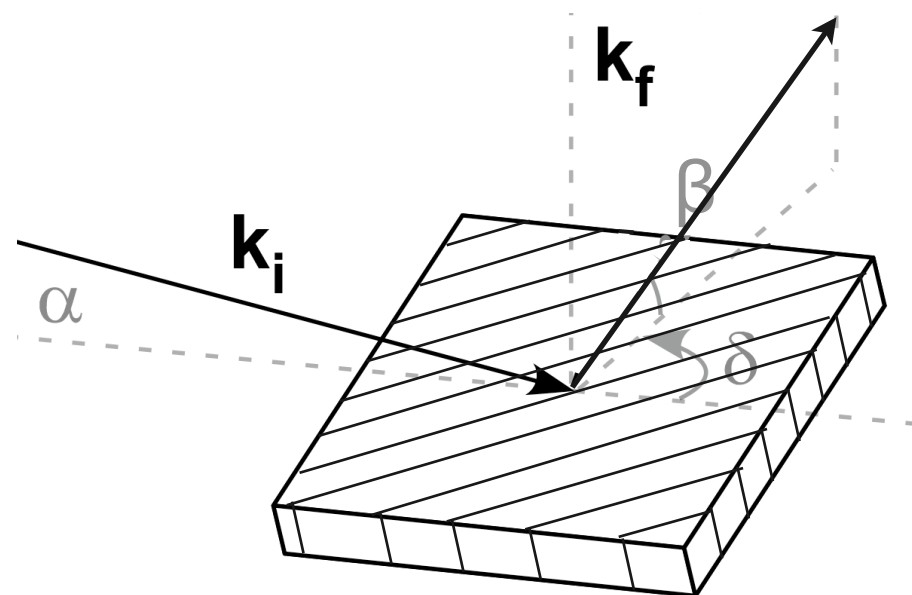
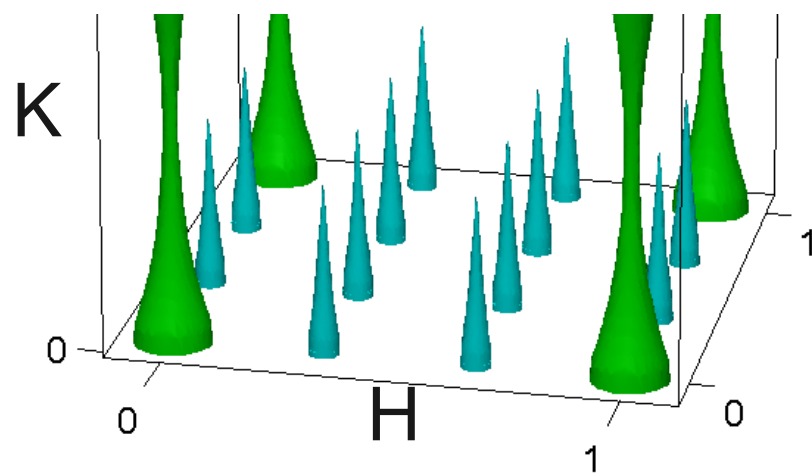
# In-plane peaks ( $L \sim 0$ ): surface reconstructions



This is actually the layer under the PbO surface



A. Munkholm *et al.*, Phys. Rev. Lett. **88**, 016101 (2001)

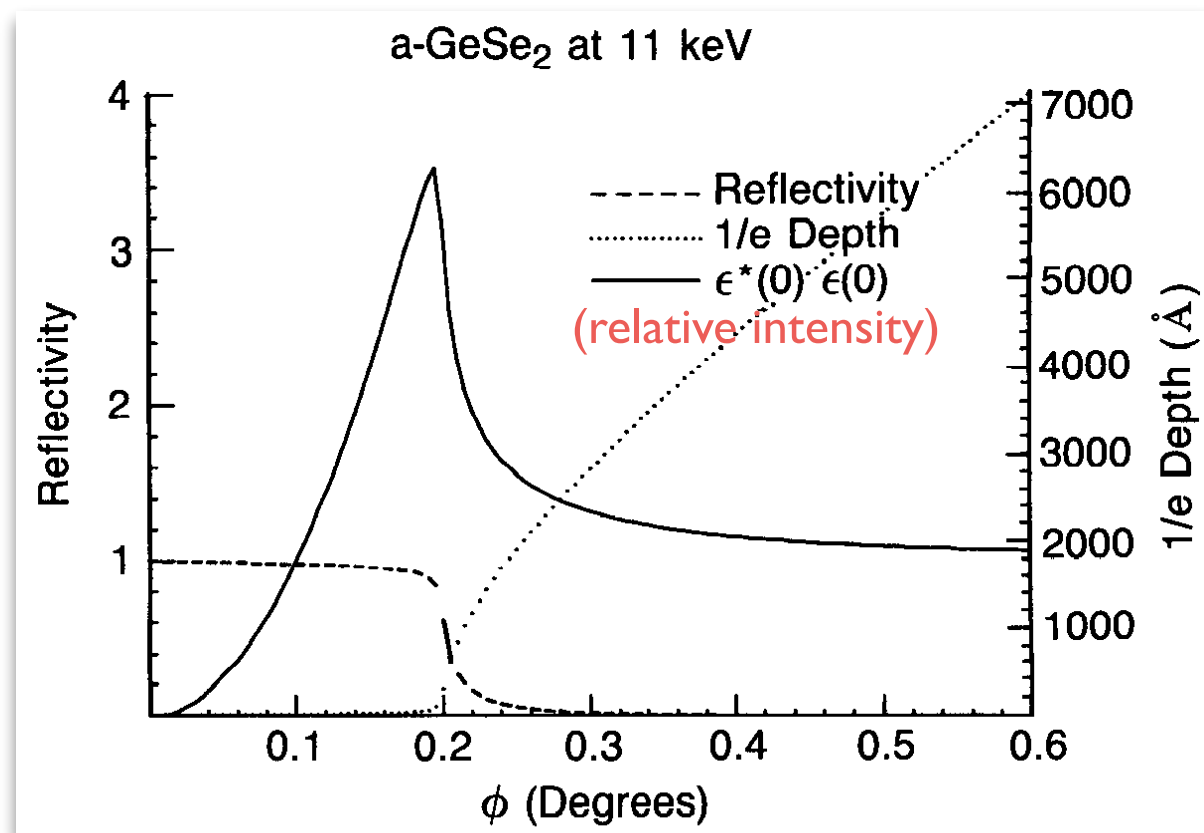
In-plane peaks ( $L \sim 0$ ): surface reconstructionsPbTiO<sub>3</sub>: PbO-induced reconstruction



# Grazing incidence

at and below  $\alpha_c$ ,

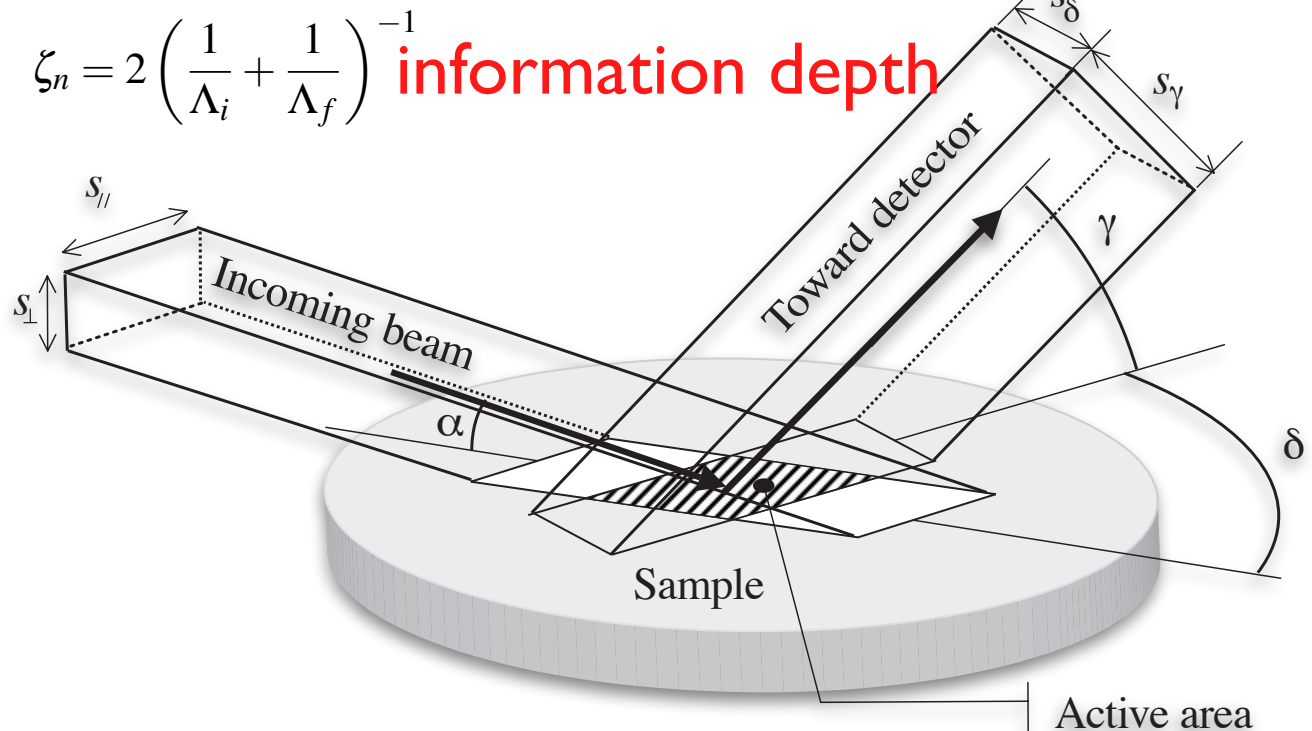
- penetration depth  $\sim 30 \text{ \AA}$  (“perfect” reflection below  $\alpha_c$ )
  - can work at  $\alpha_c$  for in-plane diffraction studies [you get a relative intensity enhancement]
    - e.g., H 0 0 scan [grazing incidence + grazing exit] - often for studies of in-plane reconstruction peaks
    - can also do CTR-scans on ultrathin films (e.g., 1-5 unit cells) - but out-of-plane scans are shifted in  $L$
    - can improve signal from intensity boost at  $\alpha_c$  from total external reflection + large footprint
- **but you don't need to vary penetration depth to get depth dependent info**
  - **from single crystals: modeling or solving phase problem also does it**



P. H. Fuoss and S. Brennan, Annu. Rev. Mater. Sci. 20, 365 (1990)

$$\Lambda_i = \frac{\lambda}{2\pi\sqrt{2}} \left( \sqrt{(\sin^2 \alpha_i - \alpha_{c,n}^2)^2 + 4\beta_n^2} + \alpha_{c,n}^2 - \sin^2 \alpha_i \right)^{-1/2} \quad \text{penetration depth}$$

$$\Lambda_f = \frac{\lambda}{2\pi\sqrt{2}} \left( \sqrt{(\sin^2 \gamma - \alpha_{c,n}^2)^2 + 4\beta_n^2} + \alpha_{c,n}^2 - \sin^2 \gamma \right)^{-1/2} \quad \text{penetration depth}$$



O. Robach et al., J. Appl. Cryst. 33, 1006 (2000)

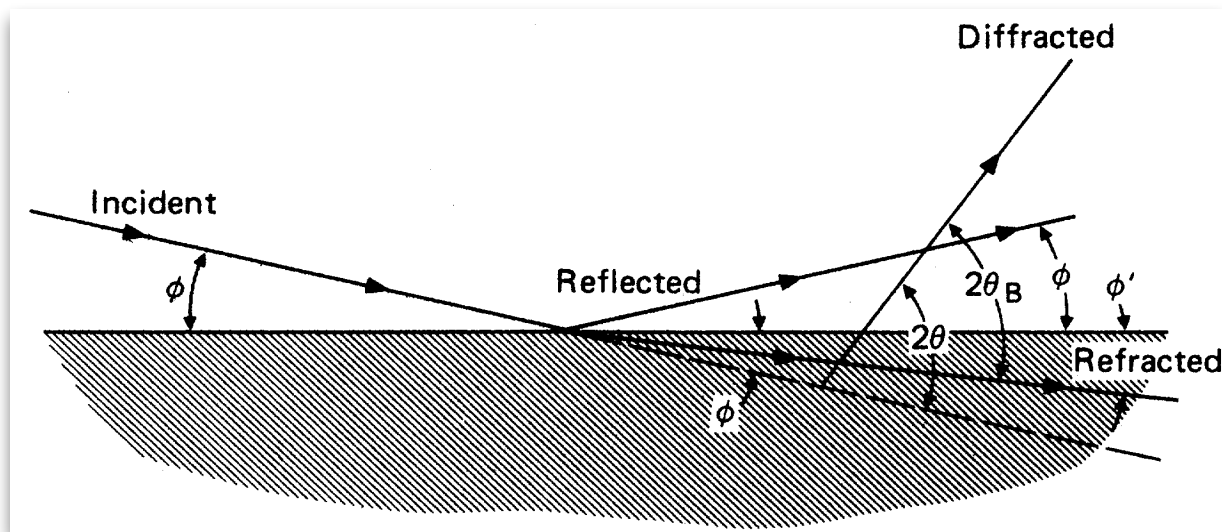
# Grazing incidence: effects of refraction

In-plane diffraction ( $L \sim 0$ ): no problem

But if you stay at  $\alpha_c$  to run up a CTR or SR:

- diffracted beam appears at altered L-position due to refraction

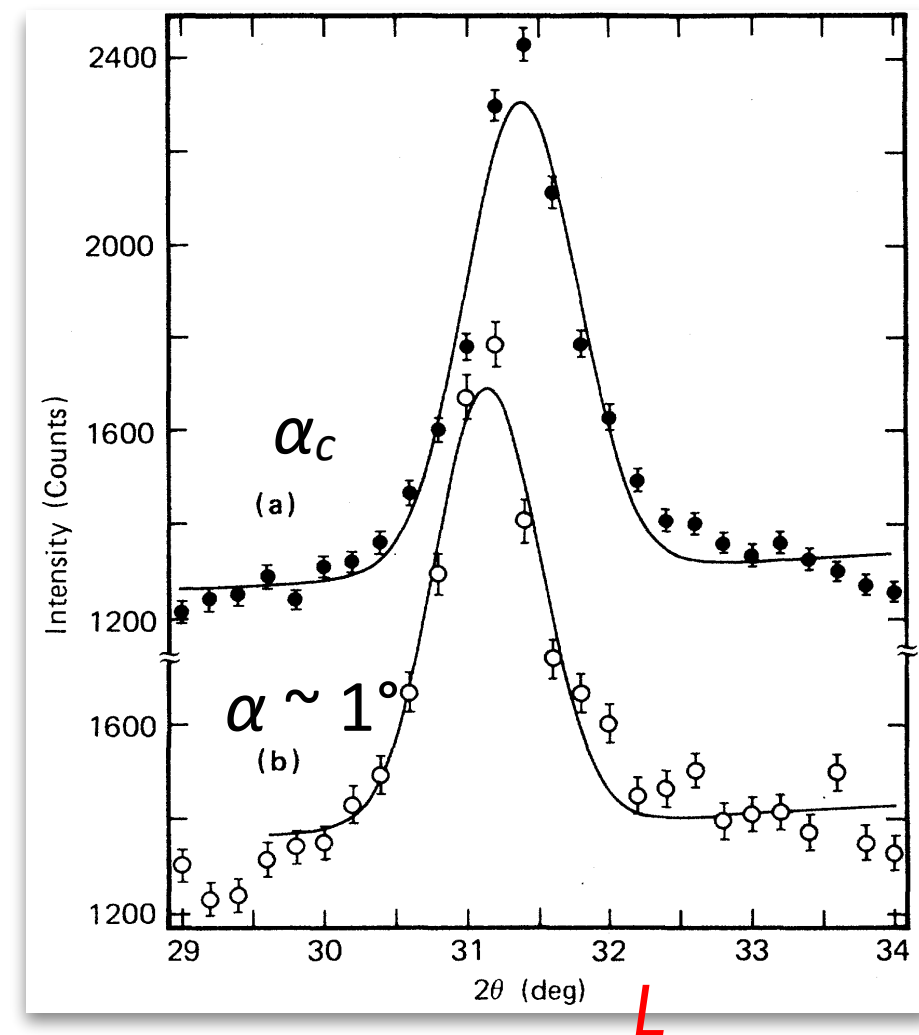
M. F. Toney and S. Brennan, Phys. Rev. B **39**, 7963 (1989)



Angular shift in out-of-plane direction:

$$\begin{aligned}
 2 \Delta\theta &= 2\theta - 2\theta_B \\
 &= \phi - \frac{(k'_r)_z}{(k'_r)_x} \\
 &\approx \phi - \frac{1}{\sqrt{2}} \{ [(\phi^2 - \phi_c^2)^2 + 4\beta^2]^{1/2} - \phi_c^2 + \phi^2 \}^{1/2} .
 \end{aligned}$$

So in general, we like to keep  $\alpha \sim 1^\circ$

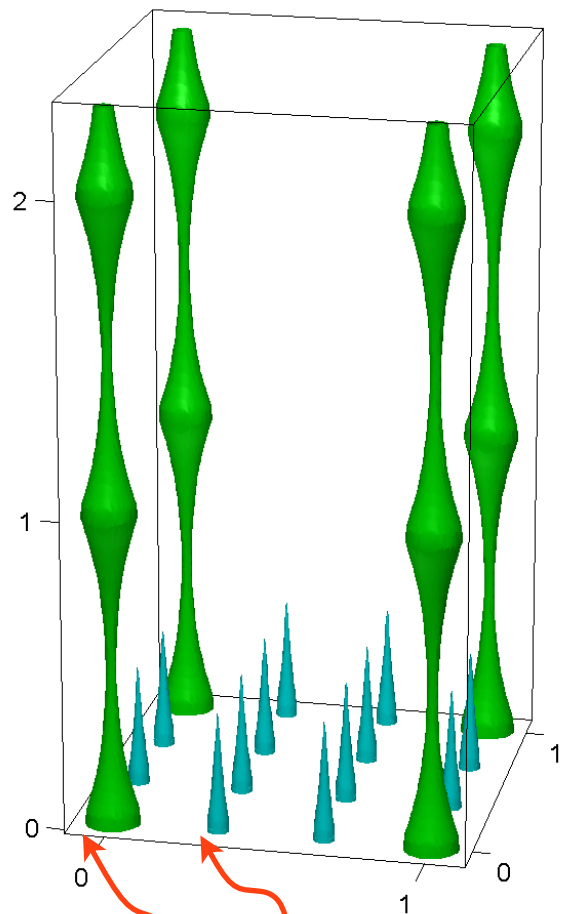


## Direct Methods

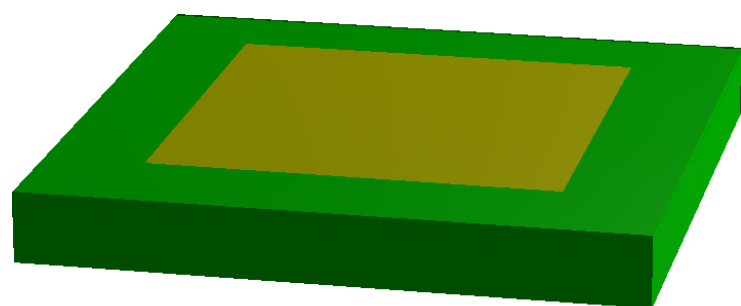
- Trying to avoid fitting
- Assumes coherent scattering (e.g., single crystal)
- if large single crystal -- doesn't need APS-U
- if small single crystal -- needs APS-U
- direct methods will become routine

Note: APS-U will make 3D Fourier transform easier

## 1D Fourier transform

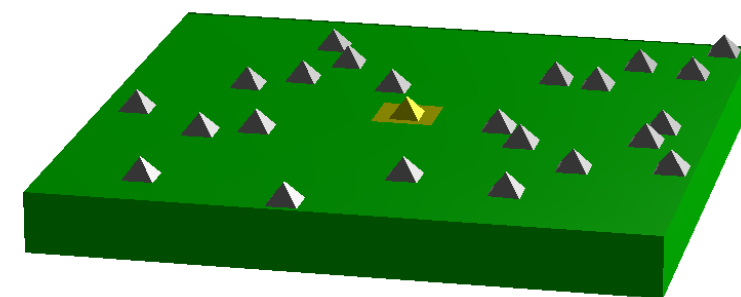
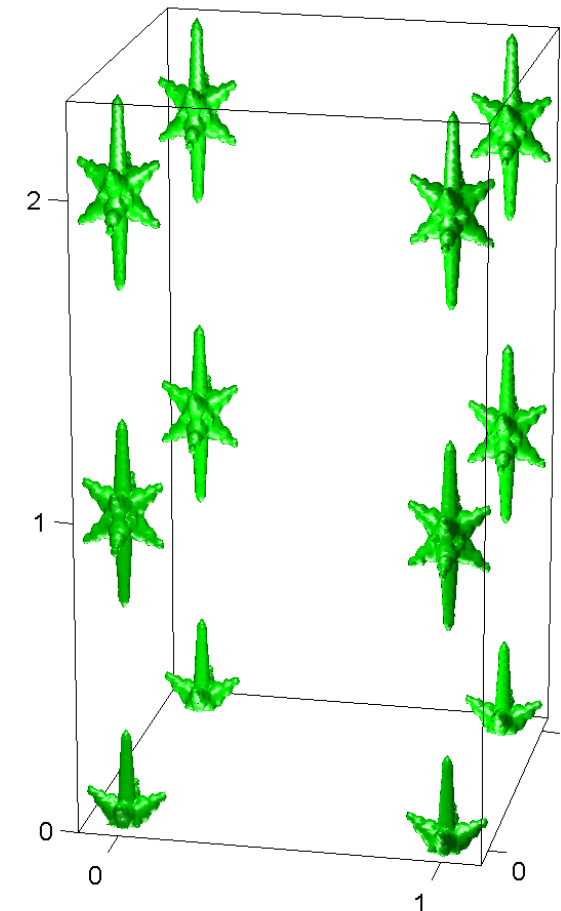


superstructure rods (SRs)  
crystal truncation rods (CTRs)



SXR D

## 3D Fourier transform



CDI

D. D. Fong *et al.* MRS Bulletin **35**, 504 (2010)

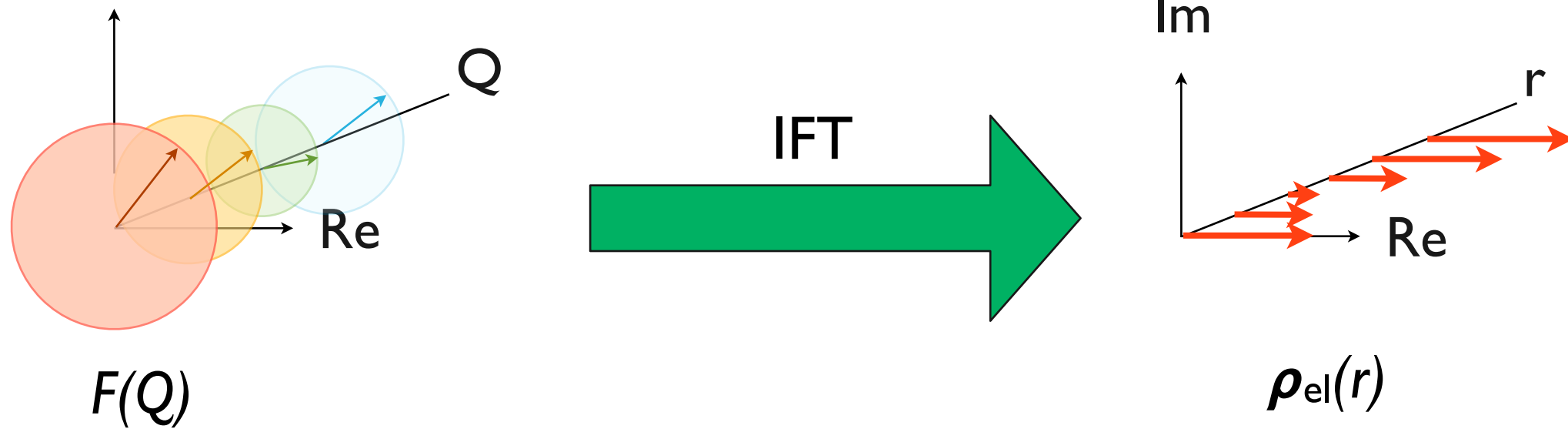




# Fourier cycling

Need to assign some phases (imaginary parts) to  $F(Q)$  to start

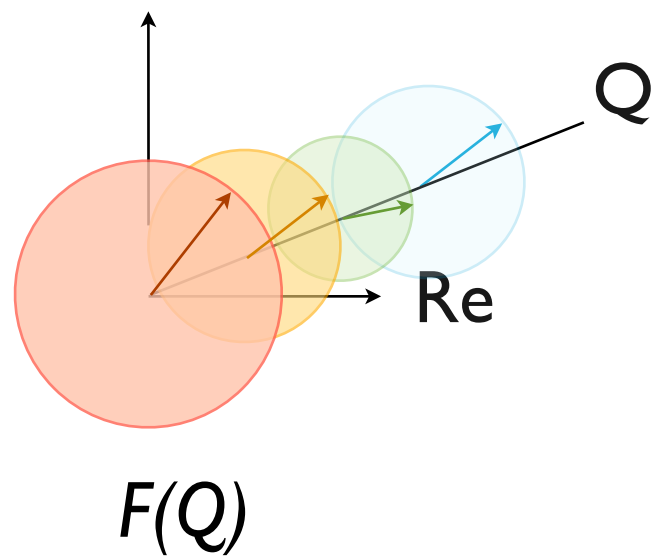
**Ideally:** Im



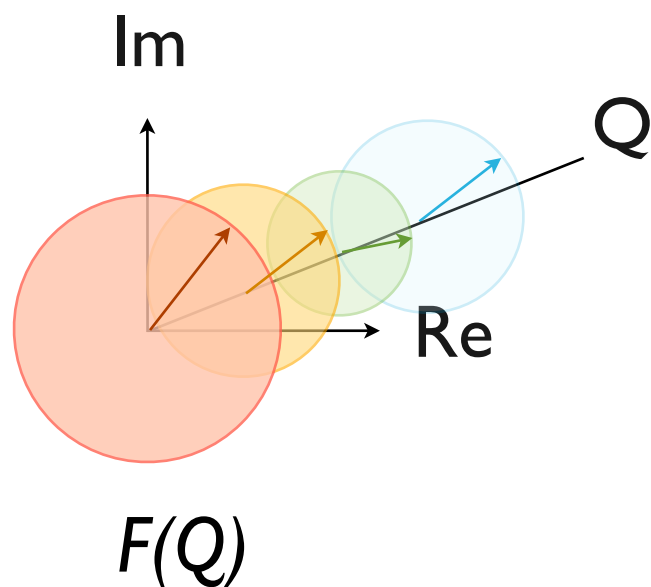
## Fourier cycling

Need to assign some phases (imaginary parts) to  $F(Q)$  to start

**Ideally:** Im



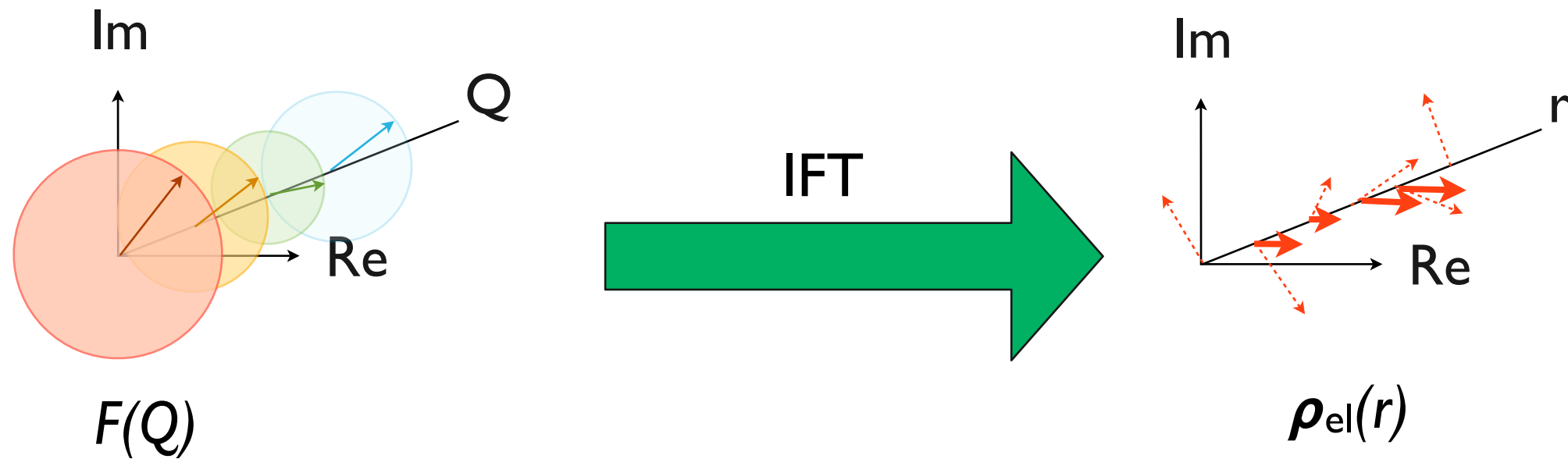
But usually:



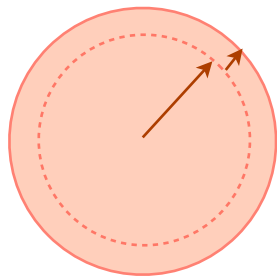
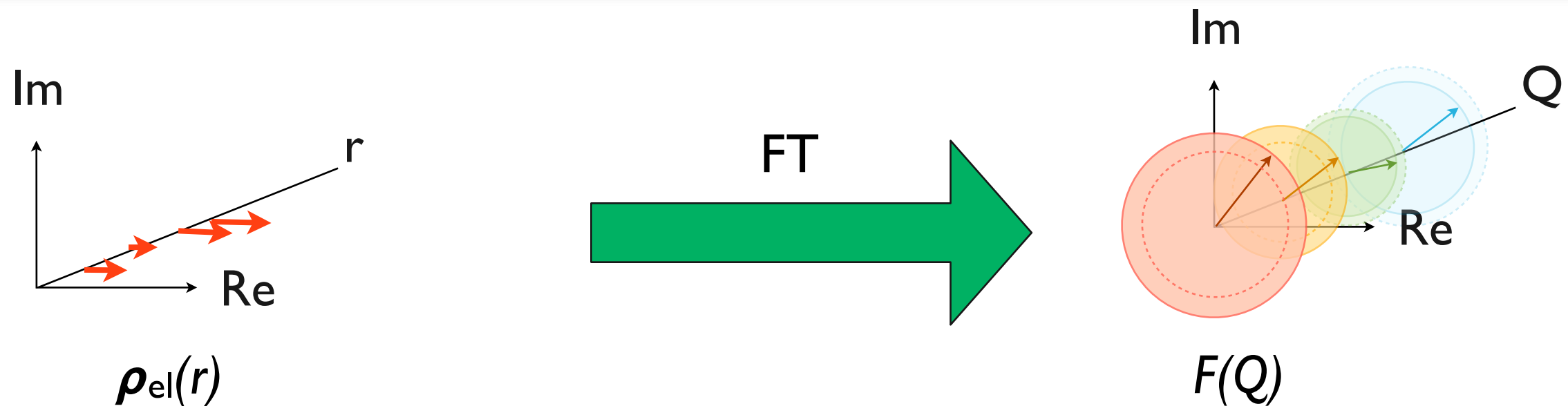


## Fourier cycling

So force it to be real & positive (zero the imaginary & negative parts)



## Fourier cycling — now FT



Fix the amplitude of  $F(Q)$  to match the data

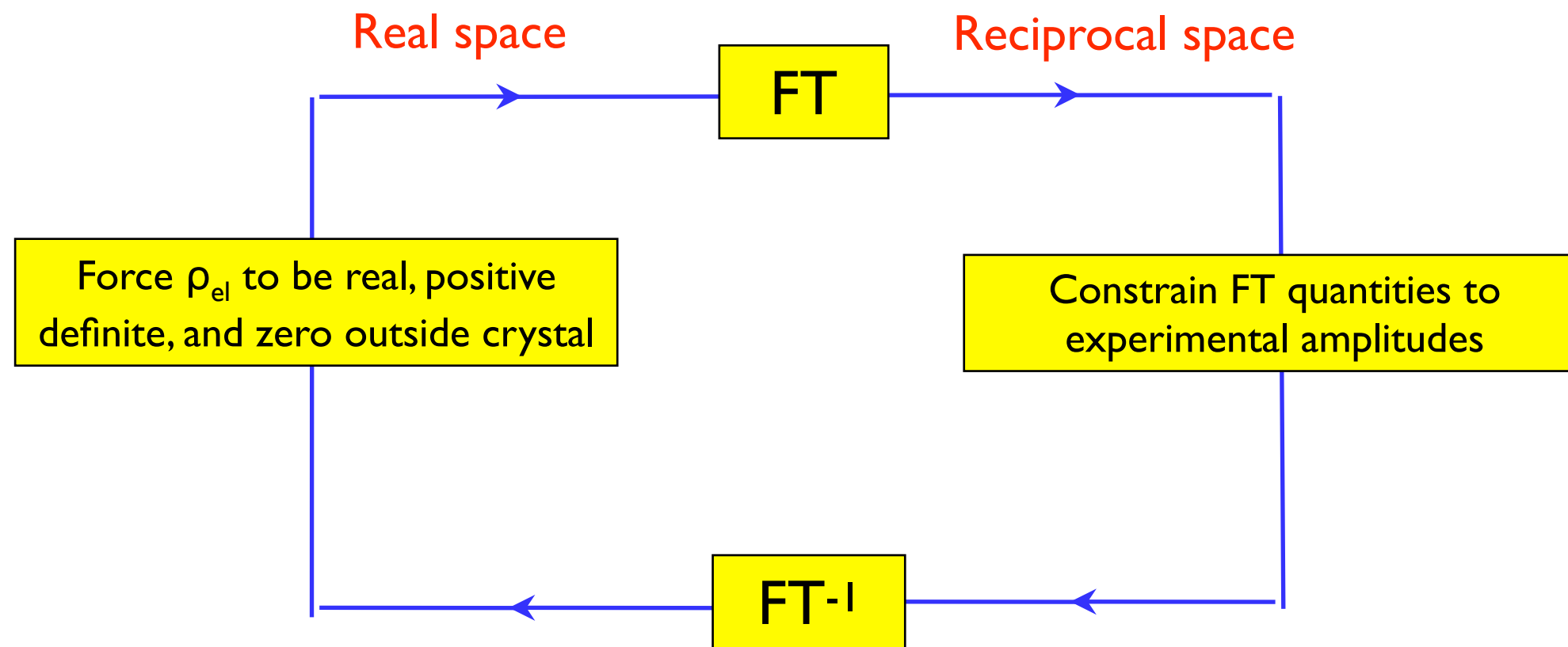
This corresponds to error corrections in reciprocal space:  $\Delta F(Q)$

Can be shown that these are “minimum-change” operations such that the sum of the squared errors can be minimized through an iterative algorithm (Fourier cycling)

# Fourier cycling

R. W. Gerchberg and W. O. Saxton, "A practical algorithm for the determination of the phase from image and diffraction plane pictures," *Optik* **35**, 237 (1972)

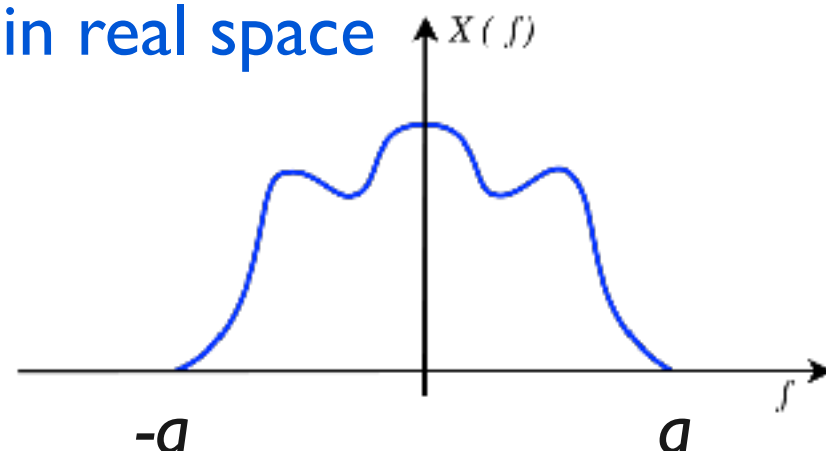
J. R. Fienup, *Opt. Letters* **3**, 27 (1978); *Appl. Opt.* **21**, 2758 (1982)



# Oversampling

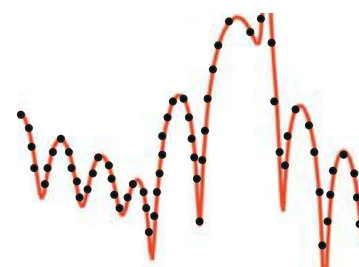
How much data do you need to take to reconstruct  $\rho_{\text{el}}$ ?

film thickness in real space



Need to sample by at least  $\Delta Q = 1/(2a)$  in reciprocal space, but this assumes we can access the complex structure factor (amplitude and phase)

- since we can only sample the structure factor amplitude, we need to sample by  $\Delta Q = 1/(4a)$
- for a thin film, this is  $\Delta Q = 1/(2t)$ , so for a 2 unit cell film, we need to sample at a spacing of  $\Delta L \sim 0.25$
- Not a problem for CTRs (continuous): we typically sample at least twice this ( $\sim 7$  points per thickness fringe) - **oversampling** (can only be done along  $L$  for thin films)
- We can do this for multiple CTRs



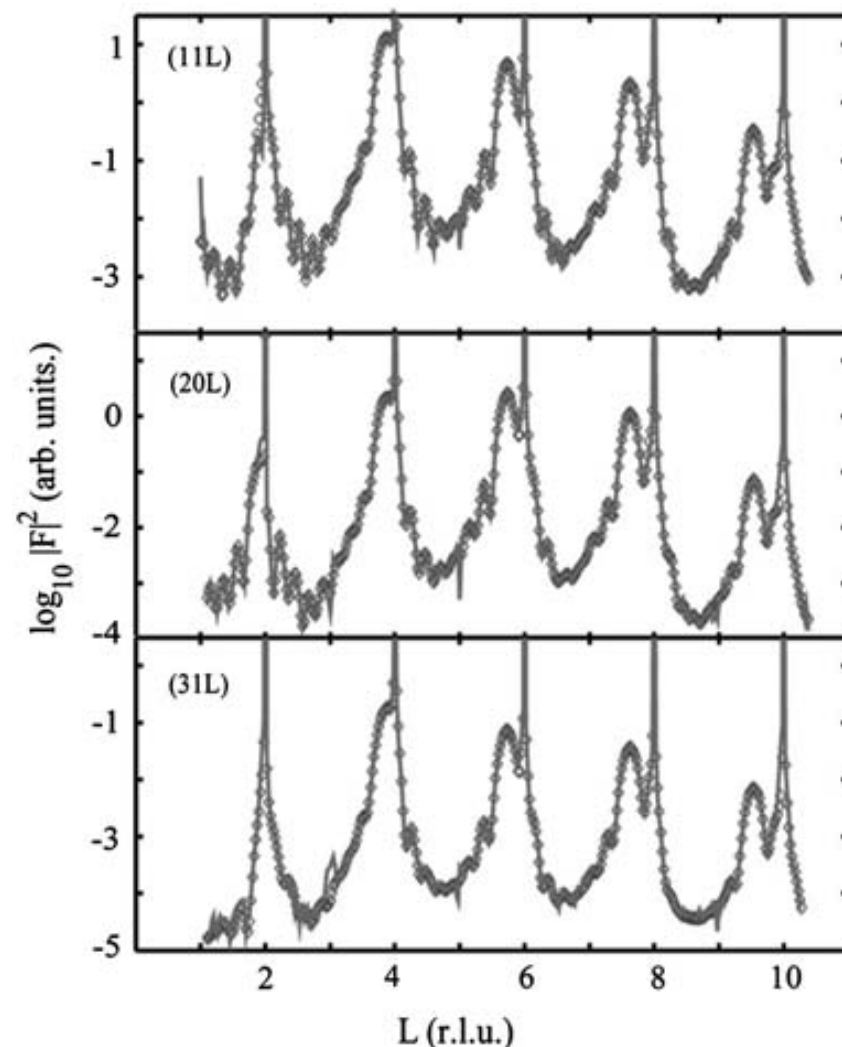
D. Sayre, Struct. Chem. **13**, 81 (2002)

COherent Bragg Rod Analysis (COBRA): Example  $\text{La}_{2-x}\text{Sr}_x\text{CuO}_4 / \text{LaSrAlO}_4(001)$ 

Measure all independent rods  $F_{HK}(L)$

$$F(\mathbf{q}) = \sum_{j=1}^{N_{uc}} f_j(q) e^{i\mathbf{q} \cdot \mathbf{r}_j}$$

$$F_{HKL} = f_A e^{\pi i(H+K)} + f_B e^{\pi i(L)} + f_O \left[ 1 + e^{\pi i(K+L)} + e^{\pi i(H+K+L)} \right]$$



E.g., for 4mm perovskite symmetry:

3 independent rods

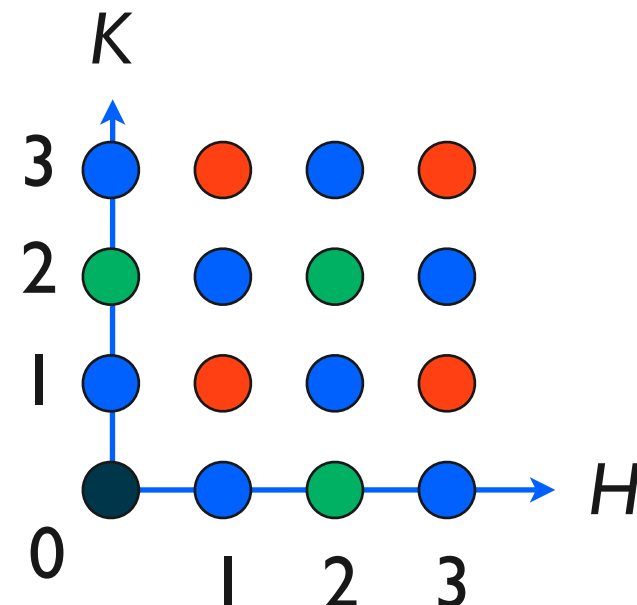
- (even, even, L) ●

- (odd, odd, L) ●

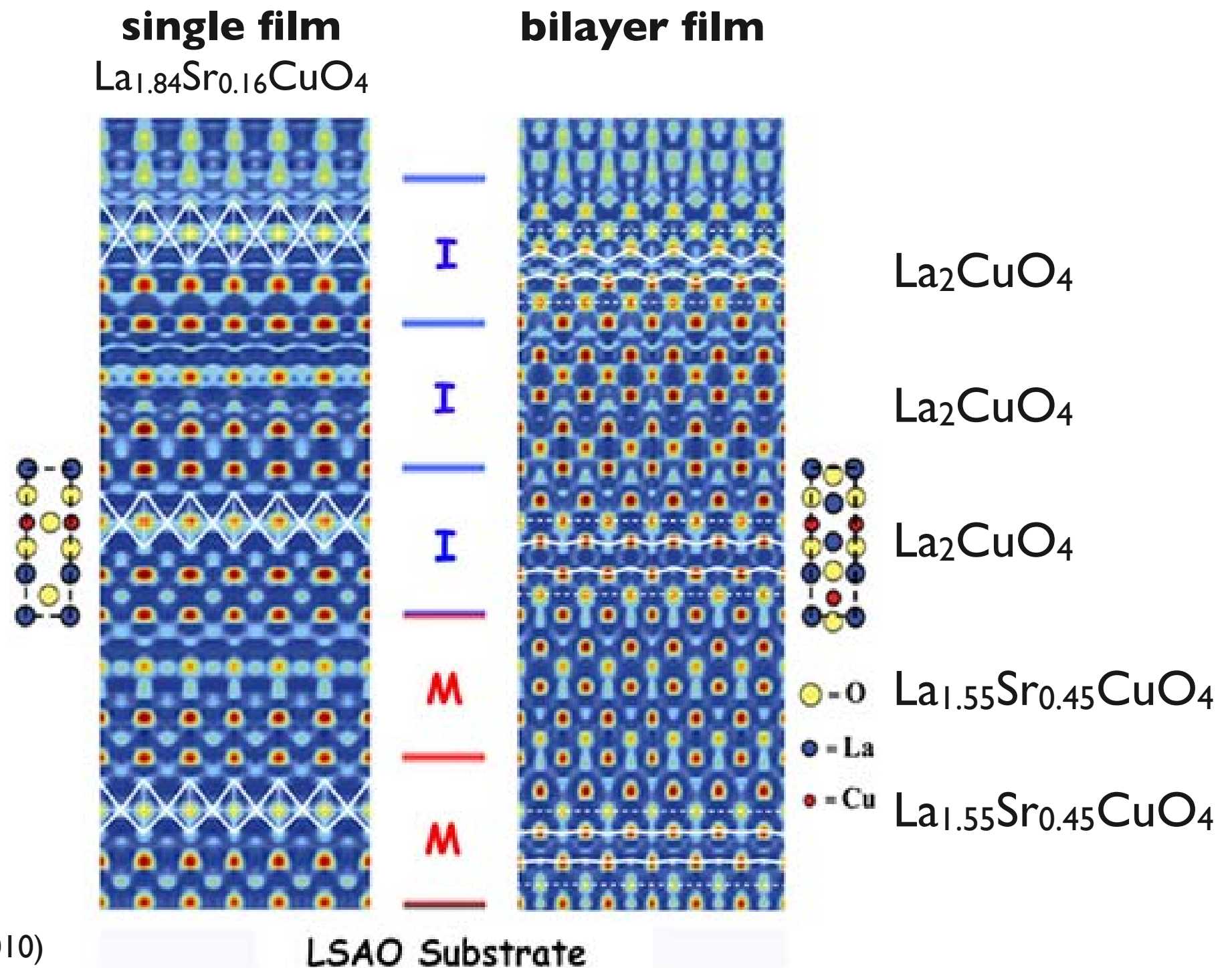
- (odd, even, L) ●

Typically more rods are measured for reduced error (at least 6 off-specular + specular)

- specular is often different (non-registered surface layers can modify the specular rod)



## Real space structures for single and bilayer films

 $\text{La}_{2-x}\text{Sr}_x\text{CuO}_4$  on  $\text{LaSrAlO}_4(001)$ 
H. Zhou *et al.*, PNAS **10**, 8103 (2010)



## Another way: DFT + fitting

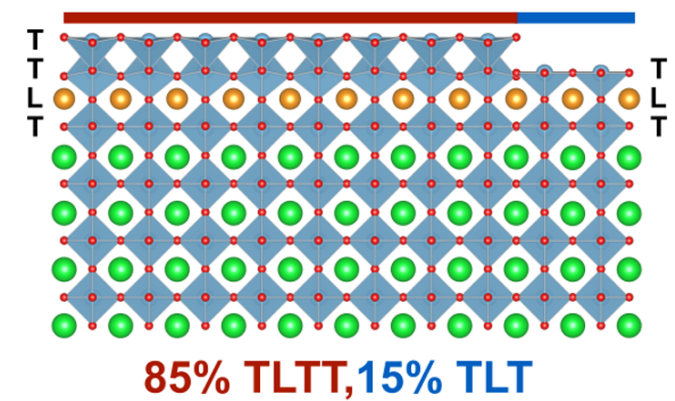
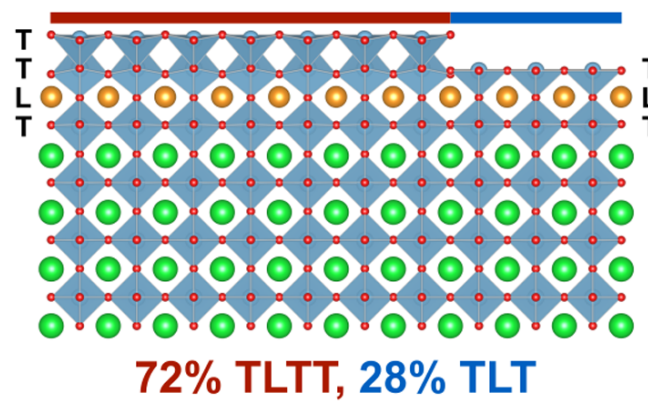
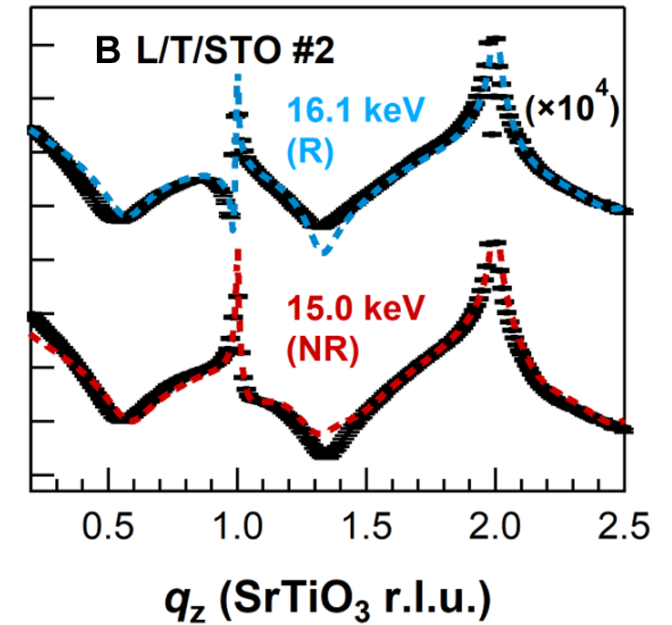
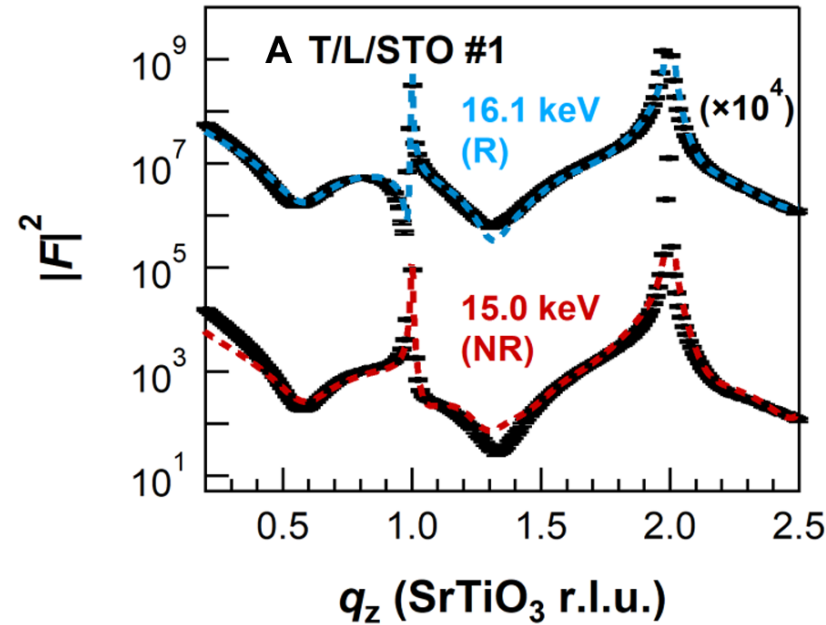
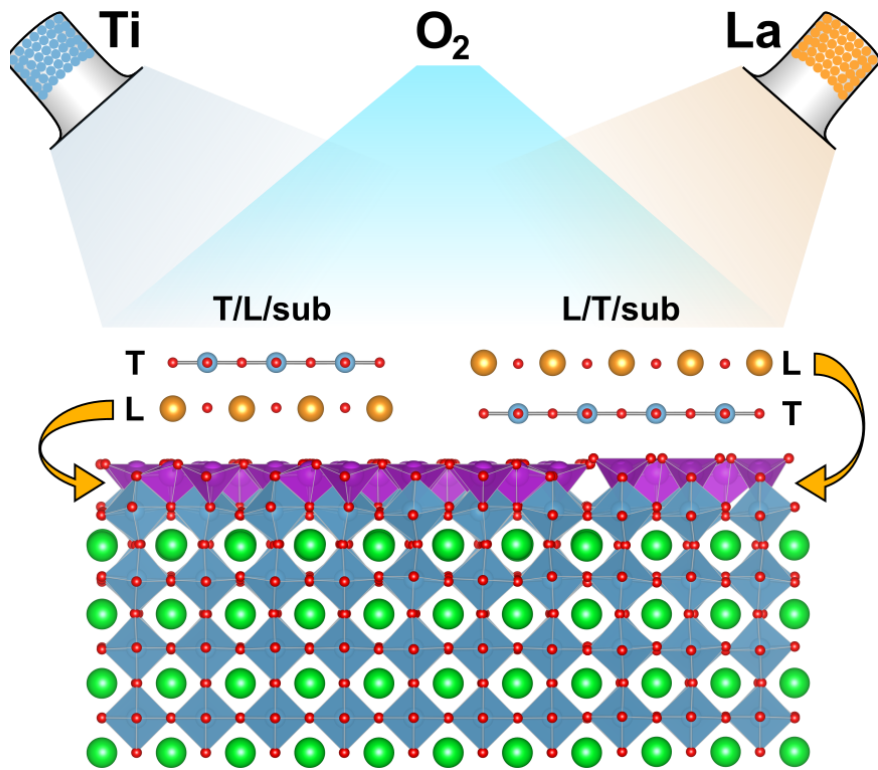
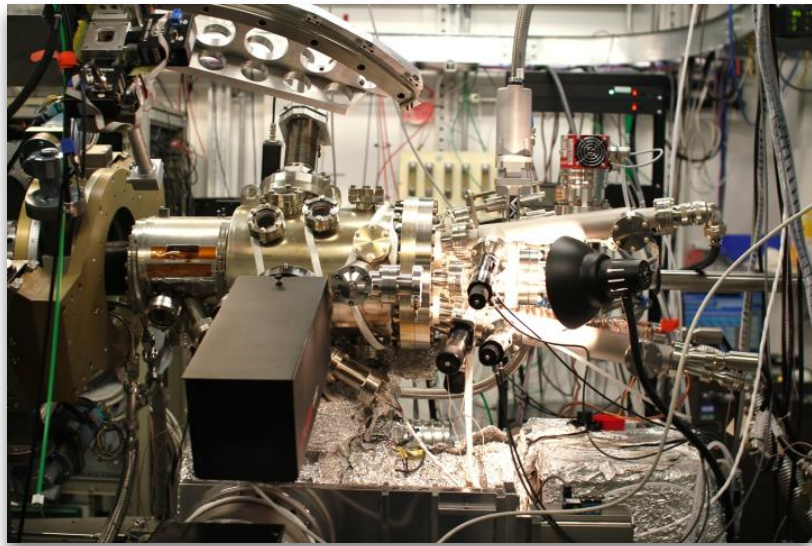
To account for disorder, defects, and non-equilibrium processes, we combine insights from theory and experiment into one fitting procedure

Experiment  $R^2 = \chi^2 + \chi_{res}^2 + \frac{1}{2} \frac{\kappa}{kT} \sum_I (\zeta_I - Z_I)^2$  DFT

Fit residual  $R^2$  for non-linear least squares fitting of atomic positions  $\{\zeta_I\}$ , Debye-Waller factors  $\{\sigma_I\}$ , and occupancies  $\{\theta_I\}$  of each atom.

- Experimental chi-squared  $\chi^2$  constrains predicted structure factor  $|F(\zeta, \sigma, \theta)|^2$  to measured structure factor  $|F_{exp}|^2$ .
- Resonant ( $\chi_{res}^2$ ) and non-resonant ( $\chi^2$ ) data may both be included in residual.
- Penalty function prevents atomic positions  $\{\zeta_I\}$  from varying significantly from the DFT predicted positions  $\{Z_I\}$ .
- $\kappa/kT$  determines weight of the penalty function compared to  $\chi^2$  with effective spring constant  $\kappa$  and temperature dependent energy scale  $kT$ .

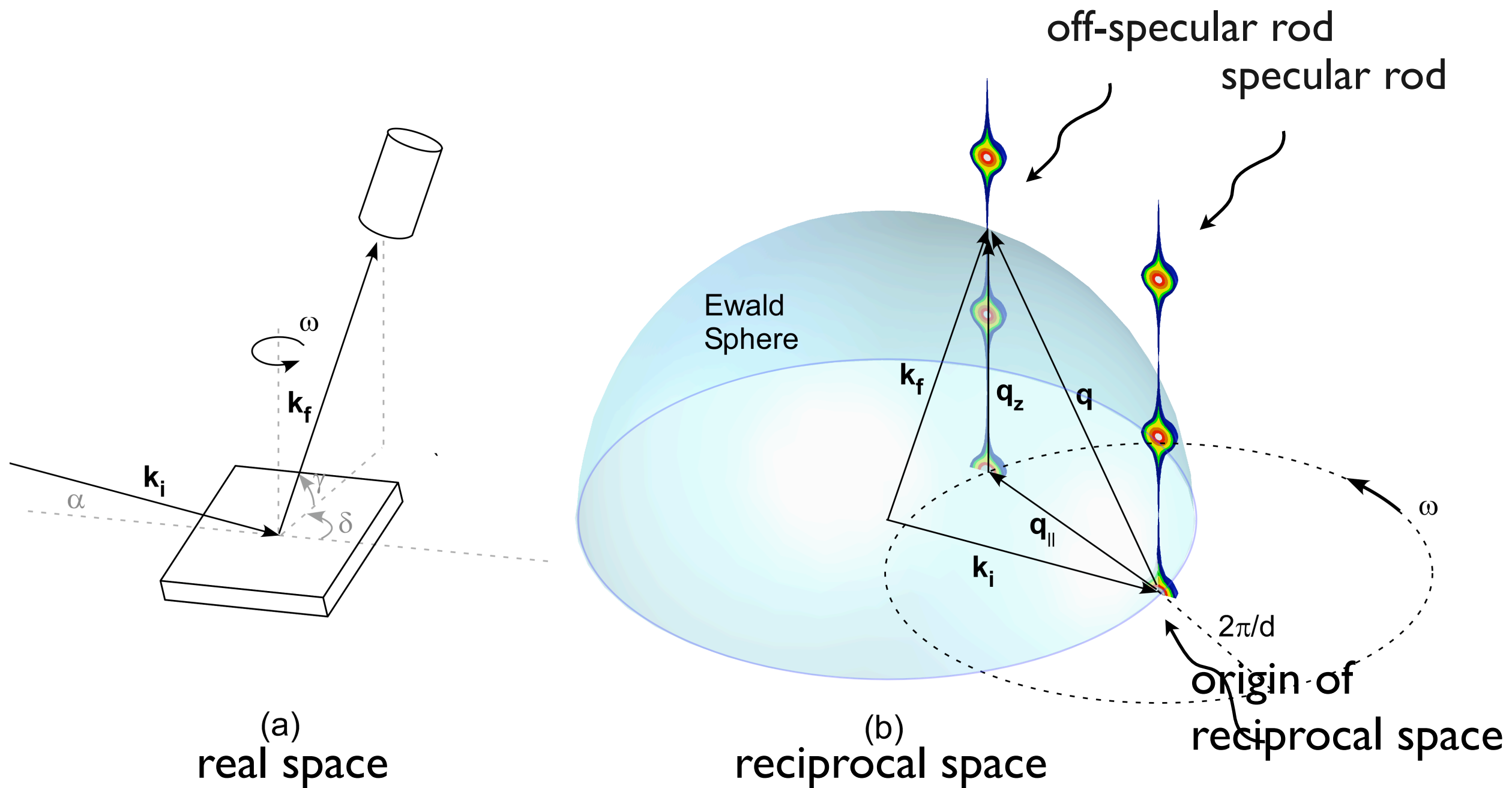
# Another way: DFT + fitting: here the SrTiO<sub>3</sub> (001) surface



Chief advantage -- you get DFT-based information as well  
 - S.Y. Cook et al., *Sci.Adv.***5**, eaav0764 (2019)

# Practicalities

## SXRD geometry

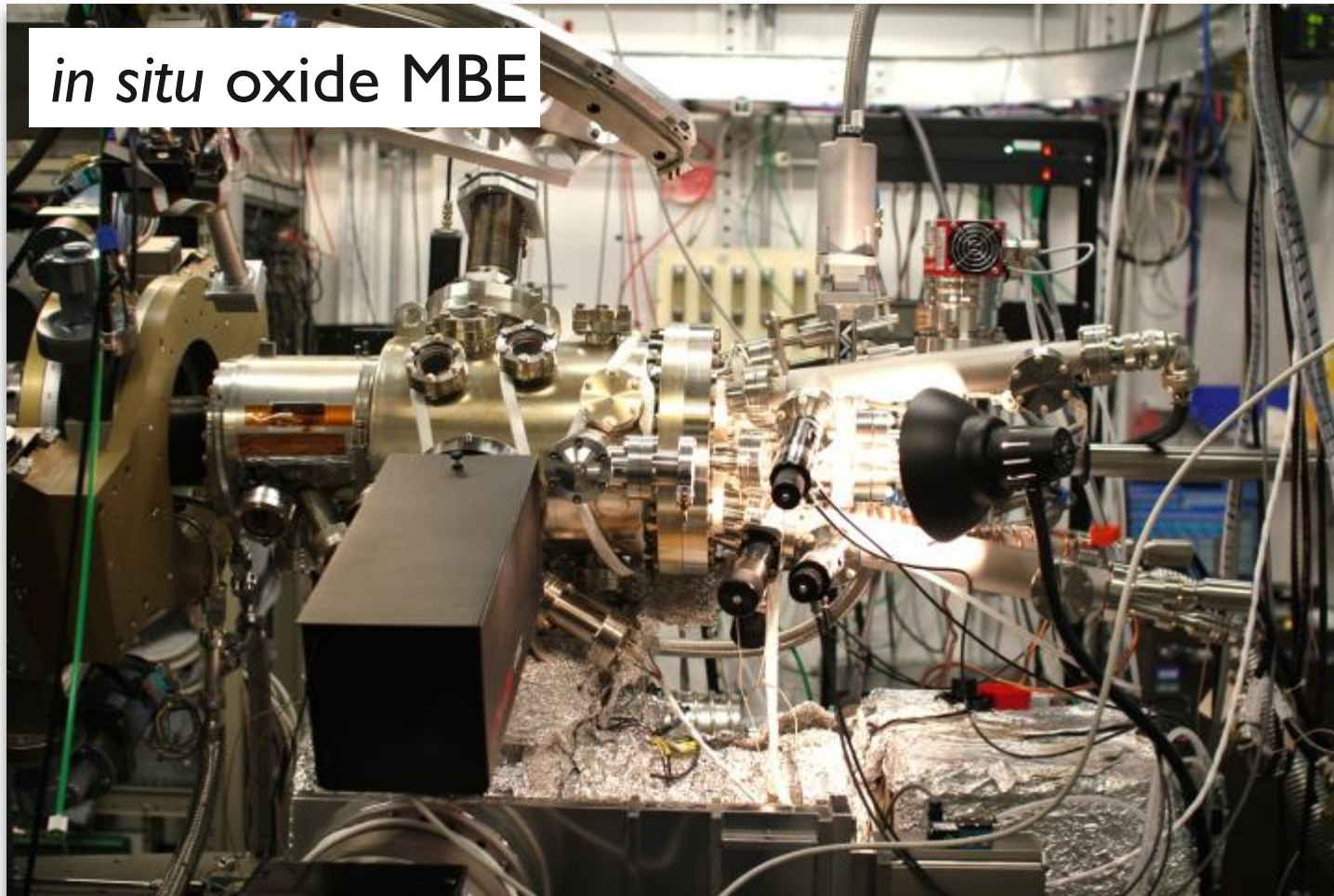


T.T. Fister & D. D. Fong in *Thin Film Metal-Oxides*, Springer (2010)

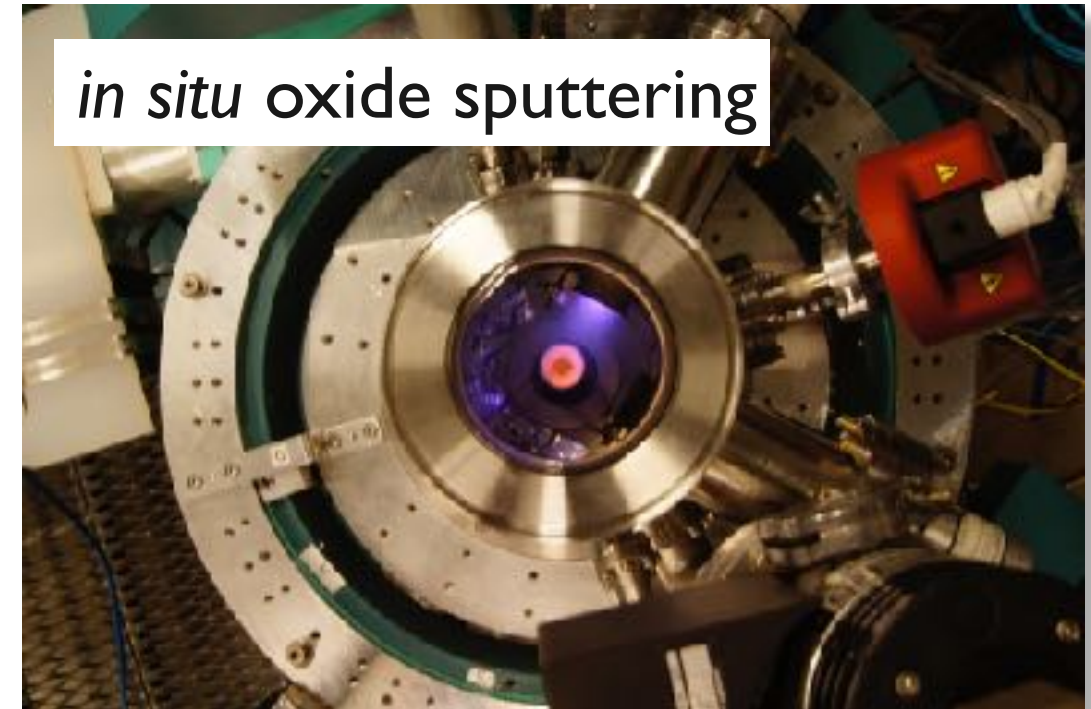


# SXRD geometry + a lot of equipment

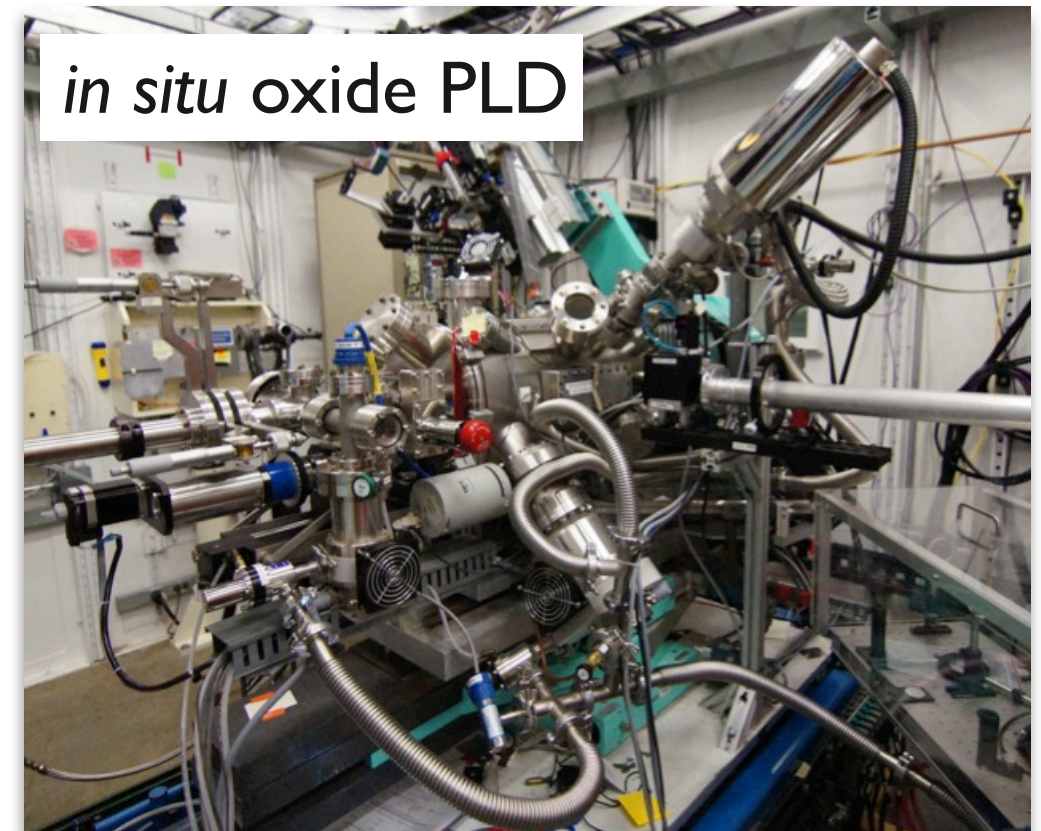
*in situ* oxide MBE



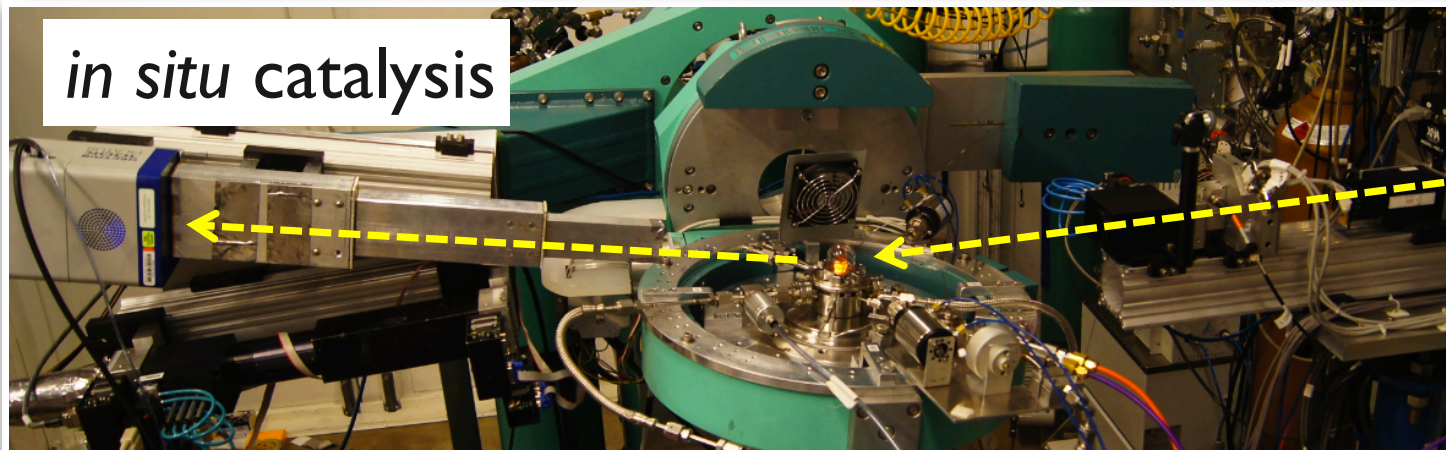
*in situ* oxide sputtering



*in situ* oxide PLD



*in situ* catalysis



- Can do a lot by combining SXRD + *in situ*
- Need to have the proper geometry

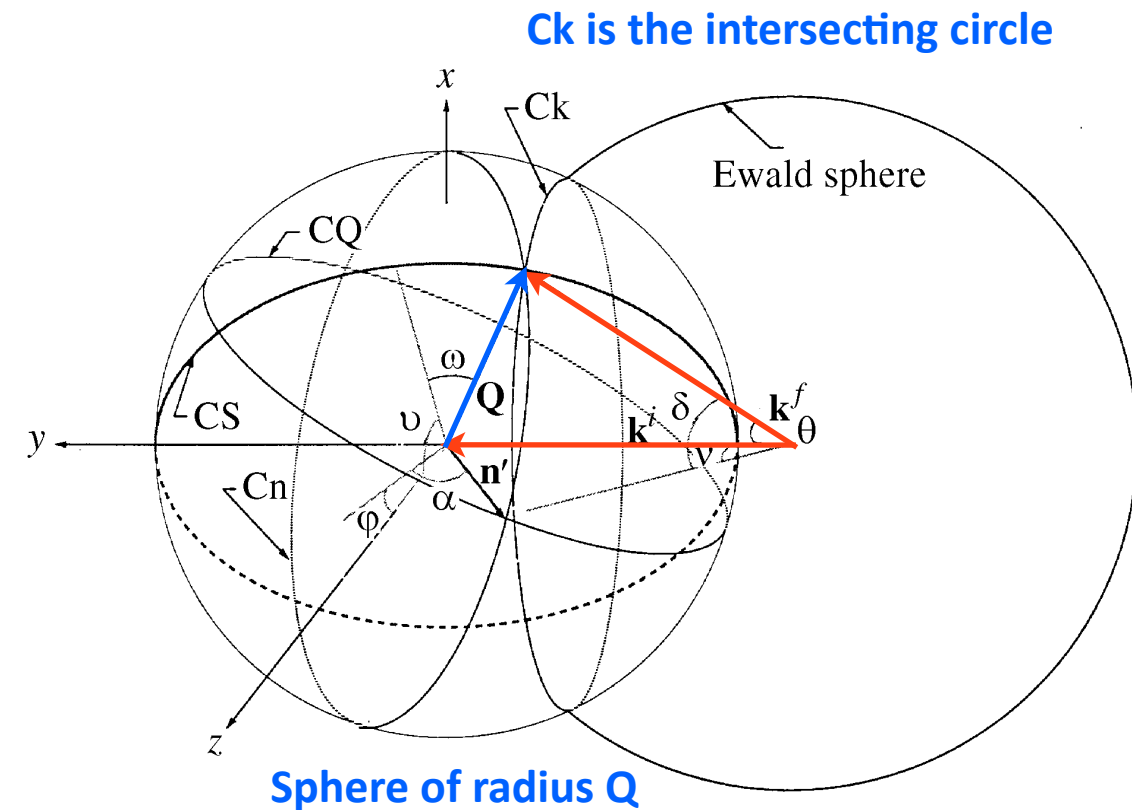
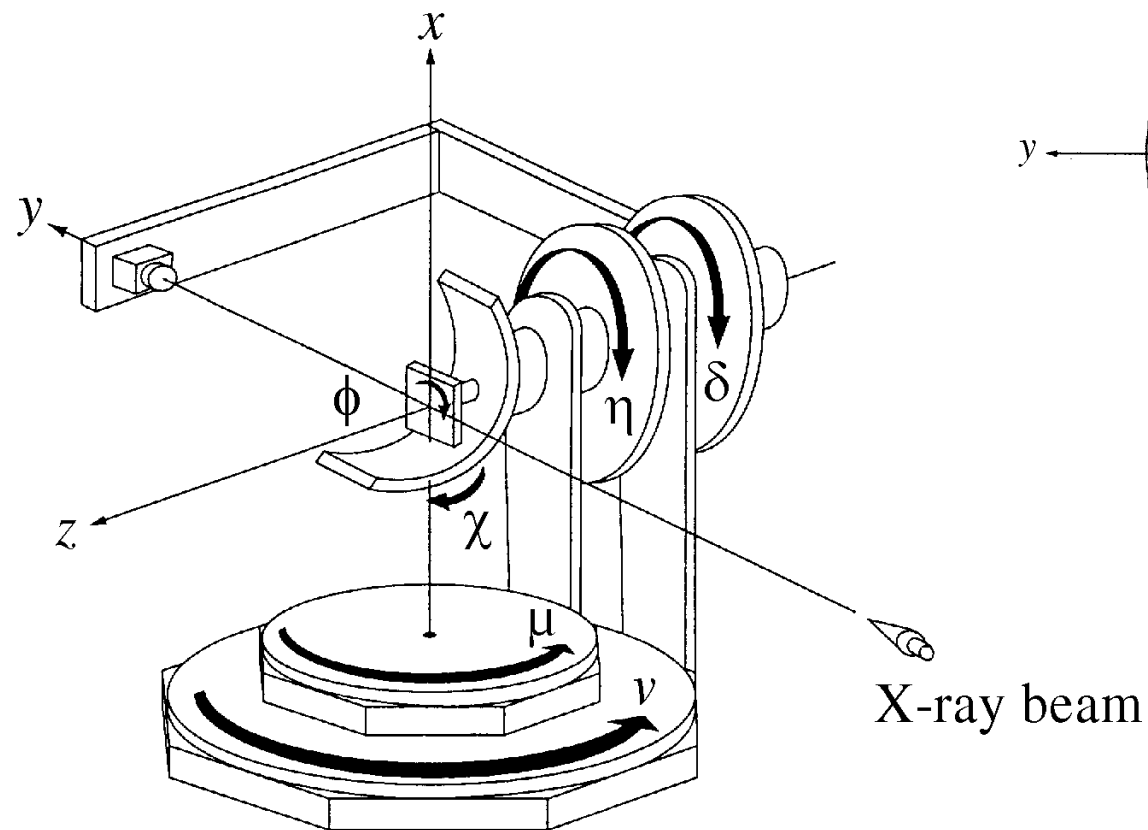


# Six-circle geometry (4S+2D)

Note the laboratory coordinate system (x,y,z)

Q is defined by

- $\theta = \omega =$  Bragg angle of Q ( $=4\pi\sin(\theta)/\lambda$ ) (longitudinal angle from xz-plane toward y)
- $\nu = \text{qaz} =$  azimuthal angle for Q (from z-axis)
- n (sample reference vector - often assumed equal to the sample normal)
- $\alpha =$  incident angle (longitudinal angle from xz-plane toward y)
- $\phi = \text{naz} =$  azimuthal angle for n (from z-axis)
- typically, n = sample normal
- $\text{naz} = 0$ : sample normal along z
- $\text{naz} = 90^\circ$ : sample normal along x



H.You, J.Appl. Cryst. **32**, 614 (1999)

T.T. Fister et al., J.Appl. Cryst. **46** (2013)

## Six-circle geometry

First, relate  $\mathbf{h}$  (i.e.,  $\mathbf{Q}$ ) to  $(x, y, z)$  [4S]

Next, relate  $\mathbf{k}_f$  to  $(x, y, z)$  [2D]

Next, by definition: at diffraction condition:  $\mathbf{h} = \mathbf{k}_f - \mathbf{k}_i$

4S

$$\mathbf{h} \xrightarrow{\mathbf{B}} \mathbf{h}_c \xrightarrow{\mathbf{U}} \mathbf{h}_\phi \xrightarrow{\Phi} \mathbf{h}_\chi \xrightarrow{\mathbf{X}} \mathbf{h}_\eta \xrightarrow{\mathbf{H}} \mathbf{h}_\mu \xrightarrow{\mathbf{M}} \mathbf{h}_M,$$

$$\Phi = \begin{pmatrix} \cos \phi & \sin \phi & 0 \\ -\sin \phi & \cos \phi & 0 \\ 0 & 0 & 1 \end{pmatrix},$$

$$\mathbf{X} = \begin{pmatrix} \cos \chi & 0 & \sin \chi \\ 0 & 1 & 0 \\ -\sin \chi & 0 & \cos \chi \end{pmatrix},$$

$$\mathbf{H} = \begin{pmatrix} \cos \eta & \sin \eta & 0 \\ -\sin \eta & \cos \eta & 0 \\ 0 & 0 & 1 \end{pmatrix},$$

$$\mathbf{M} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \mu & -\sin \mu \\ 0 & \sin \mu & \cos \mu \end{pmatrix}.$$

$$\mathbf{h}_M = \mathbf{M}\mathbf{H}\mathbf{X}\Phi\mathbf{U}\mathbf{B}\mathbf{h}$$

2D

$$\mathbf{k}_0^f \xrightarrow{\Delta} \mathbf{k}_\delta^f \xrightarrow{\Pi} \mathbf{k}_\nu^f$$

$$\Delta = \begin{pmatrix} \cos \delta & \sin \delta & 0 \\ -\sin \delta & \cos \delta & 0 \\ 0 & 0 & 1 \end{pmatrix},$$

$$\Pi = \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \nu & -\sin \nu \\ 0 & \sin \nu & \cos \nu \end{pmatrix}.$$

$$\mathbf{k}_\nu^f = k\Pi\Delta \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} = k \begin{pmatrix} \sin \delta \\ \cos \nu \cos \delta \\ \sin \nu \cos \delta \end{pmatrix}$$

at diffraction condition:

$$\mathbf{h}_M = \mathbf{Q}_L,$$

where  $\mathbf{h}_M = \mathbf{M}\mathbf{H}\mathbf{X}\Phi\mathbf{U}\mathbf{B}\mathbf{h}$

and  $\mathbf{Q}_L = \mathbf{k}_\nu^f - \mathbf{k}_L^i = (\Pi\Delta - \mathbf{I}) \begin{pmatrix} 0 \\ k \\ 0 \end{pmatrix} = k \begin{pmatrix} \sin \delta \\ \cos \delta \cos \nu - 1 \\ \cos \delta \sin \nu \end{pmatrix},$

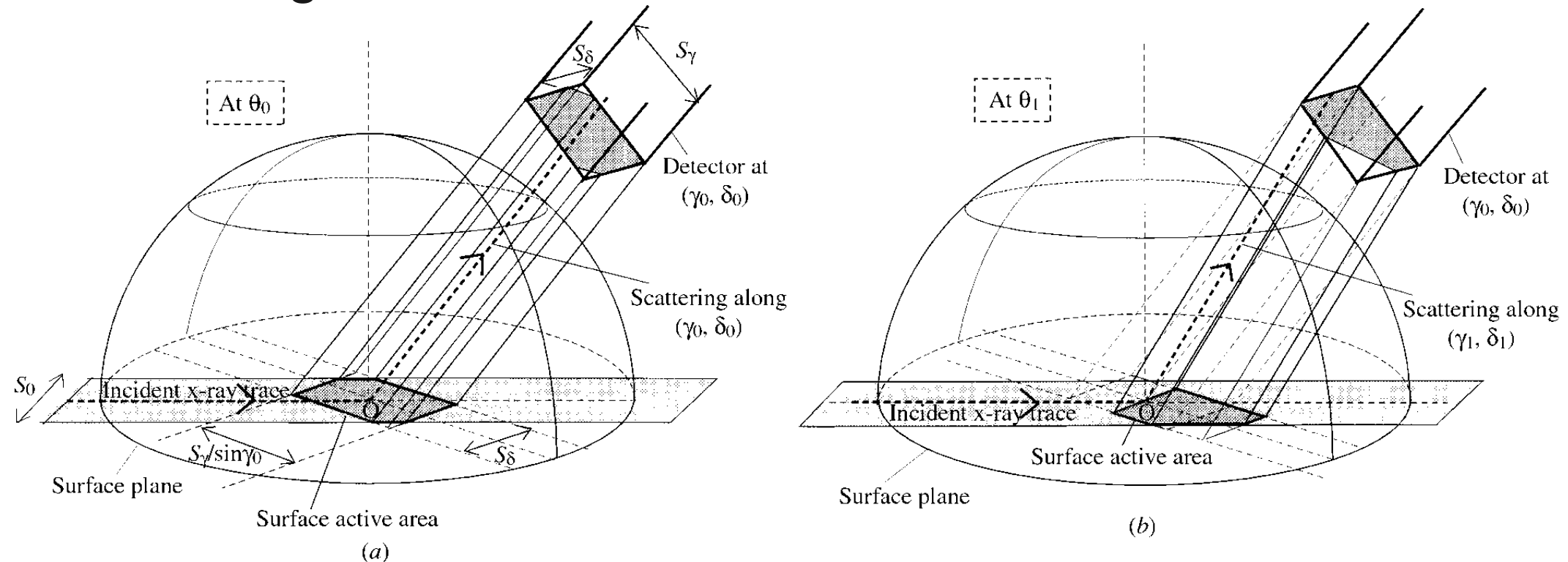
# Six-circle geometry

## Put everything into software

- spec -- <http://www.certif.com>
- modes for six-circle, four-circle, etc.
- then you can type (effectively) “go to 202; scan along 20L”

## Why do you need a six-circle?

- you can keep a constant x-ray footprint on the sample
- nice for  $L \sim 0$  work
- nice for easier geometrical corrections



N. Jedrecy, J. Appl. Cryst. **33**, 1365 (2000)

# Geometrical corrections

Integrated intensity often came from a  $\phi$ -scan+point detector

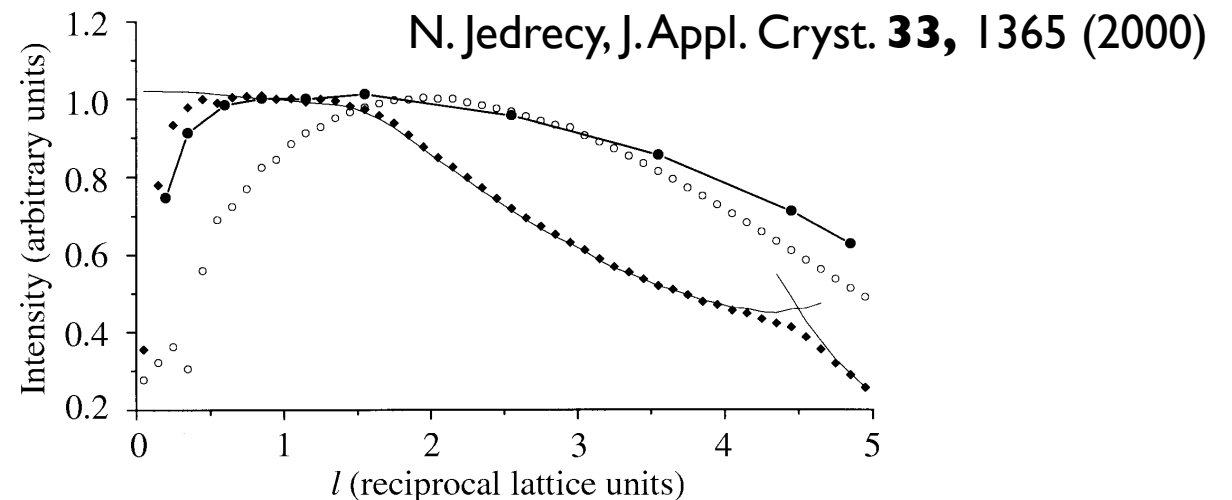
- Corrected integrated intensity

$$I_{\text{int},\phi} = (\Phi_0/\omega_0) \int (d\sigma/d\Omega) d\gamma d\psi d\phi,$$

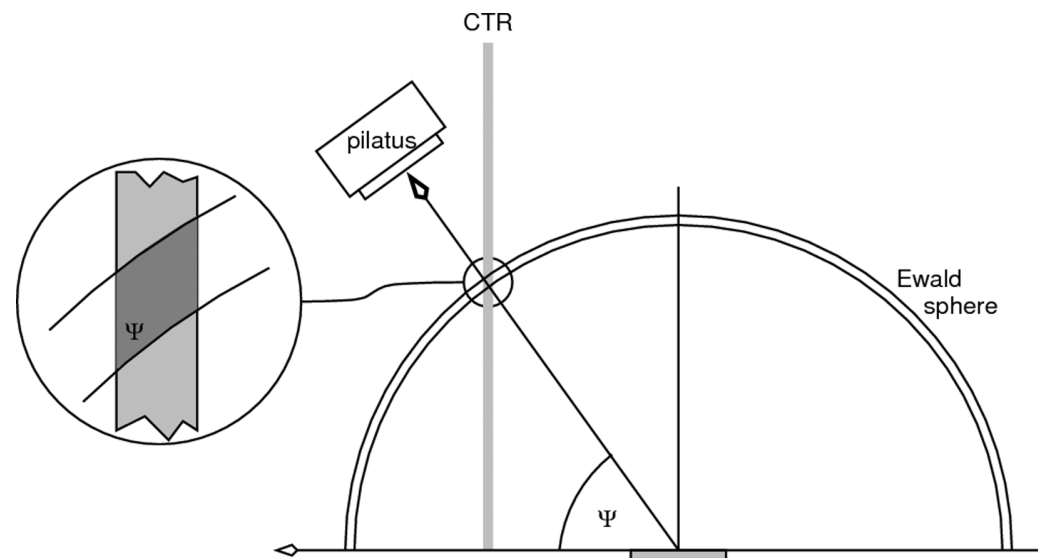
$$I_{\text{int},\phi} = (\Phi_0 r_e^2 A_0 \lambda^2 \Delta\gamma / \omega_0 A_u^2) |F_{hkl}|^2 C_{\text{tot}},$$

$$C_{\text{tot}} = PL_\phi C_{\text{rod}} C_{\text{area}} C_{\text{det}} C_{\text{beam}}.$$

E.Vlieg, J. Appl. Cryst. 30, 532 (1997)



- With 2D detectors (like Pilatus), it is easier, since we don't rock sample



still have polarization corrections:

**horizontal sample**

$$P_{\mathbf{n}_{\text{up,down}}} = 1 - \sin^2 \delta \cos^2 \gamma$$

$$P_{\mathbf{n}_{\text{in,out}}} = 1 - (\sin \alpha \cos \delta \cos \gamma + \cos \alpha \sin \gamma)^2$$

**vertical sample**

$$C_{\text{tot, spec}} = P \left[ \frac{A_{\text{num}}}{\sin \alpha} \right]$$

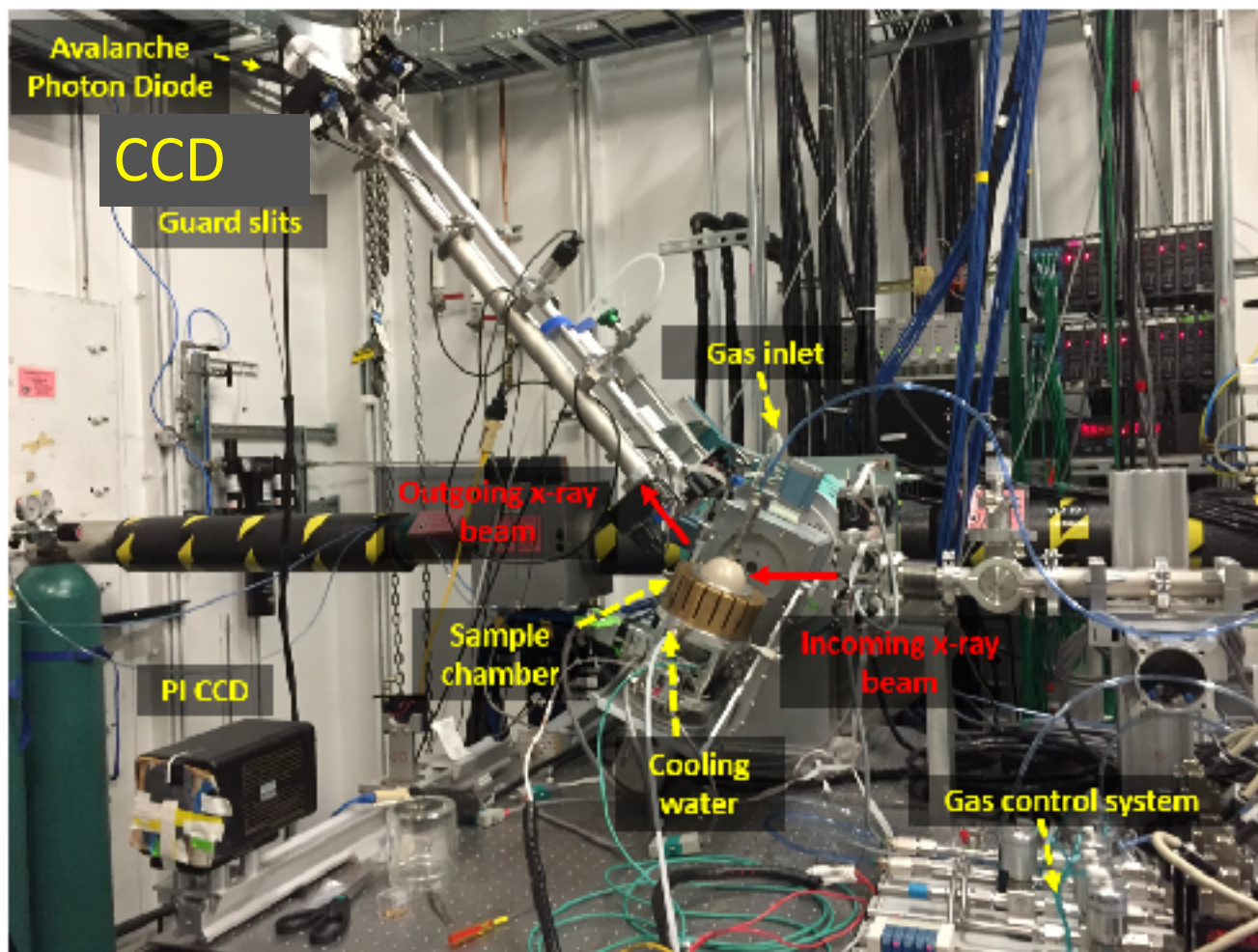
$$C_{\text{tot, non-spec}} = P \left[ \frac{1}{\cos \delta \sin(\nu - \alpha)} \right]$$

C. M. Schlepütz et al., Acta Cryst. A **61**, 418 (2005)



# Example of SXRD + X-ray photon correlation spectroscopy

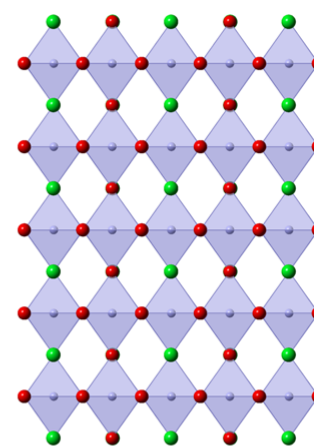
# In situ SXR D with gas control system ( $N_2 \leftrightarrow O_2, T$ )



APS, Sector 8

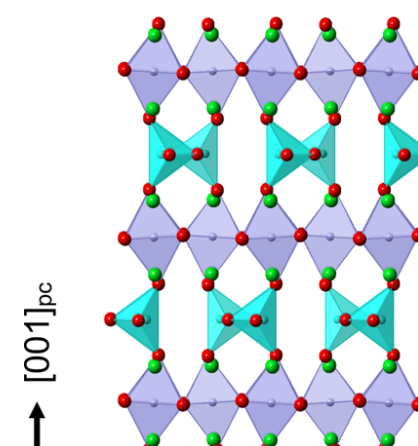
$N_2 \leftrightarrow O_2$

$SrCo^{4+}O_3$



$a_{||} \sim 0.383 \text{ nm}$

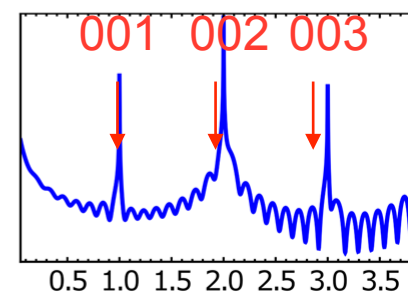
$SrCo^{3+}O_{2.5}$



$[001]_{pc}$   
 $[110]_{pc}$

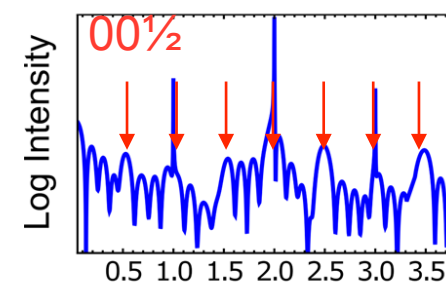
$a_{||} \sim 0.389 \text{ nm}$

$SrCoO_3$



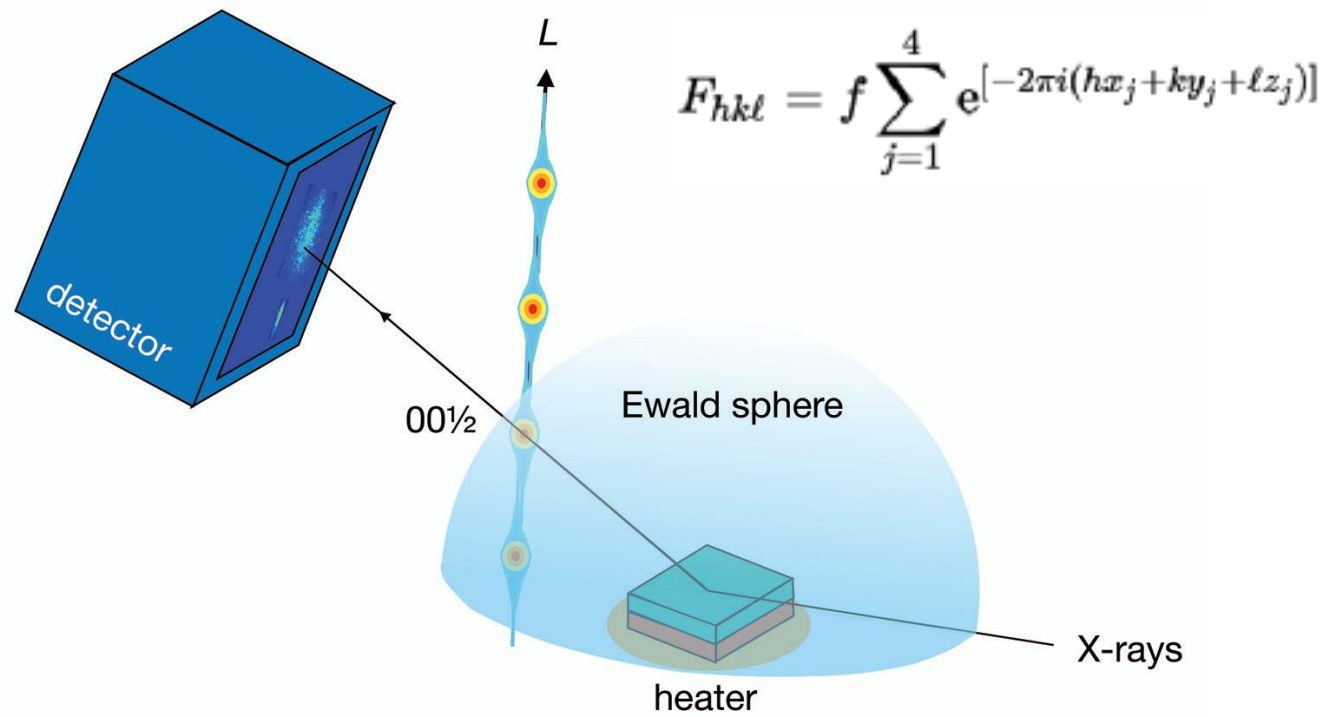
L (r.l.u.)

$SrCoO_{2.5}$

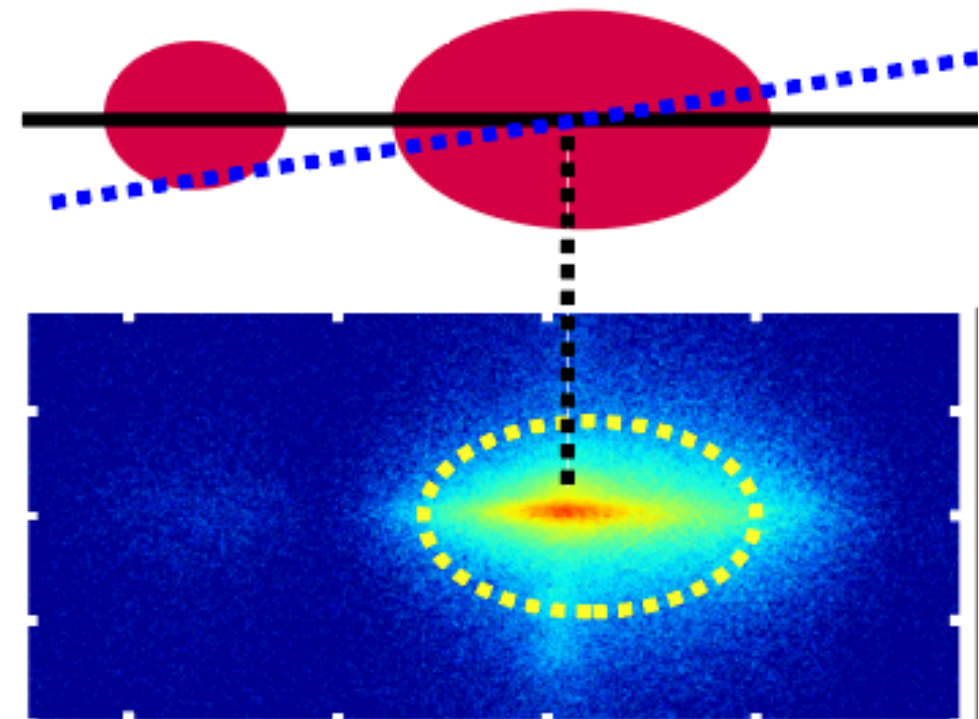


L (r.l.u.)

# Time-dependent speckle reveals dynamics

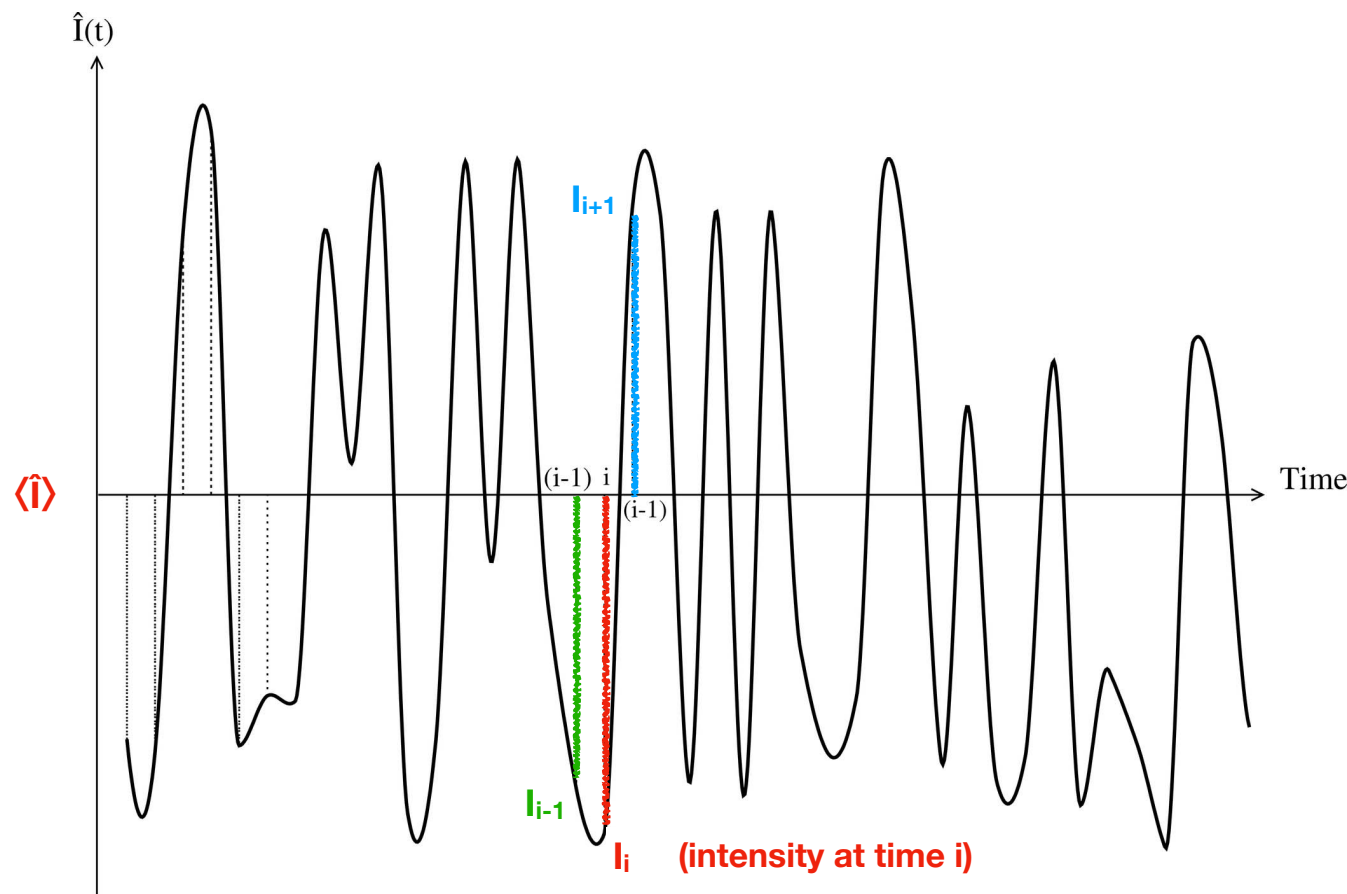


001/2 BM  
Bragg Peak



J. K. Wenderott et al. Adv. Mater. Int. 2300127 (2023)

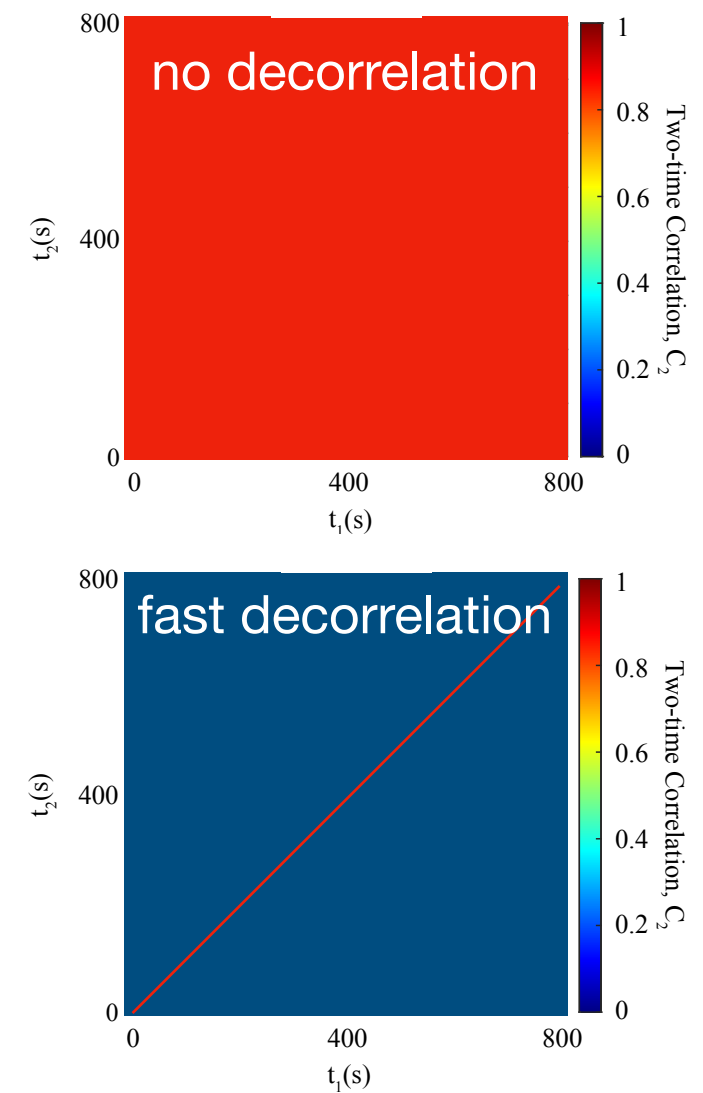
# Dynamics and time correlations (at any $Q$ )



Two-time correlation function ( $C_2$ ) at  $Q$ :

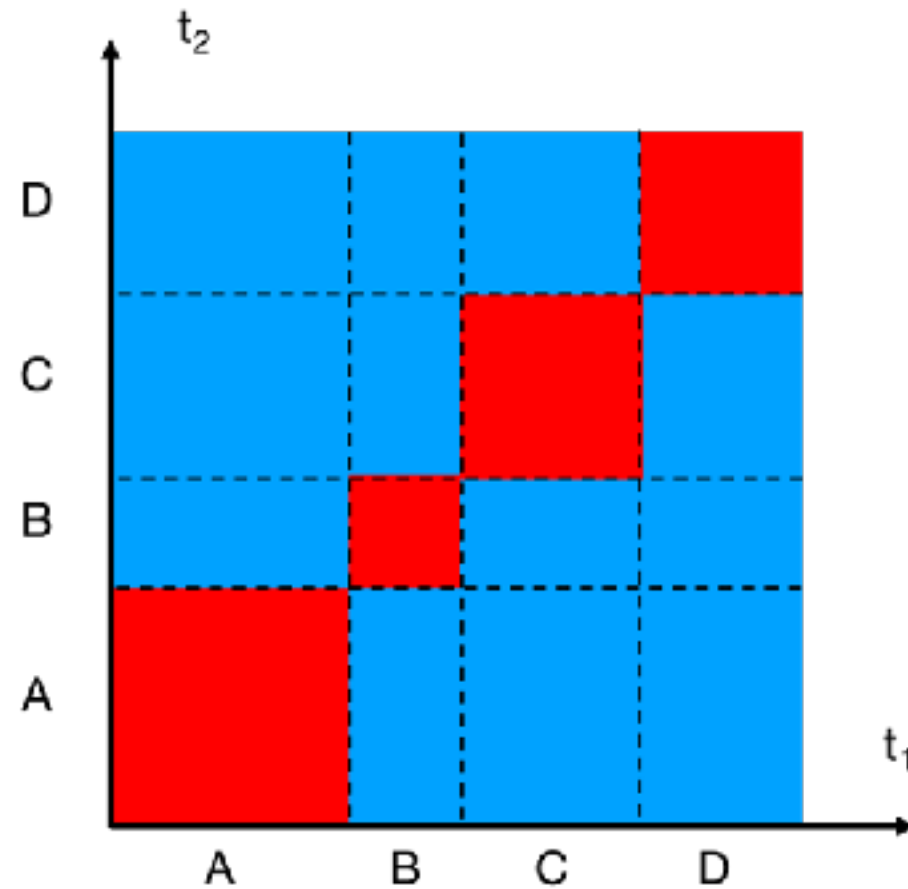
$$C_{m,n}(t_1, t_2) \left( \frac{I_{m,n}(t_1) - I_{m,n}^{inc}}{I_{m,n}^{inc}} \right) \left( \frac{I_{m,n}(t_2) - I_{m,n}^{inc}}{I_{m,n}^{inc}} \right) \rangle_q$$

O. Bikondoa, J. Appl. Cryst. **50**, 357 (2017)



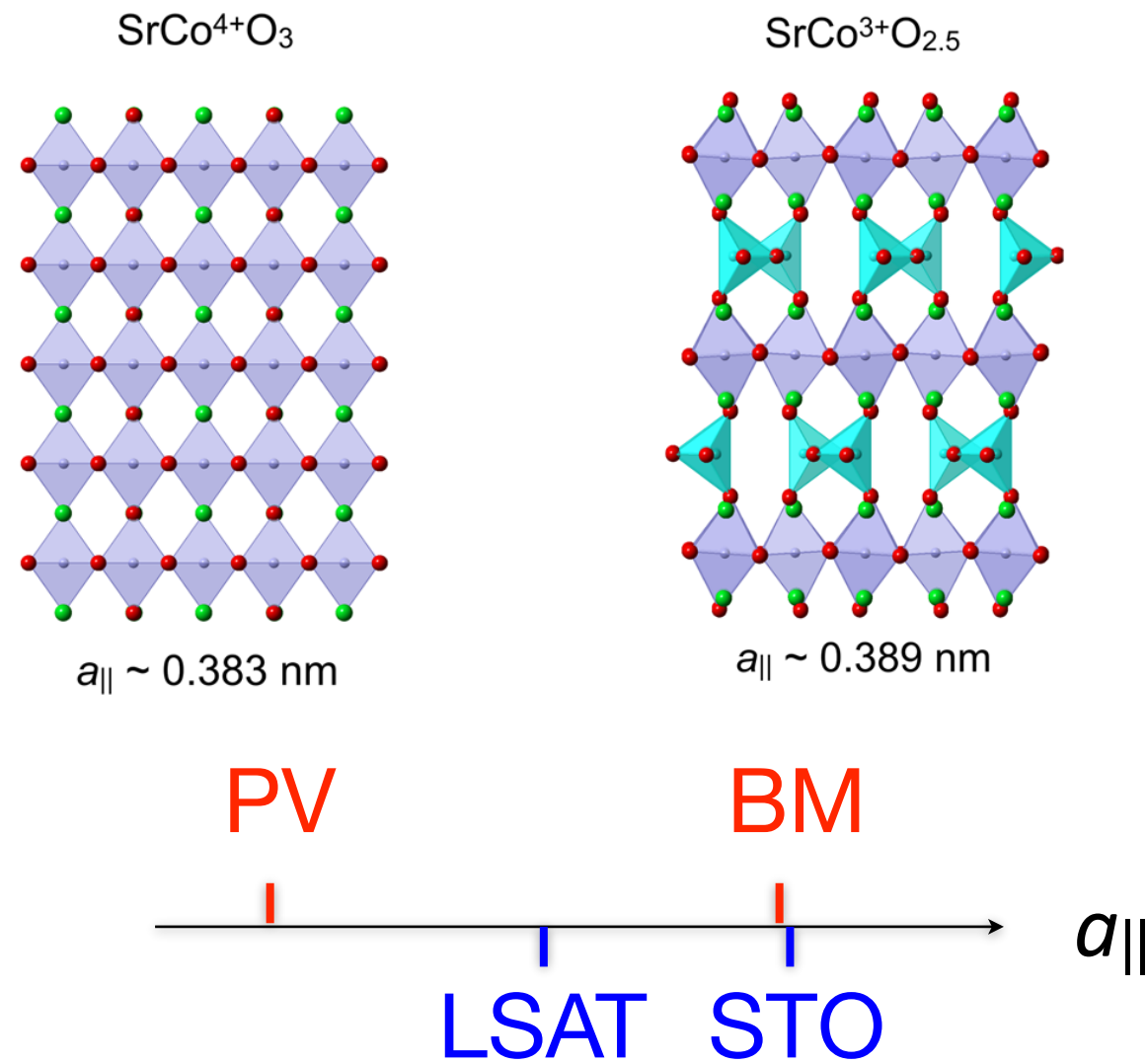


# Dynamics and time correlations (at any $Q$ )



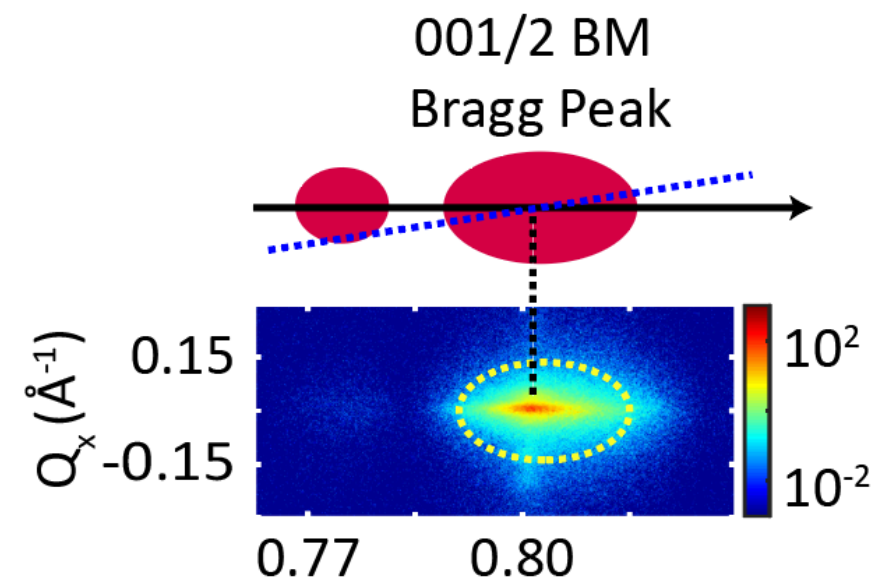
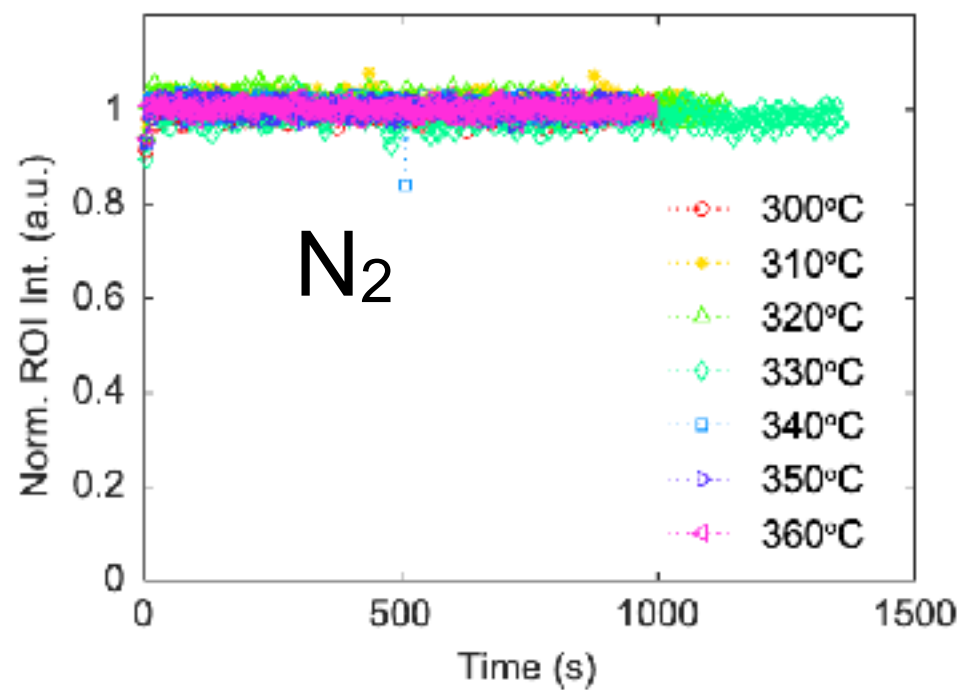
state of material varies from A to B to C to D

# SrCoO<sub>x</sub>/LSAT (001) phase equilibrium



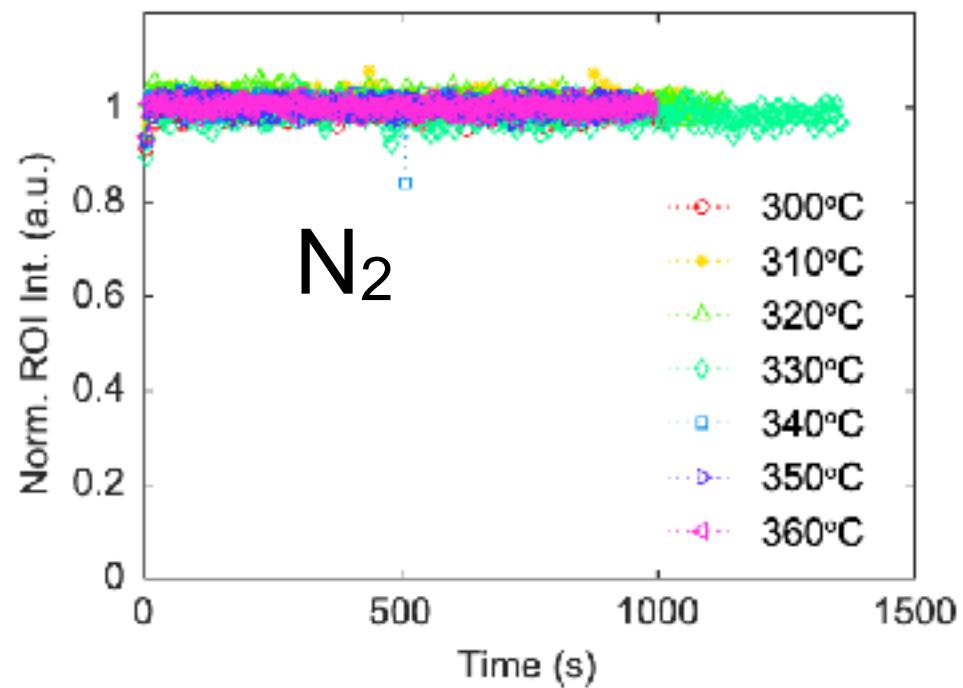
# SrCoO<sub>x</sub>/LSAT (001): Kinetics in N<sub>2</sub>

Intensity of  
001/2: stable  
with time

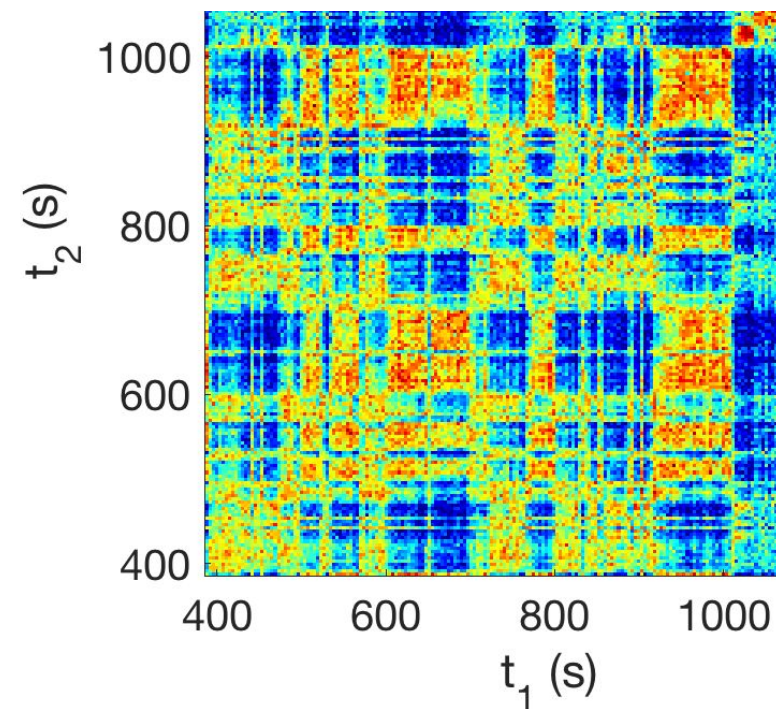


# SrCoO<sub>x</sub>/LSAT (001): Dynamics in N<sub>2</sub>

Intensity of  
00 $\frac{1}{2}$ : stable  
with time



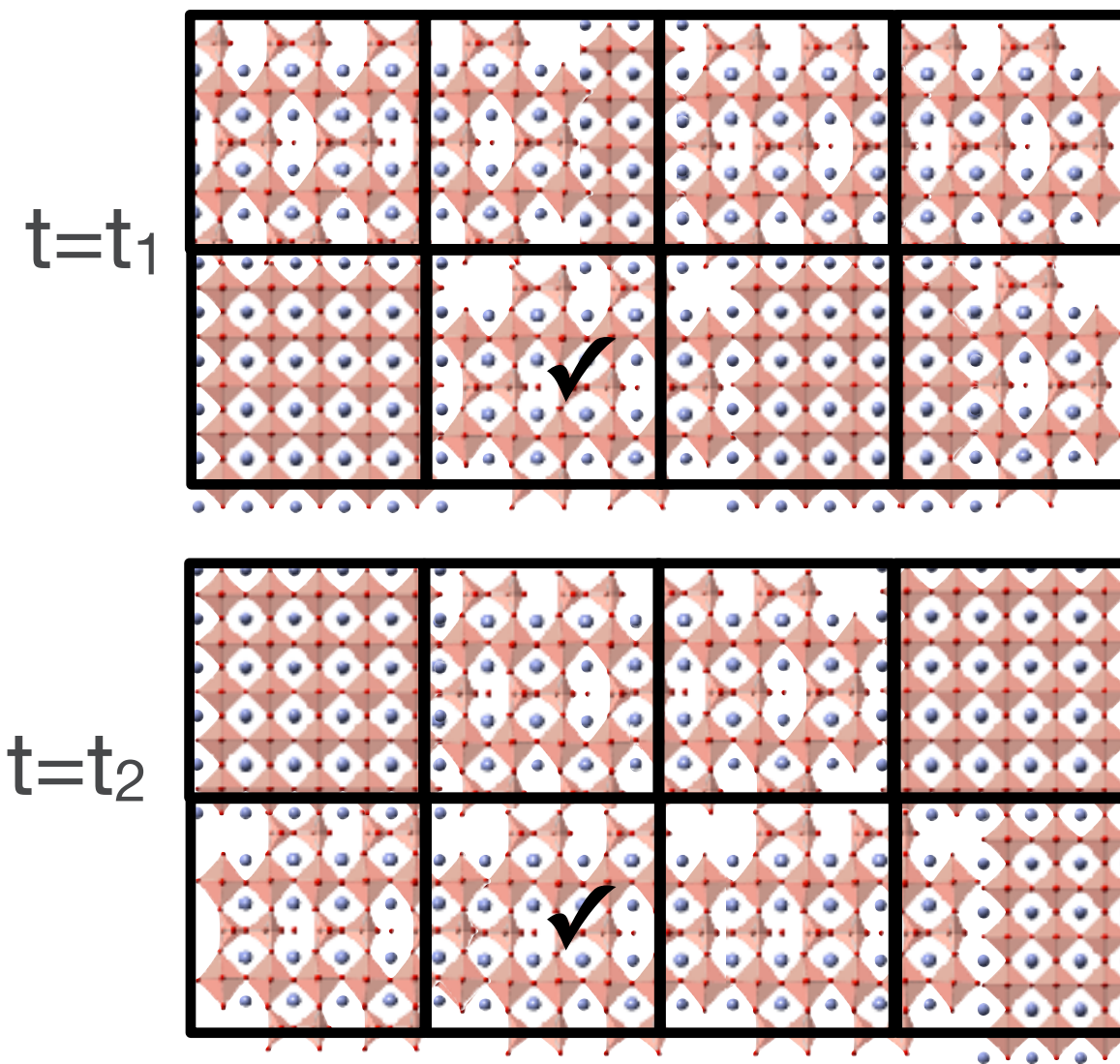
Dynamics of  
00 $\frac{1}{2}$ : fluctuating  
with time



N<sub>2</sub> at 350°C



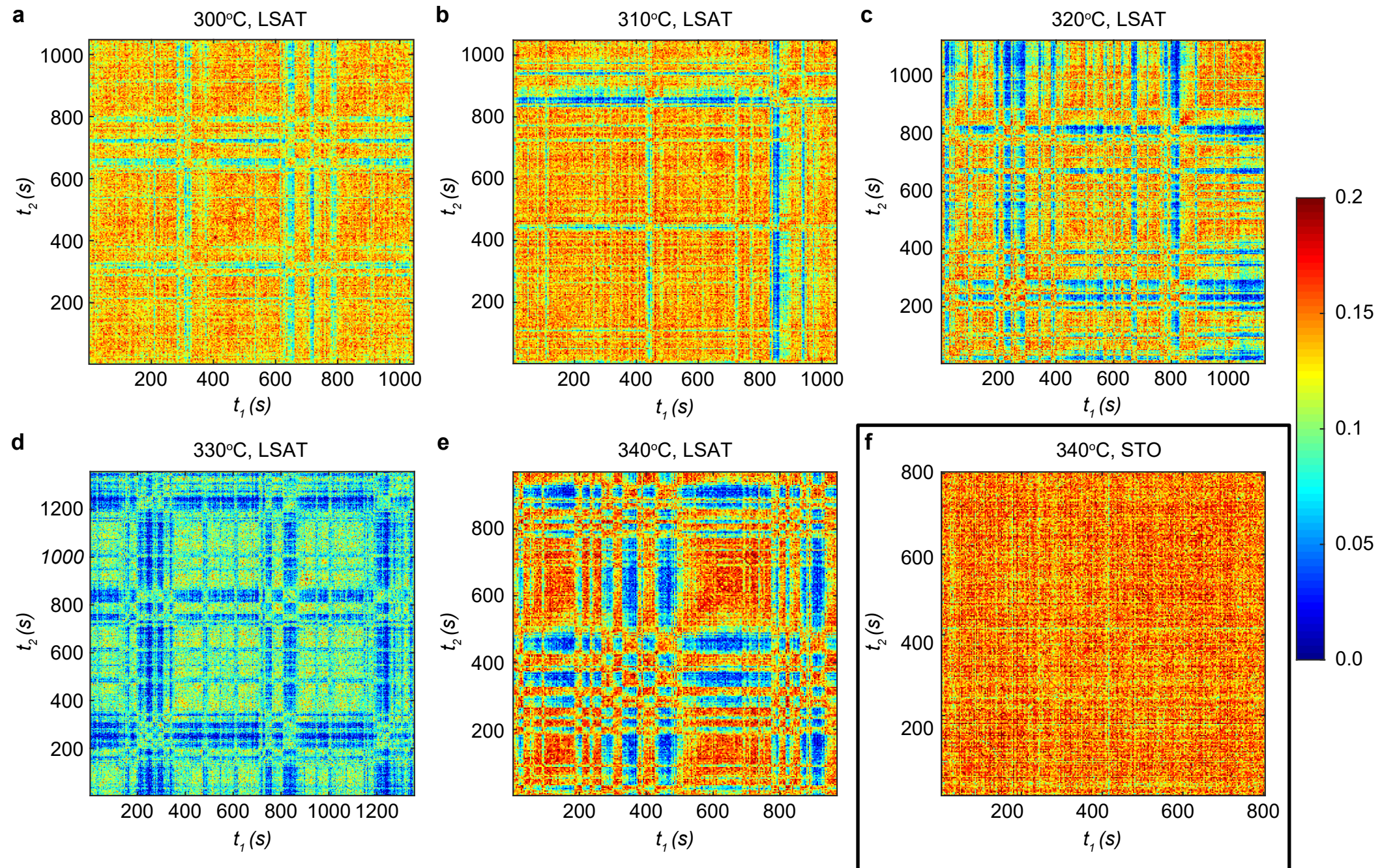
# Real space: vacancy fluctuations at 350°C



partially correlated in time



# Temperature dependence



Questions?

<https://forms.office.com/g/MdYE7snFqs>

NXS Lecture - Dillon Fong:  
"Surface and Interface Scattering"



<https://forms.office.com/g/MdYE7snFqs>